

**VALIDATION OF KENO V.a
COMPARISON WITH CRITICAL EXPERIMENTS**

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ABSTRACT

Section 1 of this report documents the validation of KENO V.a against 258 critical experiments. Experiments considered were primarily high or low enriched uranium systems. The results indicate that the KENO V.a Monte Carlo Criticality Program accurately calculates a broad range of critical experiments. A substantial number of the calculations showed a positive or negative bias in excess of 1½% in k-effective (k_{eff}). Classes of criticals which show a bias include 3% enriched green blocks, highly enriched uranyl fluoride slab arrays, and highly enriched uranyl nitrate arrays. If these biases are properly taken into account, the KENO V.a code can be used with confidence for the design and criticality safety analysis of uranium-containing systems.

Section 2 of this report documents the results of investigation into the cause of the bias observed in Sect. 1. The results of this study indicate that the bias seen in Sect. 1 is caused by code bias, cross-section bias, reporting bias, and modeling bias. There is evidence that many of the experiments used in this validation and in previous validations are not adequately documented. The uncertainty in the experimental parameters overshadows bias caused by the code and cross sections and prohibits code validation to better than about 1% in k_{eff} .

1. VALIDATION OF KENO V.a IN Y12CSG

1.1 INTRODUCTION

The KENO V.a Monte Carlo Criticality Program is currently being validated in several different ways. Each of these validations will be reported separately. The intent of this study is to validate KENO V.a¹ in the Y12CSG package against critical experiments. Y12CSG is a frozen version of a system of nuclear criticality safety computer codes similar to the nuclear criticality safety codes available through the SCALE² package. The sequence which is being validated is the CSAS25 sequence documented in CSAS4 of the SCALE manual. The sequence uses control module CSAS25 created on 85.162 and program modules Q#008 (BONAMI-2) created on 85.011, Q#002 (NITAWL) created on 85.011, and Q#009 (KENO V.a) created on 85.162. The 27-group ENDF/B-IV cross-section master library created on 84.066 and stored in data set Y.LMP12852.Y12CSG.X27 was used for all calculations.

The purpose of a code validation is manifold. ANSI Standard ANS-8.1³ requires that calculational methods used for criticality safety be validated and any bias be determined by correlating the results of critical experiments with calculations. In the past, the primary source of criticality safety information applicable to the handling of fissile material outside of nuclear reactors was obtained from critical experiments or from nuclear safety guides and handbooks based upon critical experiments. These experiments were costly and often took a substantial amount of time before the results were available. With the closing of many of the critical experiment facilities, using critical experiments for operational criticality safety approval has become virtually impossible. Increasing reliance is being placed upon calculational methods to fill in and extend existing experimental data. Extension of data has been accomplished by making use of trends in the bias established in code validation. It is essential that the computational methods used for nuclear criticality safety purposes be sufficiently accurate that one can be confident of subcriticality when adequate safety margins are applied. It is also important that the applied safety margins not be unduly conservative. To accomplish both of these goals simultaneously requires the ability to accurately predict the neutron multiplication factor of a system.

This portion of the KENO V.a validation is based primarily on uranium experiments which have been used in the past for KENO validation.⁴⁻⁸ The validation is being done independent of any particular nuclear criticality safety organization, with close cooperation with the authors of the code and personnel familiar both with the codes and many of the critical experiments which were used in the earlier validations. In this manner, trends in the bias can be identified and areas of applicability can be established. In addition, calculational deficiencies may be identified and possibly eliminated.

A total of 258 low enriched (<5% U-235) and highly enriched (~90% U-235) experiments have been modeled. These include various solution systems, intermediate density systems, and uranium oxide and metal systems. Four primary sources of bias were identified during the course of the validation. These were (1) bias caused by approximations and the manner in which the theory was implemented in portions of the code (code bias), (2) bias caused by the group structure of the cross sections (cross-section bias), (3) bias caused by the manner in which the experiments were reported versus what was actually done (reporting bias), and (4) bias caused because of the manner in which the analyst chose to model the critical experiment (modeling bias). Mitigation of the bias for the first two cases is fairly straightforward since they are systematic and are introduced by the KENO program and control modules. If trends can be established, it may be possible to eliminate bias in future updates to the codes. The third source of bias, reporting bias, is not well defined and is much more difficult to resolve. Reporting bias is very difficult to distinguish from code and cross-section bias without additional information beyond what was originally reported. The necessary details which have been omitted are different from experiment to experiment and are influenced by the date the experiments were performed along with the prevailing

belief of the experimenters of what was important and what could be ignored. The fourth source, modeling bias, is bias which stems from the analyst's model and is also difficult to distinguish from other forms of bias, especially when the analyst chooses to ignore (or include) specific portions of a model based on past experience with similar calculations.

The results of this validation are reported in Sect. 1. The discussion of the cause-and-effect of the identified bias for the experiments are presented in Sect. 2. In Sect. 2, many of the calculations were performed with modified versions of the code and with adjusted parameters. The results in Sect. 2 should not be considered part of the validation of the code. They are presented in order to aid in establishing the source of the bias observed in the validation.

1.2 DESCRIPTION OF THE CODE PACKAGE

1.2.1 CSAS25 Module

The CSAS25 control module allows simplified data input to the functional modules such as BONAMI, NITAWL, and KENO V.a. The module will calculate atomic densities for both mixtures and standard solutions. The module also generates input data for NITAWL, allowing various options for treatment of the cross sections in the resonance region for both homogeneous and heterogeneous systems. Since the earlier validations reported in refs. 6 and 7, several corrections have been made to the CSAS25 control module.

1.2.2 BONAMI

For the 27-group master cross-section library used in this validation, the primary purpose of the BONAMI functional module is to select the required material cross sections and to create a smaller master cross-section library to be processed by NITAWL. There is no data processing done in BONAMI for the 27-group cross-section library.

1.2.3 NITAWL

The NITAWL functional module treats the resonance region cross sections for resonance absorbers. The treatment is based on the Nordheim Integral Transform method. The analyst has the option of treating the resonance parameters in the manner most appropriate for the problem detail. The options include (1) an homogeneous medium treatment which treats the resonance region of the fissile mixture as if it were an infinite homogeneous media, and (2) a finite lump treatment which treats the resonance region as if the fissile mixture were in a discrete lump with a 1/E return flux at the boundary for problems where the system is substantially heterogeneous or where reflector effects are important. These options are automatically invoked in the CSAS25 module according to the keywords INFHOMMEDIUM, LATTICECELL, or MULTIREGION. The INFHOMMEDIUM option treats the fissile mixture as an infinite homogeneous medium. The LATTICECELL option utilizes a multiple repeated cell for the resonance self-shielding correction. With the MULTIREGION option, a single-cell resonance self-shielding calculation is made.

1.2.4 KENO V.a

KENO V.a is a substantial revision of KENO IV,⁹ and includes an enhanced geometry package which allows modeling of a wide variety of complex three-dimensional geometries. The geometry package allows nested arrays and "holes" to be placed in the geometry model. The code allows the use of reflector options, including mirror reflection, differential albedo reflection, and an automatic reflector; the latter has the capability of using reflector region weighting functions which are based on one-dimensional adjoint calculations. The reflector options simplify geometry data input and/or reduce the

running time of a specific problem. Cross-section input and atom density input are handled by the CSAS25 module. Most of the major KENO parameters have defaults which work for a wide variety of problems, but which can be overridden if the problem or analyst dictates. The major revision to KENO V.a since the validations reported in refs. 6 and 7 is that the program module ICE has been deleted, and KENO V.a mixes its own cross sections. In addition, there have been a few changes in the program logic involving the treatment of computer round-off error during tracking.

1.2.5 The 27-Group Neutron Cross-Section Library

The 27-group cross-section library was created in August 1981 from the ENDF/B-IV 218-group master library.¹⁰ (It should be noted that ref. 10 does not include a discussion of all the nuclides which have been placed in the 218-group library and that several of the nuclides have been regenerated since the document was issued.) Prior to 1981, the primary cross-section set in use at ORNL was the Knight-Modified Hansen-Roach, 16-group cross-section library. The 27-group set is considered to be an improvement because more thermal neutron groups are available, upscatter is included in the set, and the origin of the base data used to create the data set is better documented. The 27-group set was collapsed with the weighting spectra which was generated with the 218-group library and which was based on the weighting spectra used to prepare the 218-group library from ENDF/B-IV data.

1.3 CALCULATIONAL PROCEDURE

In the KENO V.a validation process, many of the available options in CSAS25 and KENO V.a were exercised. These options include the automatic atomic density generation features, the various treatments in NITAWL, and the geometry and reflector options in KENO V.a. This was done in order to validate the mechanics and capabilities of the code for a broad spectrum of problems. The majority of the calculations repeat calculations which were modeled by different people at different times. Usually there are multiple ways that a problem may be specified, all of which are equally correct. The original input data were left substantially unchanged in order to allow testing for discrepancies or bias which might have been caused by the differences in analysts' problem specifications. A complete listing of the input data has been included in Appendix A.

The resonance treatment used was the one which appeared to most accurately fit the problem specifications. All problems were run for 103 generations of 600 neutrons per generation. Some problems were run using the adjoint reflector weighting (bias ID), whereas others were run using full neutron tracking in the reflector in order to test for bias which might be caused by one or the other treatment.

With KENO V.a, there is no single k_{eff} which is "the answer" for the problem. The code starts with an initial neutron distribution and calculates the effective multiplication for a generation of neutrons. The next generation uses a starting distribution based on the fission points of the previous generation and calculates the effective multiplication for the current generation. Since 103 generations were run, there are 103 different answers. In the ideal situation, once the source has converged and the original (and usually arbitrary) starting distribution has decayed, the difference in the batch-to-batch k_{eff} may be attributed to the statistical nature of the Monte Carlo calculation, and the "best" answer should be the average of the remaining calculations. The common practice in KENO V.a is to tabulate the average k_{eff} as a function of the number of generations skipped. Considerable judgment is then required in determining the answer. Many calculations do not approach the ideal situation. For example, under-sampling may exist where the number of neutrons per generation is not sufficient to sustain a proper source distribution, or the number of generations is insufficient to converge the source distribution. In order to remove the element of judgment from the interpretation of the results and to mechanize the process of validating and comparing results to previous validation, the average k_{eff} by generation skipped with the lowest calculated standard deviation is reported here. This number appears as the "final value"

in the plot of average k_{eff} by generation skipped in the KENO V.a output. The analyst is encouraged to review the tabulated results against the plots in Appendix B when using the validation for establishing safety margins for the different types of criticals which were run.

In each calculation, the optional parameter NUB was set to "yes" in KENO V.a so the program would calculate and print the average energy group of the neutron-causing fission. This parameter has been frequently used in past validations because of trends which have been observed and appear to be correlated.

1.4 PROBLEM DESCRIPTION AND RESULTS

A brief problem description and results are presented in Tables 1-6. The experimental models used to generate Table 1 are from low enriched uranium experiments obtained from ref. 8. These include experiments for homogeneous single-unit criticals, both reflected and unreflected, as well as heterogeneous uranium metal rods in water. The fissile compounds considered were UO_2F_2 , U metal, and U_3O_8 , all at 4.89% U-235 enrichment. The moderating materials were water, sterotex, and UO_2F_2 solution.

The experimental models used to generate Table 2 are from low enriched uranium experiments obtained from ref. 11. These experiments are formally undocumented experiments for 3.85% enriched uranium metal rods in water. The heterogeneous systems consist of large diameter rods which are water moderated. In some cases the rods have an internal hole which is also water moderated. The critical experiments were modeled in detail from descriptions in the experiment logbook. Extensive detail was included in these calculations in order to thoroughly test the KENO V.a geometry package.

Table 3 includes models from ref. 7 which were used for the validation of Y12CSG for the Oak Ridge Gaseous Diffusion Plant. The validation considered single-unit criticals, both reflected and unreflected, at several enrichments ranging from 1.4 to 4.98%. The first 30 experiments are UF_4 /paraffin-moderated systems and UO_2F_2 solution systems at various moderation levels. The last 20 experiments are 4.46% enriched damp oxide experiments performed at Rocky Flats. These later experiments test the code's ability to handle both intermixed and interstitial moderation. Several of the damp oxide experiments, which were driven by highly enriched uranium systems, were added to the series.

Highly enriched uranium experiments from ref. 8 were used to generate Table 4. These are UO_2F_2 and $\text{UO}_2(\text{NO}_3)_2$ solution systems. Both single-unit and array systems were analyzed under a variety of reflection conditions including unreflected, fully water reflected, concrete reflected, and Plexiglas reflected.

Table 5 includes experiments from ref. 6 which were used for validation of Y12CSG for the Y-12 Plant. Single-unit reflected and unreflected systems for uranium metal, uranium alloy, UO_2F_2 solution and $\text{UO}_2(\text{NO}_3)_2$ solutions were considered. Extensive calculations were performed on arrays, including (1) arrays of metal units with and without interstitial moderation, (2) arrays of UO_2F_2 slab systems, and (3) arrays of 5-liter containers of $\text{UO}_2(\text{NO}_3)_2$ having varying reflector thicknesses of paraffin and/or Plexiglas.

Table 6 contains the experimental models and results from the eta experiments performed at Y-12.^{12,13} These experiments are $\text{UO}_2(\text{NO}_3)_2$ solution experiments in simple unreflected geometry. The systems are typically very dilute. The experiments included boron poisoned solutions and U-233 systems.

Table 1. KENO V.a calculated k_{eff} for experimentally critical low enriched uranium systems (last modeled in ref. 8)

| Case | Experimental description | Reference | $k_{\text{eff}} \pm \sigma$ |
|-------|--|-----------|-----------------------------|
| CAA01 | Experiment 1A. 401-4.89% U rods, 0.762-cm diam, 30-cm long, 1.3-cm pitch, H ₂ O moderated and reflected | 14 | 0.9945 \pm 0.0036 |
| CAA02 | Experiment 4B. 400-4.89% U rods, 0.762-cm diam, 30-cm long, 1.3-cm pitch, H ₂ O moderated and reflected | 14 | 0.9912 \pm 0.0030 |
| CAA03 | Experiment 11A. 240-4.89% U rods, 0.762-cm diam, 30-cm long, 1.3-cm pitch, H ₂ O moderated and reflected | 14 | 0.9924 \pm 0.0031 |
| CAA04 | Experiment 6A. 203-4.89% U rods, 0.762-cm diam, 30-cm long, 2.05-cm pitch, H ₂ O moderated and reflected | 14 | 0.9942 \pm 0.0032 |
| CAA05 | Experiment 8C. 400-4.89% U rods, 0.762-cm diam, 30-cm long, 2.05-cm pitch, H ₂ O moderated and reflected | 14 | 0.9839 \pm 0.0034 |
| CAA06 | Experiment 14A. 398-4.89% U rods, 0.762-cm diam, 30-cm long, 1.3-cm pitch, H ₂ O moderated, H ₂ O top reflector, Plexiglas bottom reflector, Pb reflected 1 face | 14 | 0.9957 \pm 0.0036 |
| CAA07 | Experiment 23B. 400-4.89% U rods, 0.762-cm diam, 30-cm long, 1.3-cm pitch, H ₂ O moderated, H ₂ O top reflector, Plexiglas bottom reflector, Pb reflected 4 faces | 14 | 0.9778 \pm 0.0036 |
| CAA08 | Experiment 26A. 215-4.89% U rods, 0.762-cm diam, 30-cm long, 1.3-cm pitch, H ₂ O moderated, H ₂ O top reflector, Plexiglas bottom reflector, Pb reflected 4 faces | 14 | 0.9966 \pm 0.0030 |
| CAA09 | Experiment 28A. 255-4.89% U rods, 0.762-cm diam, 30-cm long, 1.3-cm pitch, H ₂ O moderated, H ₂ O top reflector, Plexiglas bottom reflector, Pb reflected 4 faces, SS in center | 14 | 0.9950 \pm 0.0029 |
| CAA10 | Experiment 30C. 494-4.89% U rods, 0.762-cm diam, 30-cm long, 1.3-cm pitch, H ₂ O moderated, H ₂ O to reflector, Plexiglas bottom reflector, Pb reflected 4 faces, boral in row 6 | 14 | 1.0010 \pm 0.0032 |
| CAA11 | Experiment 31C. 494-4.89% U rods, 0.762-cm diam, 30-cm long, 1.3-cm pitch, H ₂ O moderated, H ₂ O top reflector, Plexiglas bottom reflector, Pb reflected 4 faces, Cd in row 6 | 14 | 0.9921 \pm 0.0033 |
| CAA12 | Experiment 32S. 11 x 12 array of 4.89% U rods in ~300 g U/l UO ₂ F ₂ solution, 0.762-cm diam, 2.05-cm pitch, in 95.88-cm-diam tank | 14 | 0.9885 \pm 0.0026 |

Table 1 (continued)

| Case | Experimental description | Reference | $k_{\text{eff}} \pm \sigma$ |
|-------|--|-----------|-----------------------------|
| CAA13 | Experiment 33S. 9 x 10 array of 4.89% U rods in ~300 g U/l UO_2F_2 solution, 0.762-cm diam, 2.05-cm pitch, in 95.88-cm-diam tank | 14 | 1.0035 ± 0.0022 |
| CAA14 | Experiment 36S. 9 x 10 array of 4.89% U rods in ~300 g U/l UO_2F_2 solution, 0.762-cm diam, 2.453-cm pitch, in 95.88-cm-diam tank | 14 | 0.9921 ± 0.0025 |
| CAA15 | Experiment 40S. 6 x 7 array of 4.89% U rods in ~300 g U/l UO_2F_2 solution, 1.31-cm diam, 2.99-cm pitch, in 95.88-cm-diam tank | 14 | 0.9908 ± 0.0020 |
| CAA16 | Experiment 42S. 6 x 7 array of 4.89% U rods in ~300 g U/l UO_2F_2 solution, 1.31-cm diam, 3.40-cm pitch, in 95.88-cm-diam tank | 14 | 0.9940 ± 0.0025 |
| CAA17 | Experiment 44S. 6 x 7 array of 4.89% U rods in ~300 g U/l UO_2F_2 solution, 1.31-cm diam, 3.94-cm pitch, in 95.88-cm-diam tank | 14 | 0.9884 ± 0.0029 |
| CAA18 | Experiment 45S. 6 x 7 array of 4.89% U rods in ~300 g U/l UO_2F_2 solution, 1.31-cm diam, 4.40-cm pitch, in 95.88-cm-diam tank | 14 | 0.9885 ± 0.0025 |
| CAA19 | 4.89% U_3O_8 - Stereotex blocks 55.5 g U-235/l, unreflected | 15 | 0.9875 ± 0.0035 |
| CAA20 | 4.89% U_3O_8 - Stereotex blocks 40.6 g U-235/l (H/X = 395.0), unreflected | 15 | 1.0030 ± 0.0031 |
| CAA21 | 4.89% U_3O_8 - Stereotex blocks, 22.1 g U-235/l (H/X = 757.0), unreflected | 15 | 1.0055 ± 0.0029 |
| CAA22 | 4.89% U_3O_8 - Stereotex blocks 33.3 g U-235/l (H/X = 503.6), unreflected | 15 | 1.0042 ± 0.0034 |
| CAA23 | 4.89% U_3O_8 - Stereotex blocks 64.91 g U-235/l (H/X = 199.3), paraffin top reflector, H_2O reflected bottom and sides | 15 | 0.9791 ± 0.0036 |
| CAA24 | 4.89% U_3O_8 - Stereotex blocks 56.2 g U-235/l (H/X = 244.8), paraffin top reflector, H_2O reflected bottom and sides | 15 | 0.9918 ± 0.0033 |
| CAA25 | 4.89% U_3O_8 - Stereotex blocks 40.6 g U-235/l (H/X = 396.7), paraffin top reflector, H_2O reflected bottom and sides | 15 | 1.0015 ± 0.0035 |

Table 1 (continued)

| Case | Experimental description | Reference | $k_{\text{eff}} \pm \sigma$ |
|-------|---|-----------|-----------------------------|
| CAA26 | 4.89% U_3O_8 - Stereotex blocks 22.2 g U-235/1 (H/X = 756.5), paraffin top reflector, H_2O reflected bottom and sides | 15 | 0.9991 ± 0.0025 |
| CAA27 | 4.89% U_3O_8 - Stereotex blocks 81.1 g U-235/1 (H/X = 146.8), paraffin top reflector, H_2O reflected bottom and sides | 15 | 0.9991 ± 0.0040 |
| CAA28 | 4.89% U_3O_8 - Stereotex blocks 107.0 g U-235/1 (H/X = 82.7), paraffin top reflector, H_2O reflected bottom and sides | 15 | 0.9739 ± 0.0035 |
| CAA29 | 4.89% U_3O_8 - Stereotex blocks 33.3 g U-235/1 (H/X = 504.1), paraffin top reflector, H_2O reflected bottom and sides | 15 | 0.9938 ± 0.0031 |
| CAA30 | 4.89% UO_2F_2 solution 42.54 g U-235/1 (H/X = 524) in a 20-in.-diam SS cylinder, unreflected | 15 | 0.9861 ± 0.0032 |
| CAA31 | 4.89% UO_2F_2 solution 42.54 g U-235/1 (H/X = 524) in a 20 x 20 in. aluminum box, unreflected | 15 | 0.9936 ± 0.0032 |
| CAA32 | 4.89% UO_2F_2 solution 31.79 g U-235/1 (H/X = 735) in a 20-in.-diam SS cylinder, unreflected | 15 | 0.9936 ± 0.0028 |
| CAA33 | 4.89% UO_2F_2 solution 24.04 g U-235/1 (H/X = 1002) in a 27.3-in.-diam aluminum sphere, unreflected | 15 | 0.9949 ± 0.0027 |
| CAA34 | 4.89% UO_2F_2 solution 24.28 g U-235/1 (H/X = 991) in a 30-in.-diam aluminum cylinder, unreflected | 15 | 0.9959 ± 0.0022 |
| CAA35 | 4.89% UO_2F_2 solution 42.54 g U-235/1 (H/X = 524) in a 15-in.-diam SS cylinder, H_2O reflected | 15 | 1.0029 ± 0.0030 |
| CAA36 | 4.89% UO_2F_2 solution 42.54 g U-235/1 (H/X = 524) in a 20 x 20 in. aluminum box, H_2O reflected | 15 | 1.0106 ± 0.0026 |
| CAA37 | 4.89% UO_2F_2 solution 31.79 g U-235/1 (H/X = 735) in a 15-in.-diam SS cylinder, H_2O reflected | 15 | 0.9931 ± 0.0027 |
| CAA38 | 4.89% UO_2F_2 solution 22.11 g U-235/1 (H/X = 991) in a 27.3-in.-diam aluminum sphere, H_2O reflected | 15 | 0.9927 ± 0.0022 |
| CAA39 | 4.89% UO_2F_2 solution 24.22 g U-235/1 (H/X = 994) in a 20-in.-diam SS cylinder, H_2O reflected | 15 | 1.0001 ± 0.0025 |

Table 2. KENO V.a calculated k_{eff} for experimentally critical low enriched uranium systems (last modeled in ref. 11)

| Case | Experimental description | Reference | $k_{\text{eff}} \pm \sigma$ |
|-------|---|-----------|-----------------------------|
| CAB01 | (EBJ.1) lattice 2. 15-3.85% U rods, 7.2 in. diam x 30 in. long in square lattice, 7.2 in. center to center, 77.8 cm water height | 16 | 0.9893 ± 0.0026 |
| CAB02 | (EBJ.2X) lattice 5. 11-3.85% U rods, 7.2 in. diam x 30 in. long in square lattice, 7.95 in. center to center, 72.4 cm water height | 16 | 1.0025 ± 0.0029 |
| CAB03 | (EBJ.3X) lattice 8. 24-3.85% U rods, 7.2 in. diam x 30 in. long in square lattice, 8.70 in. center to center, 75.0 cm water height | 16 | 0.9927 ± 0.0025 |
| CAB07 | (EBJ.4) lattice 3. 16-3.85% U rods, 7.2 in. diam x 30 in. long in triangular lattice, 7.45 in. center to center, 79.3 cm water height | 16 | 0.9897 ± 0.0025 |
| CAB08 | (EBJ.5X) lattice 9. 7-3.85% U rods, 7.2 in. diam x 30 in. long in triangular lattice, 8.20 in. center to center, 53.1 cm water height | 16 | 0.9924 ± 0.0032 |
| CAB09 | (EBJ.6X) lattice 2. 11-3.85% U rods, 7.2 in. OD x 2.6 in. ID x 30 in. long in triangular lattice, 7.20 center to center, 77.2 cm water height | 16 | X* |
| CAB10 | (EBJ.8) lattice 5. 6-3.85% U rods, 7.2 in. OD x 2.6 in. ID x 30 in. long in square lattice, 7.95 in. center to center, 91.4 cm water height (2 subcritical) | 16 | 0.9998 ± 0.0024 |
| CAB11 | (EBJ.9) lattice 6. 16-3.85% U rods, 7.2 in. OD x 2.6 in. ID x 30 in. long in square lattice, 8.70 in. center to center, 49.2 cm water height | 16 | 0.9953 ± 0.0025 |
| CAB12 | (EBJ.10) lattice 14. 20-3.85% U rods, 7.2 in. OD x 2.6 in. ID x 30 in. long in square lattice, 9.07 in. center to center, 79 cm water height | 16 | 0.9943 ± 0.0028 |

Table 2 (continued)

| Case | Experimental description | Reference | $k_{\text{eff}} \pm \sigma$ |
|-------|---|-----------|-----------------------------|
| CAB13 | (EBJ.11) lattice 19. 8-3.85% U rods, 7.2 in. OD x 2.6 in. ID x 30 in. long in square lattice, 7.2 in. center to center, 72.5 cm water height | 16 | 0.9960 ± 0.0028 |
| CAB14 | (EBJ.12) lattice 3. 22-3.85% U rods, 2.5 in. diam x 30 in. long in square lattice, 2.85 in. center to center, 72.3 cm water height | 16 | 1.0093 ± 0.0026 |
| CAB15 | (EBJ.13) lattice 9. 15-3.85% U rods, 2.5 in. diam x 30 in. long in square lattice, 3.25 in. center to center, 64.8 cm water height | 16 | 0.9992 ± 0.0030 |
| CAB16 | (EBJ.14) lattice 2. 23-3.85% U rods, 2.5 in. diam x 30 in. long in square lattice 4.00 in. center to center, 68.9 cm water height | 16 | 0.9877 ± 0.0029 |

*Job failed in execution.

Table 3. KENO V.a calculated k_{eff} for experimentally critical low enriched uranium systems (last modeled in ref. 7)

| Case | Experimental description | Reference | $k_{\text{eff}} \pm \sigma$ |
|-------|--|-----------|-----------------------------|
| CAS04 | An unreflected rectangular parallelepiped of homogeneous $\text{U}(1.4)\text{F}_4$ and paraffin with an H/U-235 atomic ratio of 421.8; 93.1 cm x 93.0 cm x 123.8 cm | 17 | 0.9998 ± 0.0022 |
| CAS05 | An unreflected rectangular parallelepiped of homogeneous $\text{U}(1.4)\text{F}_4$ and paraffin with an H/U-235 atomic ratio of 421.8; 100.0 cm x 99.9 cm x 103.1 cm | 17 | 0.9989 ± 0.0026 |
| CAS06 | An unreflected rectangular parallelepiped of homogeneous $\text{U}(1.4)\text{F}_4$ and paraffin with an H/U-235 atomic ratio of 421.8; 130.7 cm x 130.6 cm x 74.2 cm | 17 | 0.9967 ± 0.0022 |
| CAS11 | A reflected rectangular parallelepiped of homogeneous $\text{U}(2)\text{F}_4$ and paraffin with an H/U-235 atomic ratio of 195.2; 56.22 cm x 56.22 cm x 112.88 cm, reflected with 15.2 cm of paraffin on top and sides and 15.2 cm of Plexiglas on the bottom | 18 | 1.0023 ± 0.0030 |
| CAS12 | An unreflected rectangular parallelepiped of homogeneous $\text{U}(2)\text{F}_4$ and paraffin with an H/U-235 atomic ratio of 195.2; 71.47 cm x 71.47 cm x 94.14 cm | 18 | 1.0096 ± 0.0026 |
| CAS13 | A reflected rectangular parallelepiped of homogeneous $\text{U}(2)\text{F}_4$ and paraffin with an H/U-235 atomic ratio of 293.9; 51.11 cm x 51.11 cm x 73.87 cm, reflected with 15.2 cm of paraffin on top | 18 | 1.0054 ± 0.0029 |
| CAS14 | An unreflected rectangular parallelepiped of homogeneous $\text{U}(2)\text{F}_4$ and paraffin with an H/U-235 atomic ratio of 293.9; 56.22 cm x 56.22 cm x 122.47 cm | 18 | 1.0028 ± 0.0027 |
| CAS15 | A reflected rectangular parallelepiped of homogeneous $\text{U}(2)\text{F}_4$ and paraffin with an H/U-235 atomic ratio of 406.3; 53.67 cm x 53.67 cm x 54.29 cm, reflected with 15.2 cm of paraffin on top and sides and 15.2 cm of Plexiglas on the bottom | 18 | 0.9967 ± 0.0024 |
| CAS16 | A reflected rectangular parallelepiped of homogeneous $\text{U}(2)\text{F}_4$ and paraffin with an H/U-235 atomic ratio of 495.9; 46.00 cm x 46.00 cm x 96.57 cm, reflected with 15.2 cm of paraffin on top and sides and 15.2 cm of Plexiglas on the bottom | 18 | 1.0000 ± 0.0026 |
| CAS17 | A reflected rectangular parallelepiped of homogeneous $\text{U}(2)\text{F}_4$ and paraffin with an H/U-235 atomic ratio of 613.6; 56.32 cm x 61.29 cm x 54.08 cm, reflected with 15.2 cm of polyethylene on top and sides and 15.2 cm of Plexiglas on the bottom | 18 | 0.9982 ± 0.0027 |

Table 3 (continued)

| Case | Experimental description | Reference | $k_{\text{eff}} \pm \sigma$ |
|-------|---|-----------|-----------------------------|
| CAS18 | An unreflected rectangular parallelepiped of homogeneous $U(2)F_4$ and paraffin with an H/U-235 atomic ratio of 613.6; 61.3 cm x 66.54 cm x 66.52 cm | 18 | 0.9975 ± 0.0024 |
| CAS19 | A reflected rectangular parallelepiped of homogeneous $U(2)F_4$ and paraffin with an H/U-235 atomic ratio of 971.7; 76.51 cm x 76.44 cm x 82.42 cm, reflected with 5.2 cm of polyethylene on top and sides and 15.2 cm of Plexiglas on the bottom | 18 | 0.9885 ± 0.0020 |
| CAS20 | An unreflected rectangular parallelepiped of homogeneous $U(2)F_4$ and paraffin with an H/U-235 atomic ratio of 971.7; 81.45 cm x 86.70 cm x 88.22 cm | 18 | 0.9846 ± 0.0018 |
| CAS21 | A reflected rectangular parallelepiped of homogeneous $U(3)F_4$ and paraffin with an H/U-235 atomic ratio of 133.4; 51.14 cm x 51.14 cm x 51.27 cm, reflected with 15.2 cm of paraffin on top and sides and 15.2 cm of Plexiglas on the bottom | 18 | 1.0145 ± 0.0030 |
| CAS22 | A reflected rectangular parallelepiped of homogeneous $U(3)F_4$ and paraffin with an H/U-235 atomic ratio of 133.4; 43.47 cm x 43.47 cm x 86.39 cm, reflected with 15.2 cm of paraffin on top and sides and 15.2 cm of Plexiglas on the bottom | 18 | 1.0228 ± 0.0030 |
| CAS23 | A reflected rectangular parallelepiped of homogeneous $U(3)F_4$ and paraffin with an H/U-235 atomic ratio of 133.4; 46.02 cm x 46.02 cm x 67.57 cm, reflected with 15.2 cm of paraffin on top and sides and 15.2 cm of Plexiglas on the bottom | 18 | 1.0169 ± 0.0032 |
| CAS24 | A reflected rectangular parallelepiped of homogeneous $U(3)F_4$ and paraffin with an H/U-235 atomic ratio of 133.4; 56.25 cm x 56.25 cm x 43.41 cm, reflected with 15.2 cm of paraffin on top and sides and 15.2 cm of Plexiglas on the bottom | 18 | 1.0129 ± 0.0026 |
| CAS25 | A reflected rectangular parallelepiped of homogeneous $U(3)F_4$ and paraffin with an H/U-235 atomic ratio of 133.4; 61.36 cm x 61.36 cm x 38.67 cm, reflected with 15.2 cm of paraffin on top and sides and 15.2 cm of Plexiglas on the bottom | 18 | 1.0201 ± 0.0032 |
| CAS26 | An unreflected rectangular parallelepiped of homogeneous $U(3)F_4$ and paraffin with an H/U-235 atomic ratio of 133.4; 56.47 cm x 56.47 cm x 86.64 cm | 18 | 1.0152 ± 0.0025 |

Table 3 (continued)

| Case | Experimental description | Reference | $k_{\text{eff}} \pm \sigma$ |
|-------|--|-----------|-------------------------------|
| CAS27 | An unreflected rectangular parallelepiped of homogeneous $\text{U}(3)\text{F}_4$ and paraffin with an H/U-235 atomic ratio of 133.4; 56.25 cm x 61.36 cm x 74.38 cm | 18 | 1.0187 ± 0.0030 |
| CAS28 | An unreflected rectangular parallelepiped of homogeneous $\text{U}(3)\text{F}_4$ and paraffin with an H/U-235 atomic ratio of 133.4; 61.4 cm x 61.4 cm x 66.0 cm | 18 | 1.0180 ± 0.0028 |
| CAS29 | A reflected rectangular parallelepiped of homogeneous $\text{U}(3)\text{F}_4$ and paraffin with an H/U-235 atomic ratio of 276.9; 40.81 cm x 40.80 cm x 39.49 cm, reflected with 15.2 cm of polyethylene on top and sides and 15.2 cm of Plexiglas on the bottom | 18 | 1.0131 ± 0.0030 |
| CAS30 | An unreflected rectangular parallelepiped of homogeneous $\text{U}(3)\text{F}_4$ and paraffin with an H/U-235 atomic ratio of 276.9; 40.90 cm x 40.93 cm x 116.80 cm | 18 | 1.0173 ± 0.0030 |
| CAS31 | An unreflected rectangular parallelepiped of homogeneous $\text{U}(3)\text{F}_4$ and paraffin with an H/U-235 atomic ratio of 276.9; 48.59 cm x 51.14 cm x 48.53 cm | 18 | 1.0131 ± 0.0030 |
| CAS32 | An unreflected rectangular parallelepiped of homogeneous $\text{U}(3)\text{F}_4$ and paraffin with an H/U-235 atomic ratio of 276.9; 81.71 cm x 81.66 cm x 31.34 cm | 18 | 1.0124 ± 0.0030 |
| CAS33 | A composite cadmium/steel/water side reflected stainless steel cylinder of 0.079 cm wall thickness and 19.545 cm IR filled to a height of 54.45 cm with $\text{U}(4.98)\text{O}_2\text{F}_2$ solution at an H/U-235 atomic ratio of 488 | 19 | 0.9989 ± 0.0030 |
| CAS34 | A composite 1-in. steel/water side reflected steel cylinder of 0.079 cm wall thickness and 16.51 cm IR filled to a height of 143 cm with $\text{U}(4.98)\text{O}_2\text{F}_2$ solution at an H/U-235 atomic ratio of 488 | 19 | 1.0006 ± 0.0028 stainless |
| CAS35 | An unreflected sphere of $\text{U}(4.98)\text{O}_2\text{F}_2$ with an H/U-235 atomic ratio of 490. Solution radius of 25.3873 cm and stainless steel container wall thickness of 0.0508 cm | 20 | 0.9970 ± 0.0034 |
| CAS36 | An unreflected stainless steel cylinder of 0.07874 cm wall thickness and a 19.55 cm IR filled to a height of 101.7 cm with $\text{U}(4.98)\text{O}_2\text{F}_2$ solution at an H/U-235 atomic ratio of 496 | 21 | 1.0023 ± 0.0032 |

Table 3 (continued)

| Case | Experimental description | Reference | $k_{\text{eff}} \pm \sigma$ |
|-------|---|-----------|-----------------------------|
| CAR01 | Experiment 1. 4.46% enriched U_3O_8 , H/U = 0.77, 42 fuel cans with 2.44 cm interstitial moderation, plastic reflected | 22 | 1.0081 ± 0.0034 |
| CAR02 | Experiment 2. 4.46% enriched U_3O_8 , H/U = 0.77, 43 fuel cans with 2.44 cm interstitial moderation, plastic reflected | 22 | 1.0052 ± 0.0031 |
| CAR03 | Experiment 3. 4.46% enriched U_3O_8 , H/U = 0.77, 100 fuel cans with 0.929 cm interstitial moderation, plastic reflected | 22 | 0.9876 ± 0.0030 |
| CAR04 | Experiment 13. 4.46% enriched U_3O_8 , H/U = 0.77, 40 fuel cans with 2.44 cm interstitial moderation, concrete reflected | 22 | 1.0089 ± 0.0029 |
| CAR05 | Experiment 15. 4.46% enriched U_3O_8 , H/U = 0.77, 98 fuel cans with 0.929 cm interstitial moderation, concrete reflected | 22 | 0.9998 ± 0.0027 |
| CAR06 | 4.46% enriched U_3O_8 , H/U = 0.77, driven by 93.12% enriched uranium metal sphere (29.870 kg), 120 + 4S fuel cans, plastic reflected | 23 | 0.9951 ± 0.0031 |
| CAR07 | 4.46% enriched U_3O_8 , H/U = 0.77, driven by high concentration (14.844 kg 351.18 g/l) fuel cans, plastic reflected | 23 | 0.9998 ± 0.0032 |
| CAR08 | 4.46% enriched U_3O_8 , H/U = 0.77, driven by low concentration (12.871 kg 86.42 g/l) 93.17% enriched $\text{UO}_2(\text{NO}_3)_2$, 119 + 2S fuel cans, plastic reflected | 23 | 0.9980 ± 0.0036 |
| CAR09 | 4.46% enriched U_3O_8 , H/U = 0.77, driven by low concentration (13.001 kg 86.42 g/l) 93.17% enriched $\text{UO}_2(\text{NO}_3)_2$, 119 + 2S fuel cans, plastic reflected | 23 | 0.9983 ± 0.0030 |
| CAR10 | 4.46% enriched U_3O_8 , H/U = 0.77, driven by low concentration (12.446 kg 86.42 g/l) 93.17% enriched $\text{UO}_2(\text{NO}_3)_2$, 119 + 2S fuel cans, concrete reflected | 23 | 1.0008 ± 0.0034 |
| CAR11 | Experiment A. 4.46% enriched U_3O_8 H/U = 1.25, 38 fuel cans with 2.44 cm interstitial moderation, plastic reflected | 24 | 1.0073 ± 0.0032 |
| CAR12 | Experiment B. 4.46% enriched U_3O_8 H/U = 1.25, 78 fuel cans with 0.929 cm interstitial moderation, plastic reflected | 24 | 1.0109 ± 0.0031 |

Table 3 (continued)

| Case | Experimental description | Reference | $k_{\text{eff}} \pm \sigma$ |
|-------|---|-----------|-----------------------------|
| CAR13 | Experiment C. 4.46% enriched U_3O_8 H/U = 1.25, 80 fuel cans with 0.929 cm interstitial moderation, plastic reflected | 24 | 1.0108 ± 0.0032 |
| CAR14 | 4.46% enriched U_3O_8 H/U = 1.25, driven by high concentration (12.268 kg 351.64 gU/l), 93.17% enriched $\text{UO}_2(\text{NO}_3)_2$, 119 + 2S fuel cans, plastic reflected | 24 | 0.9907 ± 0.0034 |
| CAR15 | 4.46% enriched U_3O_8 H/U = 1.25, driven by high concentration (12.400 kg 351.65 gU/l), 93.17% enriched $\text{UO}_2(\text{NO}_3)_2$, 119 + 2S fuel cans, plastic reflected | 24 | 1.0106 ± 0.0033 |
| CAR16 | 4.46% enriched U_3O_8 H/U = 1.25, driven by low concentration (10.836 kg p 86.60 gU/l), 93.17% enriched $\text{UO}_2(\text{NO}_3)_2$, 119 + 2S fuel cans, plastic reflected | 24 | 0.9978 ± 0.0036 |
| CAR17 | Experiment F. 4.46% enriched U_3O_8 H/U = 2.03, 48 fuel cans with 0.92 cm interstitial moderation, plastic reflected | 25 | 1.0069 ± 0.0033 |
| CAR18 | Experiment G. 4.46% enriched U_3O_8 H/U = 2.03, 30 fuel cans with 2.44 cm interstitial moderation, plastic reflected | 25 | 1.0005 ± 0.0030 |
| CAR19 | Experiment D. 4.46% enriched U_3O_8 H/U = 2.03, driven by 93.12% enriched uranium metal sphere (13.73 kg), 120 + 4S fuel cans, plastic reflected | 25 | 1.0097 ± 0.0032 |
| CAR20 | Experiment E. 4.46% enriched U_3O_8 H/U = 2.03, driven by 93.12% enriched hollow uranium metal sphere (12.786 kg), 120 + 4S fuel cans, plastic reflected | 25 | 0.9911 ± 0.0031 |

Table 4. KENO V.a calculated k_{eff} for experimentally critical highly enriched uranium systems (last modeled in ref. 8)

| Case | Experimental description | Reference | $k_{\text{eff}} \pm \sigma$ |
|-------|--|-----------|-----------------------------|
| CAA01 | U(93.2)O ₂ F ₂ solution sphere H/X = 1112, unreflected | 26 | 1.0096 ± 0.0026 |
| CAA02 | U(93.2)O ₂ F ₂ solution sphere H/X = 1393 unreflected | 26 | 1.0036 ± 0.0023 |
| CAA03 | U(93.2)O ₂ (NO ₃) ₂ solution sphere H/X = 1379, unreflected | 26 | 0.9998 ± 0.0023 |
| CAA04 | U(93.2)O ₂ F ₂ solution sphere H/X = 76.1, H ₂ O reflected | 26 | 1.0071 ± 0.0039 |
| CAA05 | U(93.2)O ₂ F ₂ solution sphere H/X = 126.5, H ₂ O reflected | 26 | 0.9971 ± 0.0046 |
| CAA06 | U(93.2)O ₂ F ₂ solution sphere H/X = 1270, H ₂ O reflected | 26 | 0.9964 ± 0.0023 |
| CAA07 | U(93.2)O ₂ F ₂ solution sphere H/X = 268.8, H ₂ O reflected | 27 | 1.0097 ± 0.0043 |
| CAA08 | U(93.2)O ₂ F ₂ solution sphere H/X = 515.1, H ₂ O reflected | 27 | 1.0212 ± 0.0033 |
| CAA09 | U(93.2)O ₂ F ₂ solution sphere H/X = 203.5 unreflected | 27 | 0.9991 ± 0.0039 |
| CAA10 | U(93.2)O ₂ F ₂ solution sphere H/X = 239.3, H ₂ O reflected | 27 | 1.0164 ± 0.0042 |
| CAA11 | U(93.2)O ₂ F ₂ solution sphere H/X = 468.2, H ₂ O reflected | 27 | 1.0351 ± 0.0039 |
| CAA12 | U(93.2)O ₂ (NO ₃) ₂ solution 142.92 g U/l, 28.01 cm diam cylinder, unreflected | 28 | 1.0090 ± 0.0039 |
| CAA13 | U(93.2)O ₂ (NO ₃) ₂ solution 357.71 g U/l, 28.01 cm diam cylinder, unreflected | 28 | 1.0060 ± 0.0035 |
| CAA14 | U(93.2)O ₂ (NO ₃) ₂ solution 54.89 g U/l, 33.01 cm diam cylinder, unreflected | 28 | 1.0119 ± 0.0042 |
| CAA15 | U(93.2)O ₂ (NO ₃) ₂ solution 137.4 g U/l, 33.01 cm diam cylinder, unreflected | 28 | 1.0027 ± 0.0046 |

Table 4 (continued)

| Case | Experimental description | Reference | $k_{\text{eff}} \pm \sigma$ |
|-------|--|-----------|-----------------------------|
| CAA16 | U(93.2)O ₂ (NO ₃) ₂ solution 357.71 g U/l, 33.01 cm diam cylinder, unreflected | 28 | 1.0024 ± 0.0045 |
| CAA17 | U(93.2)O ₂ (NO ₃) ₂ solution 144.38 g U/l, 28.01 cm diam cylinder, concrete reflected | 28 | 1.0106 ± 0.0041 |
| CAA18 | U(93.2)O ₂ (NO ₃) ₂ solution 334.77 g U/l, 28.01 cm diam cylinder, concrete reflected | 28 | 1.0145 ± 0.0044 |
| CAA19 | U(93.2)O ₂ (NO ₃) ₂ solution 144.38 g U/l, 33.01 cm diam cylinder, concrete reflected | 28 | 1.0056 ± 0.0043 |
| CAA20 | U(93.2)O ₂ (NO ₃) ₂ solution 334.77 g U/l, 33.01 cm diam cylinder, concrete reflected | 28 | 1.0037 ± 0.0044 |
| CAA21 | U(93.2)O ₂ (NO ₃) ₂ solution 144.38 g U/l, 28.01 cm diam cylinder, concrete reflected | 28 | 1.0094 ± 0.0040 |
| CAA22 | U(93.2)O ₂ (NO ₃) ₂ solution 334.77 g U/l, 33.01 cm diam cylinder, concrete reflected | 28 | 1.0092 ± 0.0037 |
| CAA23 | U(93.2)O ₂ (NO ₃) ₂ solution 147.66 g U/l, 28.01 cm diam cylinder, Plexiglas reflected | 28 | 1.0085 ± 0.0040 |
| CAA24 | U(93.2) solution 345.33 g U/l, 28.01 cm diam cylinder, Plexiglas reflected | 28 | 1.0113 ± 0.0047 |
| CAA25 | U(93.2)O ₂ (NO ₃) ₂ solution 147.66 g U/l, 33.01 cm diam cylinder, Plexiglas reflected | 28 | 0.9947 ± 0.0041 |
| CAA26 | U(93.2)O ₂ (NO ₃) ₂ solution 345.33 g U/l, 33.01 cm diam cylinder, Plexiglas reflected | 28 | 1.0033 ± 0.0040 |
| CAA27 | U(93.2)O ₂ (NO ₃) ₂ solution 147.66 g U/l, 28.01 cm diam cylinder, Plexiglas reflected | 28 | 1.0157 ± 0.0034 |

Table 4 (continued)

| Case | Experimental description | Reference | $k_{\text{eff}} \pm \sigma$ |
|-------|---|-----------|-----------------------------|
| CAA28 | U(93.22)O ₂ (NO ₃) ₂ solution 345.33 g U/l, 33.01 cm diam cylinder, Plexiglas reflected | 28 | 1.0141 ± 0.0043 |
| CAA29 | U(93.22)O ₂ (NO ₃) ₂ solution 67.28 g U/l, 21.12 cm diam cylinder in a 4 x 4 array, concrete reflected | 28 | 1.0046 ± 0.0033 |
| CAA30 | U(93.12)O ₂ (NO ₃) ₂ solution 364.11 g U/l, 21.12 cm diam cylinder in a 4 x 4 array, concrete reflected | 28 | 1.0061 ± 0.0041 |
| CAA31 | U(93.2)O ₂ (NO ₃) ₂ solution 83.49 g U/l, 16.12 cm diam cylinder in a 4 x 4 array, concrete reflected | 28 | 1.0119 ± 0.0035 |
| CAA32 | U(93.2)O ₂ (NO ₃) ₂ solution 359.55 g U/l, 16.12 c diam cylinder in a 4 x 4 array, concrete reflected | 28 | 1.0056 ± 0.0041 |
| CAA33 | U(93.2)O ₂ (NO ₃) ₂ solution 76.09 g U/l, 21.12 cm diam cylinder in a 2 x 2 array, concrete reflected | 28 | 1.0098 ± 0.0033 |
| CAA34 | U(93.2)O ₂ (NO ₃) ₂ solution 364.11 g U/l, 21.2 cm diam cylinder in a 2 x 2 array, concrete reflected | 28 | 1.0014 ± 0.0038 |
| CAA35 | U(93.2)O ₂ (NO ₃) ₂ solution 359.55 g U/l, 16.12 cm diam cylinder in a 2 x 2 array, concrete reflected | 28 | 1.0129 ± 0.0045 |
| CAA36 | U(93.2)O ₂ (NO ₃) ₂ solution 359.55 g U/l, 16.12 cm diam cylinder in a 2 x 4 array, concrete reflected | 28 | 1.0099 ± 0.0039 |
| CAA37 | U(93.2)O ₂ (NO ₃) ₂ solution 60.32 g U/l, 21.12 cm diam cylinder in a 4 x 4 array, Plexiglas reflected | 28 | 1.0000 ± 0.0034 |
| CAA38 | U(93.2)O ₂ (NO ₃) ₂ solution 355.94 g U/l, 21.12 cm diam cylinder in a 4 x 4 array, Plexiglas reflected | 28 | 0.9961 ± 0.0038 |
| CAA39 | U(93.2)O ₂ (NO ₃) ₂ solution 60.32 g U/l, 16.12 cm diam cylinder in a 4 x 4 array, Plexiglas reflected | 28 | 1.0045 ± 0.0034 |

Table 4 (continued)

| Case | Experimental description | Reference | $k_{\text{eff}} \pm \sigma$ |
|-------|---|-----------|-----------------------------|
| CAA40 | U(93.2)O ₂ (NO ₃) ₂ solution 355.94 g U/l, 16.12 cm diam cylinder in a 4 x 4 array, Plexiglas reflected | 28 | 0.9985 ± 0.0039 |
| CAA41 | U(93.2)O ₂ (NO ₃) ₂ solution 60.32 g U/l, 21.12 cm diam cylinder in a 2 x 2 array, Plexiglas reflected | 28 | 0.9985 ± 0.0040 |
| CAA42 | U(93.2)O ₂ (NO ₃) ₂ solution 355.94 g U/l, 21.12 cm diam cylinder in a 2 x 2 array, Plexiglas reflected | 28 | 1.0041 ± 0.0036 |
| CAA43 | U(93.2)O ₂ (NO ₃) ₂ solution 355.94 g U/l, 16.12 cm diam cylinder in a 3 x 2 array, Plexiglas reflected | 28 | 0.9982 ± 0.0038 |

Table 5. KENO V.a calculated k_{eff} for experimentally critical highly enriched uranium systems (last modeled in ref. 6)

| Case | Experimental description | Reference | $k_{\text{eff}} \pm \sigma$ |
|-------|--|-----------|-----------------------------|
| CAS01 | Y-12 validation case A-1. 93.8% U metal sphere, unreflected (GODIVA) | 29 | 1.0004 ± 0.0027 |
| CAS04 | Y-12 validation case A-2. 93.2% U-Mo alloy cylinder annulus, unreflected | 30 | 1.0067 ± 0.0028 |
| CAS05 | Y-12 validation case A-3. 93.2% UO_2F_2 solution, 19.992 g U/l, in Al sphere, unreflected | 26 | 1.0023 ± 0.0027 |
| CAS06 | Y-12 validation case A-4. 93.18% $\text{UO}_2(\text{NO}_3)_2$ solution, 20.12 g U/l, in Al sphere, unreflected | 31 | 1.0012 ± 0.0022 |
| CAS07 | Y-12 validation case A-5. 93.5% U metal hemispherical shell, H_2O reflected | 32 | 1.0042 ± 0.0030 |
| CAS08 | Y-12 validation case A-6. 93.2% U metal cylinder annulus, graphite reflected | 33 | 1.0124 ± 0.0031 |
| CAS09 | Y-12 validation case A-7. 94% U metal cuboid, natural U reflected | 32 | 1.0027 ± 0.0025 |
| CAS10 | Y-12 validation case A-8. 93.1% U metal hemispherical shell, oil reflected | 34 | 1.0114 ± 0.0034 |
| CAS11 | Y-12 validation case A-9. 93.1% U metal hemispherical shell, steel center and oil reflected | 34 | 0.9977 ± 0.0035 |
| CAS02 | Y-12 validation case A-10. 97.67% U metal sphere, H_2O reflected | 35 | 0.9995 ± 0.0031 |
| CAS03 | Y-12 validation case A-11. 93.172% $\text{UO}_2(\text{NO}_3)_2$ solution, 346.7 g U/l, in SS cylinder, unreflected | 28 | 1.0029 ± 0.0044 |
| CAS12 | Y-12 validation case B-1. 93.2% U metal cylinder annulus, unreflected, smaller U cylinder in hole touching one wall | 36 | 1.0004 ± 0.0031 |
| CAS22 | Y-12 validation case B-2. 93.2% U metal cylinder annulus, unreflected, smaller U block in hole touching one wall | 36 | 1.0082 ± 0.0034 |
| CAS23 | Y-12 validation case B-3. 93.2% U metal, unreflected cylinders and cuboids in approximate circular arrangement, cylinder, cuboid, and hemisphere stack in center | 36 | 0.9959 ± 0.0030 |

Table 5 (continued)

| Case | Experimental description | Reference | $k_{\text{eff}} \pm \sigma$ |
|-------|--|-----------|-----------------------------|
| CAS24 | Y-12 validation case B-4. 93.2% U metal cylinders, 4 x 4 x 4 array, unreflected | 37 | 0.9928 ± 0.0033 |
| CAS25 | Y-12 validation case B-5. 93.2% U metal cylinders, 2 x 2 x 2 array, each unit in the array is a smaller cylinder capped on each end by a larger cylinder, unreflected | 37 | 1.0079 ± 0.0030 |
| CAS26 | Y-12 validation case B-6. 93.2% U metal cylinders, 2 x 2 x 2 array, paraffin reflected | 37 | 1.0011 ± 0.0033 |
| CAS27 | Y-12 validation case B-7. 93.2% U metal cylinders, 2 x 2 x 2 array, each unit in the array is a smaller cylinder capped on each end by a larger cylinder, paraffin reflected | 37 | 1.0083 ± 0.0031 |
| CAS28 | Y-12 validation case B-8. 93.2% U metal cylinders each in a Plexiglas box, 2 x 2 x 2 array of these units unreflected | 37 | 1.0102 ± 0.0037 |
| CAS29 | Y-12 validation case B-9. 92.6% $\text{UO}_2(\text{NO}_3)_2$ solution, 415 g U/l, in Plexiglas cylinders, 3 x 3 x 3 array, unreflected (see also problem U4B271F) | 38 | 0.9872 ± 0.0041 |
| CAS13 | Y-12 validation case B-10. 92.6% $\text{UO}_2(\text{NO}_3)_2$ solution, 63.3 g U/l, in Plexiglas cylinders, 3 x 3 x 3 array, unreflected (see also problem U6B271F) | 38 | 0.9854 ± 0.0035 |
| CAS14 | Y-12 validation case B-11. 93.2% $\text{UO}_2(\text{NO}_3)_2$ solution, 505 g U/l, in SS cylinders, 4 x 4 array, standing in a solution slab, Plexiglas reflected | 39 | 1.0585 ± 0.0038 |
| CAS15 | Y-12 validation case B-12. 93.2% U metal cylinders, 2 x 2 x 2 array, graphite moderated and polyethylene reflected | 40 | 1.0126 ± 0.0030 |
| CAS16 | Y-12 validation case B-13. 92.6% $\text{UO}_2(\text{NO}_3)_2$ solution, 415 g U/l, in Plexiglas cylinders, 4 x 4 x 4 array, unreflected (see also problem U4B641F) | 38 | 0.9879 ± 0.0037 |

Table 5 (continued)

| Case | Experimental description | Reference | $k_{\text{eff}} \pm \sigma$ |
|-------|--|-----------|-----------------------------|
| CAS17 | Y-12 validation case B-14. 92.6% $\text{UO}_2(\text{NO}_3)_2$ solution, 415 g U/l, in Plexiglas cylinders, 3 x 3 x 3 array, paraffin reflected (see also problem U4R27I1F) | 38 | 1.0250 ± 0.0037 |
| CAS18 | Y-12 validation case B-15. 92.6% $\text{UO}_2(\text{NO}_3)_2$ solution, 415 g U/l, in Plexiglas cylinders, 3 x 3 x 3 array, Plexiglas reflected (see also problem U4R27G1F) | 38 | 1.0010 ± 0.0045 |
| CAS19 | Y-12 validation case B-16. 93.1% $\text{UO}_2(\text{NO}_3)_2$ solution, 450.8 g U/l, in SS containers, square central column with 8 perpendicular cylindrical arms unreflected | 41,42 | 1.0329 ± 0.0046 |
| CAS20 | Y-12 validation case B-17. 93.17% $\text{UO}_2(\text{NO}_3)_2$ solution, 355.9 g U/l, in Al cylinders, 4 x 4 array, Plexiglas reflected | 28 | 1.03654 ± 0.0037 |
| CAS21 | Y-12 validation case B-18. 93.17% $\text{UO}_2(\text{NO}_3)_2$ solution, 364.1 g U/l, in Al cylinders, 4 x 4 array, concrete reflected | 28 | 1.0239 ± 0.0043 |
| CAS30 | Problem S333SPO. 93.2% UO_2F_2 solution, 81.8 g U/l, in Al slabs, 3 7.62 cm slabs in 3 x 1 array, 0 cm separation, unreflected, cylindrical tank, floor and walls in experiment room included | 43 | 0.9978 ± 0.0038 |
| CAS32 | Problem S333SP1. 93.2% UO_2F_2 solution, 81.8 g U/l, in Al slabs, 3 7.62 cm slabs in 3 x 1 array, 2.54 cm separation, unreflected, cylindrical tank, floor, and walls in experiment room included | 43 | 0.9805 ± 0.0039 |
| CAS34 | Problem S333SP3. 93.2% UO_2F_2 solution, 81.8 g U/l, in Al slabs, 3 7.62 cm slabs in 3 x 1 array, 7.62 cm separation, unreflected, cylindrical tank, floor, and walls in experiment room included | 43 | 0.9803 ± 0.0039 |
| CAS36 | Problem S333SP4. 93.2% UO_2F_2 solution, 81.8 g U/l, in Al slabs, 3 7.62 cm slabs in 3 x 1 array, 11.43 cm separation, unreflected, cylindrical tank, floor, and walls in experiment room included | 43 | 0.9933 ± 0.0035 |

Table 5 (continued)

| Case | Experimental description | Reference | $k_{\text{eff}} \pm \sigma$ |
|-------|--|-----------|-----------------------------|
| CAS38 | Problem S333SP5. 93.2% UO_2F_2 solution, 81.8 g U/l, in Al slabs, 3 7.62 cm slabs in 3 x 1 array, 13.97 cm separation, unreflected, cylindrical tank, floor, and walls in experiment room included | 43 | 0.9881 ± 0.0035 |
| CAS40 | Problem S333SP6. 93.2% UO_2F_2 solution, 81.8 g U/l, in Al slabs, 3 7.62 cm slabs in 3 x 1 array, 15.24 cm separation, unreflected, cylindrical tank, floor, and walls in experiment room included | 43 | 0.9824 ± 0.0041 |
| CAS31 | Problem S333SPOR. 93.2% UO_2F_2 solution, 81.8 g U/l, in Al slabs, 3 7.62 cm slabs in 3 x 1 array, 0 cm separation, H_2O reflected | 43 | 0.9949 ± 0.0035 |
| CAS33 | Problem S333SP1R. 93.2% UO_2F_2 solution, 81.8 g U/l, in Al slabs, 3 7.62 cm slabs in 3 x 1 array, 2.54 cm separation, H_2O reflected | 43 | 0.9995 ± 0.0039 |
| CAS35 | Problem S333SP3R. 93.2% UO_2F_2 solution, 81.8 g U/l, in Al slabs, 3 7.62 cm slabs in 3 x 1 array, 7.62 cm separation, H_2O reflected | 43 | 0.9906 ± 0.0036 |
| CAS37 | Problem S333SP4R. 93.2% UO_2F_2 solution, 81.8 g U/l, in Al slabs, 3 7.62 cm slabs in 3 x 1 array, 11.43 cm separation, H_2O reflected | 43 | 1.0030 ± 0.0031 |
| CAS39 | Problem S333SP5R. 93.2% UO_2F_2 solution, 81.8 g U/l, in Al slabs, 3 7.62 cm slabs in 3 x 1 array, 13.97 cm separation, H_2O reflected | 43 | 0.9952 ± 0.0035 |
| CAS42 | Problem S36SP2. 93.2% UO_2F_2 solution, 81.8 g U/l in Al slabs, 7.62 cm and 14.834 cm slabs in 2 x 1 array, 5.08 cm separation, unreflected | 43 | 0.9916 ± 0.0037 |
| CAS41 | Problem S36SP15. 93.2% UO_2F_2 solution, 81.8 g U/l in Al slabs, 7.62 cm and 14.834 cm slabs in 2 x 1 array, 38.1 cm separation, unreflected | 43 | 0.9767 ± 0.0038 |

Table 5 (continued)

| Case | Experimental description | Reference | $k_{\text{eff}} \pm \sigma$ |
|-------|---|-----------|-----------------------------|
| CAS43 | Problem S36SP30. 93.2% UO_2F_2 solution, 81.8 g U/l in Al slabs, 7.62 cm and 14.834 cm slabs in 2 x 1 array, 76.2 cm separation, unreflected | 43 | 0.9835 ± 0.0037 |
| CAS44 | Problem S36SP48. 93.2% UO_2F_2 solution, 81.8 g U/l in Al slabs, 7.62 cm and 14.834 cm slabs in 2 x 1 array, 121.92 cm separation, unreflected | 43 | 0.9757 ± 0.0035 |
| CAS45 | Problem S363SPO. 93.2% UO_2F_2 solution, 81.8 g U/l, in Al slabs, 7.62 cm, 14.834 cm, and 7.62 cm slabs in 3 x 1 array, 0 cm separation, unreflected | 43 | 0.9871 ± 0.0040 |
| CAS46 | Problem S363SP10. 93.2% UO_2F_2 solution, 81.8 g U/l, in Al slabs, 7.62 cm, 14.834 cm, and 7.62 cm slabs in 3 x 1 array, 25.4 cm separation, unreflected | 43 | 0.9832 ± 0.0040 |
| CAS47 | Problem S363SP20. 93.2% UO_2F_2 solution, 81.8 g U/l, in Al slabs, 7.62 cm, 14.834 cm, and 7.62 cm slabs in 3 x 1 array, 50.8 cm separation, unreflected | 43 | 0.9819 ± 0.0037 |
| CAS48 | Problem S363SP32. 93.2% UO_2F_2 solution, 81.8 g U/l, in Al slabs, 7.62 cm, 14.834 cm, and 7.62 cm slabs in 3 x 1 array, 81.28 cm separation, unreflected | 43 | 0.9813 ± 0.0039 |
| CAS52 | Problem S63SP6. 93.2% UO_2F_2 solution, 81.8 g U/l, in Al slabs. One slab is made up from two 7.62 cm slabs snugly fit together, the other is 7.62 cm, 2 x 1 array, 15.24 cm separation, unreflected | 43 | 0.9852 ± 0.0038 |
| CAS49 | Problem S63SP12. 93.2% UO_2F_2 solution, 81.8 g U/l, in Al slabs. One slab is made up from two 7.62 cm slabs snugly fit together, the other is 7.62 cm, 2 x 1 array, 30.48 cm separation, unreflected | 43 | 0.9831 ± 0.0045 |

Table 5 (continued)

| Case | Experimental description | Reference | $k_{\text{eff}} \pm \sigma$ |
|-------|--|-----------|-----------------------------|
| CAS50 | Problem S63SP18. 93.2% UO_2F_2 solution, 81.8 g U/l, in Al slabs. One slab is made up from two 7.62 cm slabs snugly fit together, the other is 7.62 cm, 2 x 1 array, 45.72 cm separation, unreflected | 43 | 0.9814 ± 0.0038 |
| CAS51 | Problem S63SP30. 93.2% UO_2F_2 solution, 81.8 g U/l, in Al slabs. One slab is made up from two 7.62 cm slabs snugly fit together, the other is 7.62 cm, 2 x 1 array, 76.2 cm separation, unreflected | 43 | 0.9791 ± 0.0036 |
| CAS54 | Problem S66SP2. 93.2% UO_2F_2 solution, 81.8 g U/l, in Al slabs. One slab is 14.834 cm, and the other is made up from two 7.62 cm slabs snugly fit together, 2 x 1 array, 5.08 cm separation, unreflected | 43 | 0.9831 ± 0.0034 |
| CAS58 | Problem S66SP2. 93.2% UO_2F_2 solution, 81.8 g U/l, in Al slabs. One slab is 14.834 cm, and the other is made up from two 7.62 cm slabs snugly fit together, 2 x 1 array, 15.24 cm separation, unreflected | 43 | 0.9824 ± 0.0037 |
| CAS53 | Problem S66SP15. 93.2% UO_2F_2 solution, 81.8 g U/l, in Al slabs. One slab is 14.834 cm, and the other is made up from two 7.62 cm slabs snugly fit together, 2 x 1 array, 38.1 cm separation, unreflected | 43 | 0.9884 ± 0.0039 |
| CAS55 | Problem S66SP20. 93.2% UO_2F_2 solution, 81.8 g U/l, in Al slabs. One slab is 14.834 cm, and the other is made up from two 7.62 cm slabs snugly fit together, 2 x 1 array, 50.8 cm separation, unreflected | 43 | 0.9876 ± 0.0038 |

Table 5 (continued)

| Case | Experimental description | Reference | $k_{\text{eff}} \pm \sigma$ |
|-------|--|-----------|-----------------------------|
| CAS56 | Problem S66SP30. 93.2% UO_2F_2 solution, 81.8 g U/l, in Al slabs. One slab is 14.834 cm, and the other is made up from two 7.62 cm slabs snugly fit together, 2 x 1 array, 76.2 cm separation, unreflected | 43 | 0.9869 ± 0.0042 |
| CAS57 | Problem S66SP48. 93.2% UO_2F_2 solution, 81.8 g U/l, in Al slabs. One slab is 14.834 cm, and the other is made up from two 7.62 cm slabs snugly fit together, 2 x 1 array, 121.92 cm separation, unreflected | 43 | 0.9864 ± 0.0041 |
| CAS59 | Problem S66SP66. 93.2% UO_2F_2 solution, 81.8 g U/l, in Al slabs. One slab is 14.834 cm, and the other is made up from two 7.62 cm slabs snugly fit together, 2 x 1 array, 167.64 cm separation, unreflected | 43 | 0.9836 ± 0.0036 |
| CAS91 | Problem U6B271F. 92.6% $\text{UO}_2(\text{NO}_3)_2$ solution, 63.3 g U/l, in Plexiglas cylinders, 3 x 3 x 3 array, unreflected, walls, floor, and tank in experiment room included | 38 | 1.0052 ± 0.0036 |
| CAS60 | Problem U2B271F. 92.6% $\text{UO}_2(\text{NO}_3)_2$ solution, 279 g U/l, in Plexiglas cylinders, 3 x 3 x 3 array, unreflected, walls, floor, and tank in experiment room included | 38 | 0.9998 ± 0.0036 |
| CAS61 | Problem U2B81F. 92.6% $\text{UO}_2(\text{NO}_3)_2$ solution, 279 g U/l, in Plexiglas cylinders, 2 x 2 x 2 array, unreflected, walls, floor, and tank in experiment room included | 38 | 1.0005 ± 0.0038 |
| CAS62 | Problem U4B1251F. 92.6% $\text{UO}_2(\text{NO}_3)_2$ solution, 415 g U/l, in Plexiglas cylinders, 5 x 5 x 5 array, unreflected, walls, floor, and tank in experiment room included | 38 | 0.9934 ± 0.0039 |

Table 5 (continued)

| Case | Experimental description | Reference | $k_{\text{eff}} \pm \sigma$ |
|-------|---|-----------|-----------------------------|
| CAS64 | Problem U4B641F. 92.6% $\text{UO}_2(\text{NO}_3)_2$ solution, 415 g U/l, in Plexiglas cylinders, 4 x 4 x 4 array, unreflected, walls, floor, and tank in experiment room included | 38 | 0.9963 ± 0.0038 |
| CAS63 | Problem U4B271F. 92.6% $\text{UO}_2(\text{NO}_3)_2$ solution, 415 g U/l, in Plexiglas cylinders, 3 x 3 x 3 array, unreflected, walls, floor, and tank in experiment room included | 38 | 1.0050 ± 0.0044 |
| CAS65 | Problem U4B81F. 92.6% $\text{UO}_2(\text{NO}_3)_2$ solution, 415 g U/l, in Plexiglas cylinders, 2 x 2 x 2 array, unreflected, walls, floor, and tank in experiment room included | 38 | 1.0081 ± 0.0039 |
| CAS90 | Problem U4U2B27. 92.6% $\text{UO}_2(\text{NO}_3)_2$ solution, 415 g U/l, in Plexiglas cylinders, 3 x 3 x 3 array, unreflected, 279 g U/l in 5 central units, walls, floor, and tank in experiment room included | 38 | 0.9977 ± 0.0042 |
| CAS66 | Problem U4R27A1F. 92.6% $\text{UO}_2(\text{NO}_3)_2$ solution, 415 g U/l, in Plexiglas cylinders, 3 x 3 x 3 array, reflected, 15.24 cm paraffin on bottom, 1.27 cm Plexiglas on other faces | 38 | 1.002 ± 0.0037 |
| CAS67 | Problem U4R27B1F. 92.6% $\text{UO}_2(\text{NO}_3)_2$ solution, 415 g U/l, in Plexiglas cylinders, 3 x 3 x 3 array, reflected, 15.24 cm paraffin on bottom, 2.54 cm Plexiglas on other faces | 38 | 1.0217 ± 0.0038 |
| CAS68 | Problem U4R27C1F. 92.6% $\text{UO}_2(\text{NO}_3)_2$ solution, 415 g U/l, in Plexiglas cylinders, 3 x 3 x 3 array, reflected, 15.24 cm paraffin on bottom, 1.27 cm Plexiglas on other faces | 38 | 1.0170 ± 0.0042 |
| CAS69 | Problem U4R27D1F. 92.6% $\text{UO}_2(\text{NO}_3)_2$ solution, 415 g U/l, in Plexiglas cylinders, 3 x 3 x 3 array, reflected, 15.24 cm paraffin on 5 faces, 15.24 cm Plexiglas on 1 face | 38 | 1.0227 ± 0.0040 |

Table 5 (continued)

| Case | Experimental description | Reference | $k_{\text{eff}} \pm \sigma$ |
|-------|---|-----------|-----------------------------|
| CAS70 | Problem U4R27E1F. 92.6% $\text{UO}_2(\text{NO}_3)_2$ solution, 415 g U/l, in Plexiglas cylinders, 3 x 3 x 3 array, reflected, 15.24 cm paraffin on bottom, 3.81 cm paraffin on other faces | 38 | 1.0205 ± 0.0039 |
| CAS71 | Problem U4R27F1F. 92.6% $\text{UO}_2(\text{NO}_3)_2$ solution, 415 g U/l, in Plexiglas cylinders, 3 x 3 x 3 array, reflected, 15.24 cm paraffin on bottom, 7.62 cm paraffin on other faces | 38 | 1.0302 ± 0.0040 |
| CAS72 | Problem U4R27G1F. 92.6% $\text{UO}_2(\text{NO}_3)_2$ solution, 415 g U/l, in Plexiglas cylinders, 3 x 3 x 3 array, reflected, 1.27 cm Plexiglas all faces | 38 | 1.0016 ± 0.0038 |
| CAS73 | Problem U4R27H1F. 92.6% $\text{UO}_2(\text{NO}_3)_2$ solution, 415 g U/l, in Plexiglas cylinders, 3 x 3 x 3 array, reflected, 1.27 cm paraffin all faces | 38 | 1.0134 ± 0.0041 |
| CAS74 | Problem U4R27I1F. 92.6% $\text{UO}_2(\text{NO}_3)_2$ solution, 415 g U/l, in Plexiglas cylinders, 3 x 3 x 3 array, reflected, 15.24 cm paraffin all faces | 38 | 1.0172 ± 0.0035 |
| CAS75 | Problem U4R27J1F. 92.6% $\text{UO}_2(\text{NO}_3)_2$ solution, 415 g U/l, in Plexiglas cylinders, 3 x 3 x 3 array, reflected, 3.81 cm paraffin all faces | 38 | 1.0300 ± 0.0037 |
| CAS76 | Problem U4R8A1F. 92.6% $\text{UO}_2(\text{NO}_3)_2$ solution, 415 g U/l, in Plexiglas cylinders, 2 x 2 x 2 array, reflected, 15.24 cm paraffin on bottom, 1.27 cm Plexiglas on other faces | 38 | 1.0046 ± 0.0044 |
| CAS77 | Problem U4R8B1F. 92.6% $\text{UO}_2(\text{NO}_3)_2$ solution, 415 g U/l, in Plexiglas cylinders, 2 x 2 x 2 array, reflected, 15.24 cm paraffin on bottom, 11.43 cm Plexiglas on other faces | 38 | 1.0225 ± 0.0040 |

Table 5 (continued)

| Case | Experimental description | Reference | $k_{\text{eff}} \pm \sigma$ |
|-------|---|-----------|-----------------------------|
| CAS78 | Problem U4R8C1F. 92.6% $\text{UO}_2(\text{NO}_3)_2$ solution, 415 g U/l, in Plexiglas cylinders, 2 x 2 x 2 array, reflected, 15.24 cm paraffin on bottom, 15.24 cm Plexiglas on other faces | 38 | 1.0237 ± 0.0045 |
| CAS79 | Problem U4R8D1F. 92.6% $\text{UO}_2(\text{NO}_3)_2$ solution, 415 g U/l, in Plexiglas cylinders, 2 x 2 x 2 array, reflected, 15.24 cm paraffin on bottom, 2.54 cm Plexiglas on other faces | 38 | 1.0137 ± 0.0036 |
| CAS80 | Problem U4R8E1F. 92.6% $\text{UO}_2(\text{NO}_3)_2$ solution, 415 g U/l, in Plexiglas cylinders, 2 x 2 x 2 array, reflected, 15.24 cm paraffin on bottom, 4.45 cm Plexiglas on other faces | 38 | 1.0223 ± 0.0045 |
| CAS81 | Problem U4R8F1F. 92.6% $\text{UO}_2(\text{NO}_3)_2$ solution, 415 g U/l, in Plexiglas cylinders, 2 x 2 x 2 array, reflected, 15.24 cm paraffin on bottom, 6.35 cm Plexiglas on other faces | 38 | 1.0197 ± 0.0037 |
| CAS82 | Problem U4R8G1F. 92.6% $\text{UO}_2(\text{NO}_3)_2$ solution, 415 g U/l, in Plexiglas cylinders, 2 x 2 x 2 array, reflected, 15.24 cm paraffin on bottom, 1.27 cm Plexiglas on other faces | 38 | 1.0195 ± 0.0038 |
| CAS83 | Problem U4R8H1F. 92.6% $\text{UO}_2(\text{NO}_3)_2$ solution, 415 g U/l, in Plexiglas cylinders, 2 x 2 x 2 array, reflected, 15.24 cm paraffin on bottom, 3.81 cm Plexiglas on other faces | 38 | 1.0225 ± 0.0039 |
| CAS84 | Problem U4R8I1F. 92.6% $\text{UO}_2(\text{NO}_3)_2$ solution, 415 g U/l, in Plexiglas cylinders, 2 x 2 x 2 array, reflected, 15.24 cm paraffin on bottom, 7.62 cm Plexiglas on other faces | 38 | 1.0247 ± 0.0041 |

Table 5 (continued)

| Case | Experimental description | Reference | $k_{\text{eff}} \pm \sigma$ |
|-------|--|-----------|-----------------------------|
| CAS85 | Problem U4R8J1F. 92.6% $\text{UO}_2(\text{NO}_3)_2$ solution, 415 g U/l, in Plexiglas cylinders, 2 x 2 x 2 array, reflected, 1.27 cm Plexiglas all faces | 38 | 1.0175 ± 0.0046 |
| CAS86 | Problem U4R8K1F. 92.6% $\text{UO}_2(\text{NO}_3)_2$ solution, 415 g U/l, in Plexiglas cylinders, 2 x 2 x 2 array, reflected, 1.27 cm paraffin all faces | 38 | 1.01675 ± 0.0042 |
| CAS87 | Problem U4R8L1F. 92.6% $\text{UO}_2(\text{NO}_3)_2$ solution, 415 g U/l, in Plexiglas cylinders, 2 x 2 x 2 array, reflected, 15.24 cm paraffin all faces | 38 | 1.0177 ± 0.0042 |
| CAS88 | Problem U4R8M1F. 92.6% $\text{UO}_2(\text{NO}_3)_2$ solution, 415 g U/l, in Plexiglas cylinders, 2 x 2 x 2 array, reflected, 3.81 cm paraffin all faces | 38 | 1.0177 ± 0.0041 |
| CAS89 | Problem U4R8N1F. 92.6% $\text{UO}_2(\text{NO}_3)_2$ solution, 415 g U/l, in Plexiglas cylinders, 2 x 2 x 2 array, reflected, 7.62 cm paraffin all faces | 38 | 1.0169 ± 0.0046 |

Table 6. KENO V.a calculated k_{eff} for experimentally critical highly enriched uranium systems

| Case | Experimental description | Reference | $k_{\text{eff}} \pm \sigma$ |
|-------|--|-----------|-----------------------------|
| CAS01 | Experiment 1. U(93.2) O ₂ (NO ₃) ₂ H/X=1378 in 27.24-in. diam sphere | 12,13 | 0.9979 ± 0.0022 |
| CAS02 | Experiment 2. U(93.2) O ₂ (NO ₃) ₂ H/X=1177, B poisoned, in 27.24-in. diam sphere | 12,13 | 0.9960 ± 0.0023 |
| CAS03 | Experiment 3. U(93.2) O ₂ (NO ₃) ₂ H/X=1033, B poisoned, in 27.24-in. diam sphere | 12,13 | 0.9920 ± 0.0027 |
| CAS04 | Experiment 4. U(93.2) O ₂ (NO ₃) ₂ H/X=972, B poisoned, in 27.24-in. diam sphere | 12,13 | 1.0020 ± 0.0024 |
| CAS05 | Experiment 5. U-233 O ₂ (NO ₃) ₂ H/X=1533, in 27.24-in. diam sphere | 12,13 | 1.0086 ± 0.0022 |
| CAS06 | Experiment 6. U-233 O ₂ (NO ₃) ₂ H/X=1470, B poisoned, in 27.24-in. diam sphere | 12,13 | 1.0079 ± 0.0025 |
| CAS07 | Experiment 7. U-233 O ₂ (NO ₃) ₂ H/X=1417, B poisoned, in 27.24-in. diam sphere | 12,13 | 1.0045 ± 0.0023 |
| CAS08 | Experiment 8. U-233 O ₂ (NO ₃) ₂ H/X=1368, B poisoned, in 27.24-in. diam sphere | 12,13 | 1.0065 ± 0.0023 |
| CAS09 | Experiment 9. U-233 O ₂ (NO ₃) ₂ H/X=1835, in 48.04-in. diam sphere | 12,13 | 1.0084 ± 0.0023 |
| CAS10 | Experiment 10. U(93.2)O ₂ (NO ₃) ₂ H/X=1835, in 48.04-in. diam sphere | 12,13 | 0.9979 ± 0.0017 |
| CAS11 | Experiment 11. U-233 O ₂ (NO ₃) ₂ H/X=1986, in 48.04-in. diam sphere | 12,13 | 0.9959 ± 0.0017 |
| CAS12 | Experiment 12. U(93.2) O ₂ (NO ₃) ₂ H/X=1604, in 60.92-in. diam cylinder | 12,13 | 0.9989 ± 0.0023 |
| CAS13 | Experiment 13. U(93.2) O ₂ (NO ₃) ₂ H/X=1634, in 60.92-in. diam cylinder | 12,13 | 0.9983 ± 0.0022 |
| CAS14 | Experiment 14. U(93.2) O ₂ (NO ₃) ₂ H/X=1821, in 60.92-in. diam cylinder | 12,13 | 0.9992 ± 0.0017 |

Table 6 (continued)

| Case | Experimental description | Reference | $k_{\text{eff}} \pm \sigma$ |
|-------|--|-----------|-----------------------------|
| CAS15 | Experiment 15. U(93.2) $\text{O}_2(\text{NO}_3)_2$ H/X=1905, in 60.92-in. diam cylinder | 12,13 | 0.9925 ± 0.0019 |
| CAS16 | Experiment 16. U(93.2) $\text{O}_2(\text{NO}_3)_2$ H/X=1981, in 60.92-in. diam cylinder | 12,13 | 0.9976 ± 0.0016 |
| CAS17 | Experiment 17. U-233 $\text{O}_2(\text{NO}_3)_2$ H/X=1819, in 60.92-in. diam cylinder | 12,13 | 0.9952 ± 0.0020 |
| CAS18 | Experiment 18. U-233 $\text{O}_2(\text{NO}_3)_2$ H/X=1900, in 60.92-in. diam cylinder | 12,13 | 0.9973 ± 0.0018 |
| CAS19 | Experiment 19. U-233 $\text{O}_2(\text{NO}_3)_2$ H/X=1996, in 60.92-in. diam cylinder | 12,13 | 0.9916 ± 0.0015 |
| CAS20 | Experiment 20. U-233 $\text{O}_2(\text{NO}_3)_2$ H/X=2106, in 60.92-in. diam cylinder | 12,13 | 0.9927 ± 0.0015 |
| CAS21 | Experiment 21. U(93.2) $\text{O}_2(\text{NO}_3)_2$ H/X=1955, in 107.7-in. diam cylinder | 12,13 | 0.9923 ± 0.0015 |
| CAS22 | Experiment 22. U(93.2) $\text{O}_2(\text{NO}_3)_2$ H/X=2004, in 107.7-in. diam cylinder | 12,13 | 0.9915 ± 0.0014 |
| CAS23 | Experiment 23. U(93.2) $\text{O}_2(\text{NO}_3)_2$ H/X=2052, in 107.7-in. diam cylinder | 12,13 | 0.9991 ± 0.0014 |

1.5 DISCUSSION

The experiments modeled were parameterized such that trend analysis could be performed. Table C.1 (Appendix C) is a relisting of the results of the 258 experiments which were calculated, along with the parameters which describe the experiments. Table C.1 is partitioned to correspond to Tables 1-6. Table 7 gives the average value of k_{eff} for each table of results. The mean values of k_{eff} are in excellent agreement with the experiments. The spread in data, however, indicates that there may be problems with certain types of calculations. The cause of the spread in data will be discussed more fully in Sect. 2.

Figures 1-3 are histograms showing frequency of k_{eff} , average energy group of the neutrons causing fission (average energy group), and the assay distribution for all 258 experiments. From Fig. 2 it can be seen that the majority of the calculations were for thermal systems. Figure 3 indicates that the modeled experiments did not include enrichments between 5 and 90%.

Figure 4 shows the value of calculated k_{eff} as a function of the average energy group of the neutron-causing fission.

Figure 5 is a plot of calculated k_{eff} as a function of the reference from which the experiments were modeled. In some of the cases where a number of experiments were run from the same reference, there seems to be a natural break. If all the cases had been equivalent as far as modeling and code treatment, k_{eff} should be normally distributed around a mean value. The natural break may be an indication of possible code and/or cross-section problems.

Figures 6 and 7 show the value of k_{eff} as a function of the assay for low-enriched and high-enriched experiments, respectively. In Fig. 6, the calculated k_{eff} of the 3% enriched experiments are considerably higher than those of other low-enriched experiments. Reasons for this trend are discussed in Sect. 2.

Figures 8-13 are plots of k_{eff} versus average energy group for each table of results. Closed-band tolerance limits similar to those discussed in ref. 7 have been plotted. The dashed line on these curves represents the lower tolerance limit for 99.9% of the population with a 95% confidence level.

Figure 12 was split into two portions (Figs. 12a and 12b) because of the large gap in average energy group of the neutron-causing fission between groups 12 and 20. This caused the tolerance band width to be smaller in Figs. 12a and 12b. The slope of the curve fit through the data changed considerably in Fig. 12b. Figure 12b highlights the importance of knowing the cause of bias in calculated results. If the bias were caused by a systematic code or cross-section error, then, according to Fig. 12b, systems similar to those used in the figure and with an average energy group in the range of 21 would have a tolerance limit of 0.97. However, if the bias were caused because of reporting bias, then Fig. 12b shows a false trend; and the tolerance limit is unknown.

1.6 CONCLUSIONS

The KENO V.a code accurately calculates a broad range of critical experiments. In some past validations, the average energy group of the neutron-causing fission has been used to report calculated results. There is no strong evidence that calculated results are highly correlated to the average energy group of the neutron-causing fission. In review, a substantial number of the calculations show a positive or negative bias in excess of 1-1/2% in k_{eff} . Classes of criticals which show a bias include 3% enriched green blocks, highly enriched uranyl fluoride slab arrays, and highly enriched uranyl nitrate arrays. If these biases are properly taken into account, the KENO V.a code in the Y12CSG package can be used

Table 7. Average k_{eff} by table

| Variable | Label | N | Mean | Standard Deviation | Minimum Value | Minimum Value |
|------------------|-------------|----|------------|--------------------|---------------|---------------|
| Table=1 | | | | | | |
| k_{eff} | k-effective | 39 | 0.99369744 | 0.00771453 | 0.97390000 | 1.01080000 |
| Table=2 | | | | | | |
| k_{eff} | k-effective | 12 | 0.99568333 | 0.00620349 | 0.98770000 | 1.00930000 |
| Table=3 | | | | | | |
| k_{eff} | k-effective | 49 | 1.00434082 | 0.00911375 | 0.98460000 | 1.02280000 |
| Table=4 | | | | | | |
| k_{eff} | k-effective | 43 | 1.00673721 | 0.00759245 | 0.99470000 | 1.03510000 |
| Table=5 | | | | | | |
| k_{eff} | k-effective | 91 | 1.00278132 | 0.01630369 | 0.97570000 | 1.05850000 |
| Table=6 | | | | | | |
| k_{eff} | k-effective | 23 | 0.99842609 | 0.00554061 | 0.99150000 | 1.00860000 |

FREQUENCY CHART FOR K-EFFECTIVE
INCLUDES 258 EXPERIMENTS

ORNL DWG. No. 86-15378

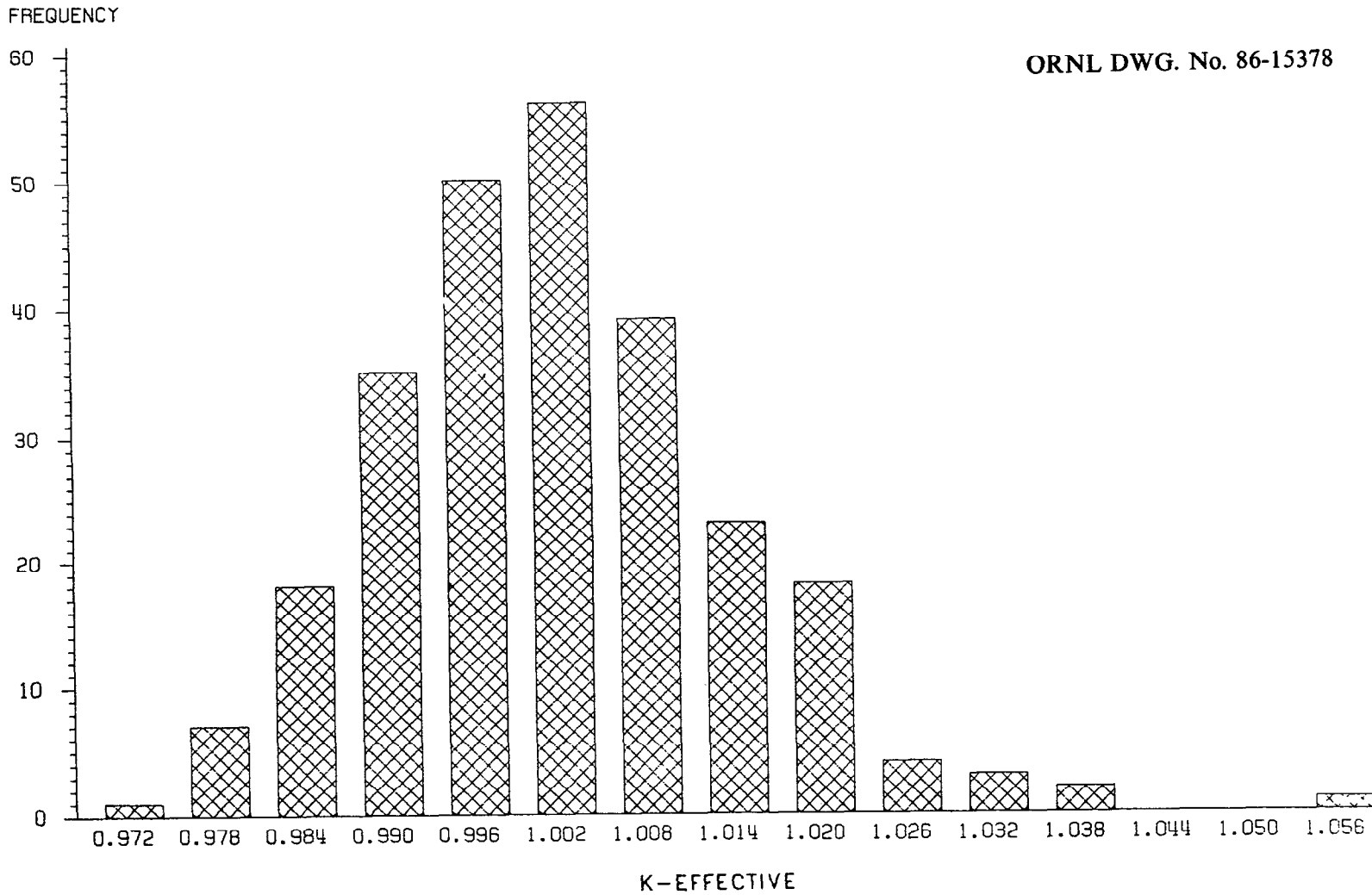
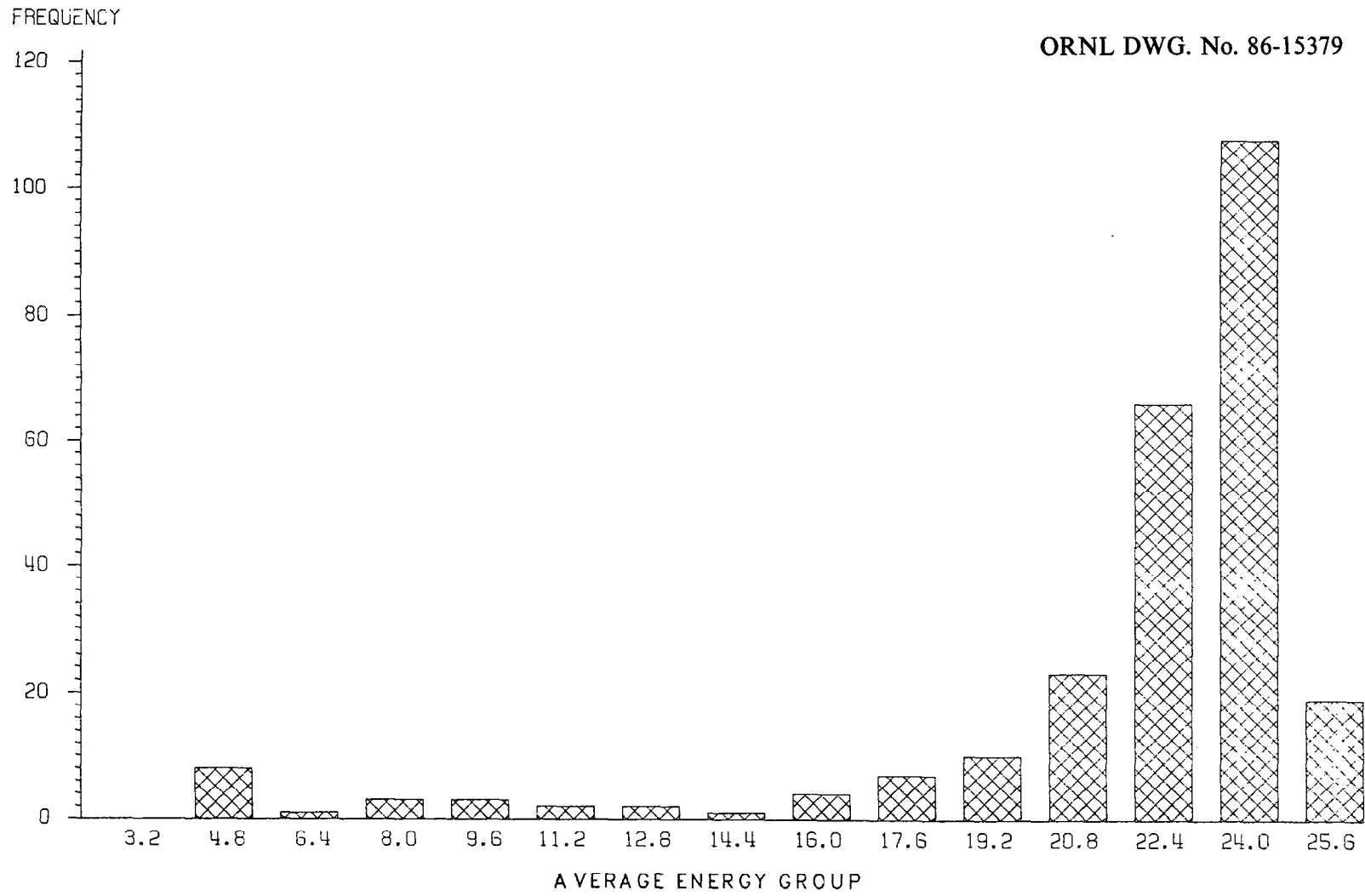


Fig. 1. Frequency chart for k-effective.

FREQUENCY CHART FOR AVERAGE ENERGY GROUP
INCLUDES 258 EXPERIMENTS

ORNL DWG. No. 86-15379



FREQUENCY CHART FOR ENRICHMENT LEVEL
INCLUDES 258 EXPERIMENTS

ORNL DWG. No. 86-15380

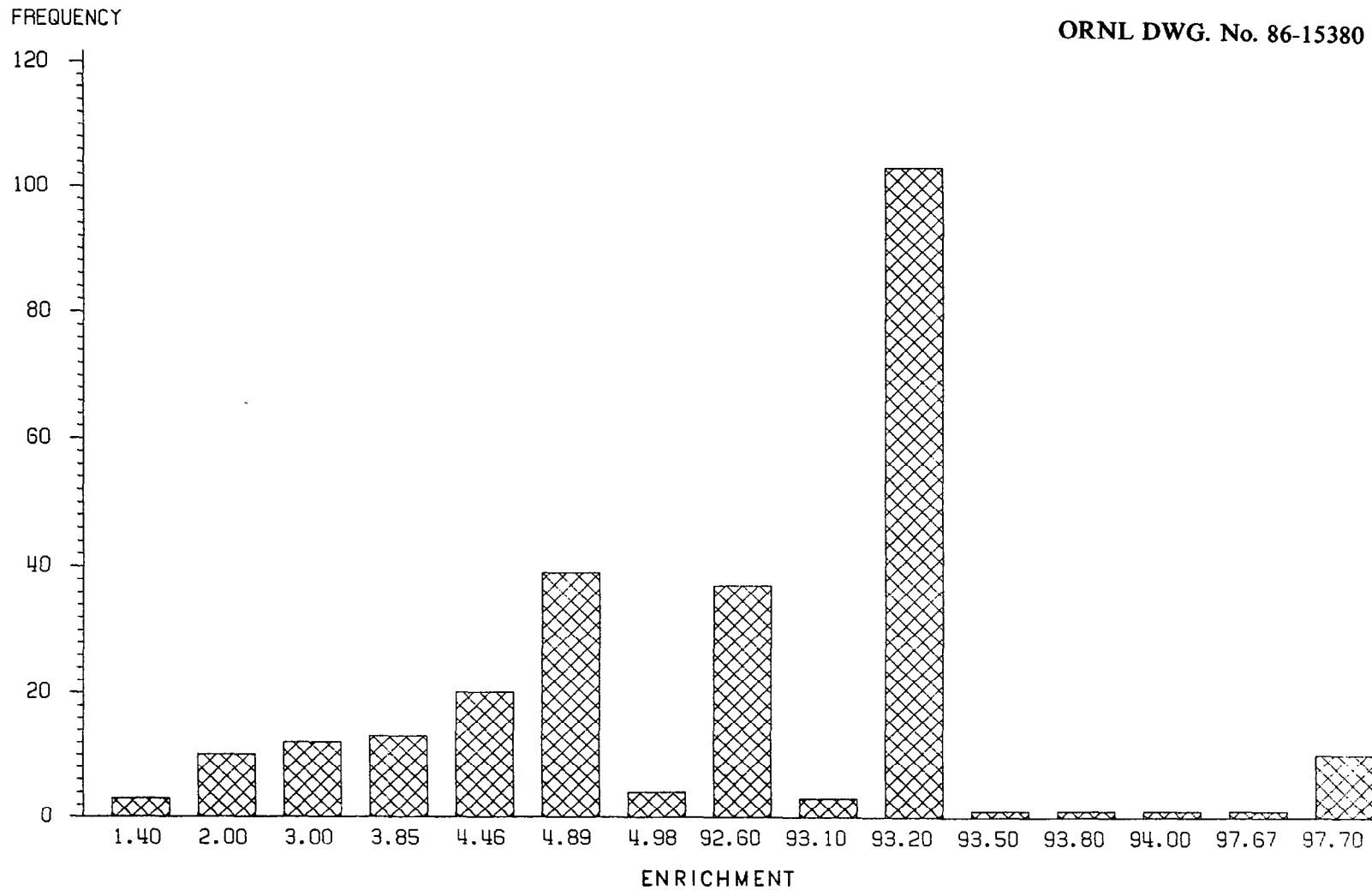


Fig. 3. Frequency chart for enrichment level.

K-EFFECTIVE VS AVERAGE ENERGY GROUP
INCLUDES 258 EXPERIMENTS

ORNL DWG. No. 86-15381

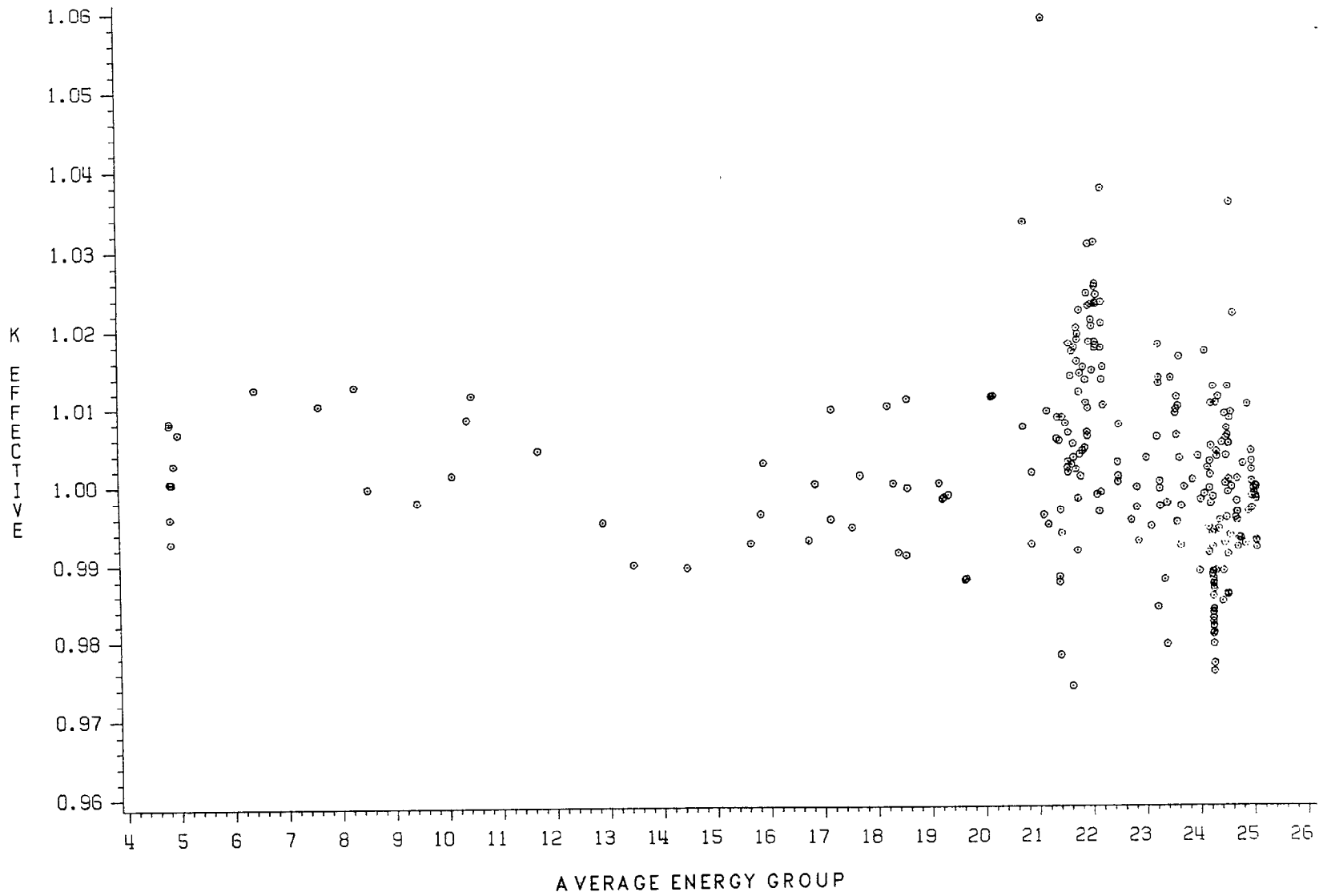
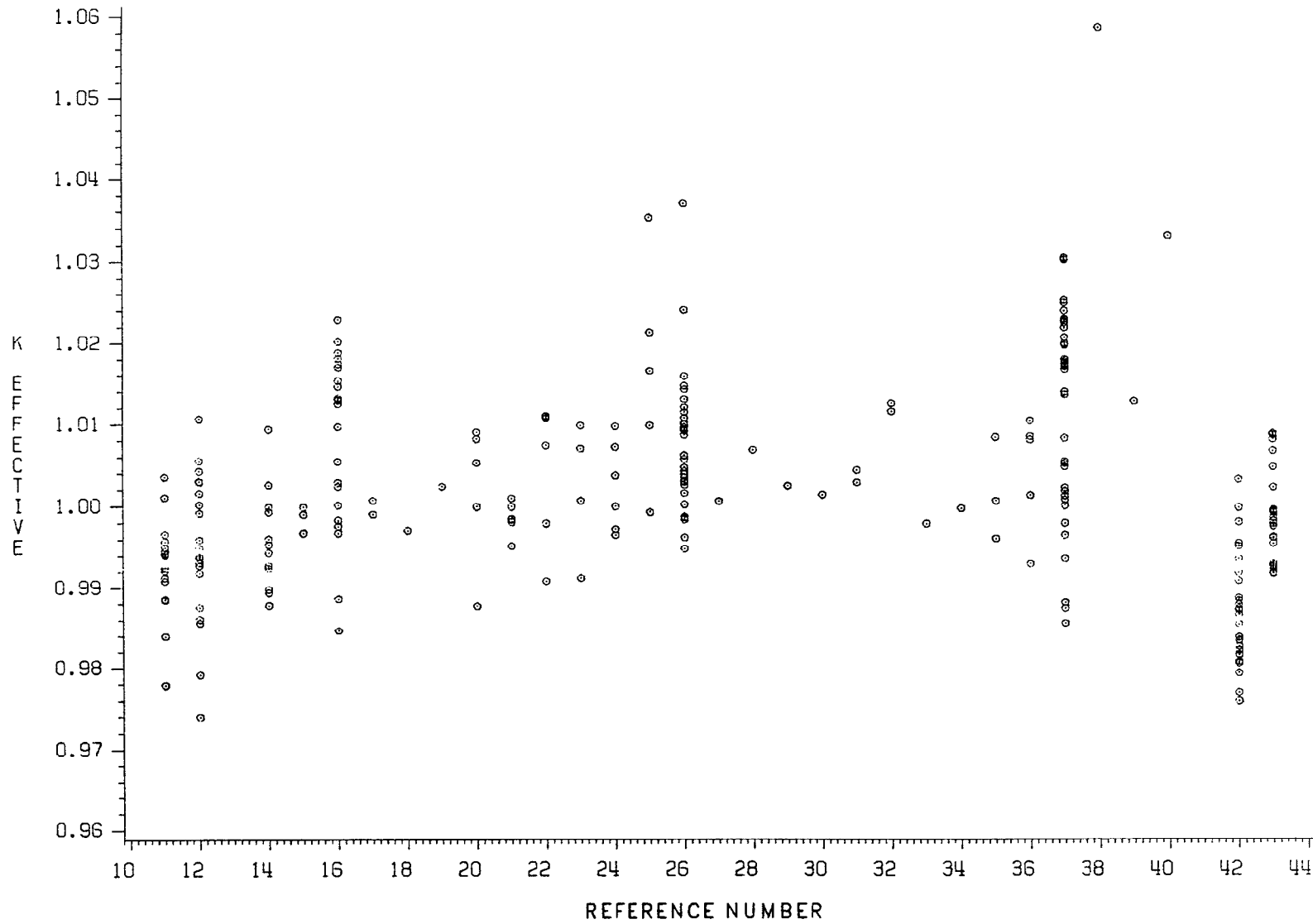


Fig. 4. K-effective vs average energy group.

K-EFFECTIVE VS REFERENCE NUMBER
INCLUDES 258 EXPERIMENTS

ORNL DWG. No. 86-15382



K-EFFECTIVE VS ENRICHMENT LEVEL LOW ENRICHMENT EXPERIMENTS

ORNL DWG. No. 86-15383

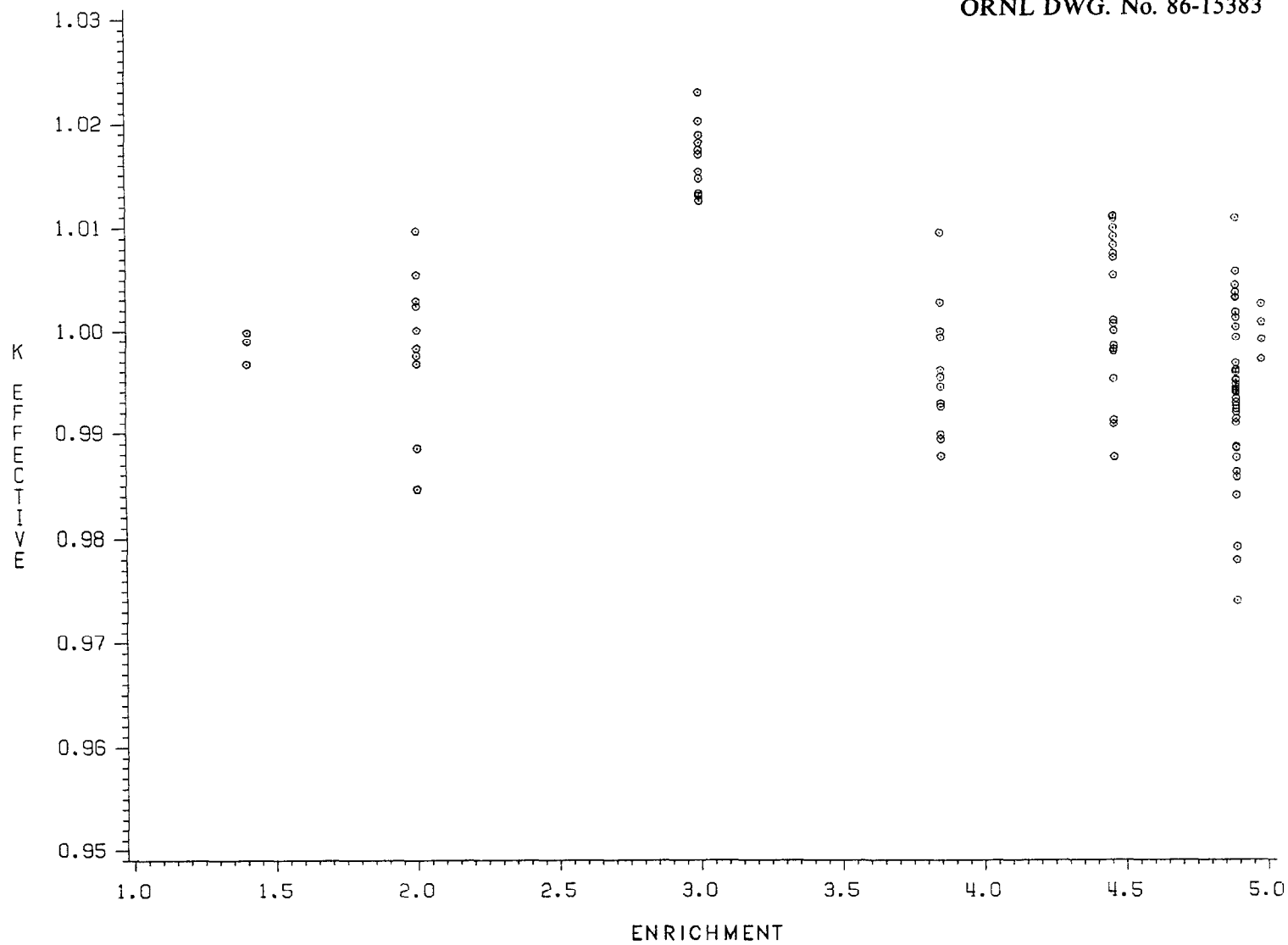


Fig. 6. K-effective vs enrichment level for low enrichment experiments.

K-EFFECTIVE VS ENRICHMENT LEVEL
HIGH ENRICHMENT EXPERIMENTS

ORNL DWG. No. 86-15384

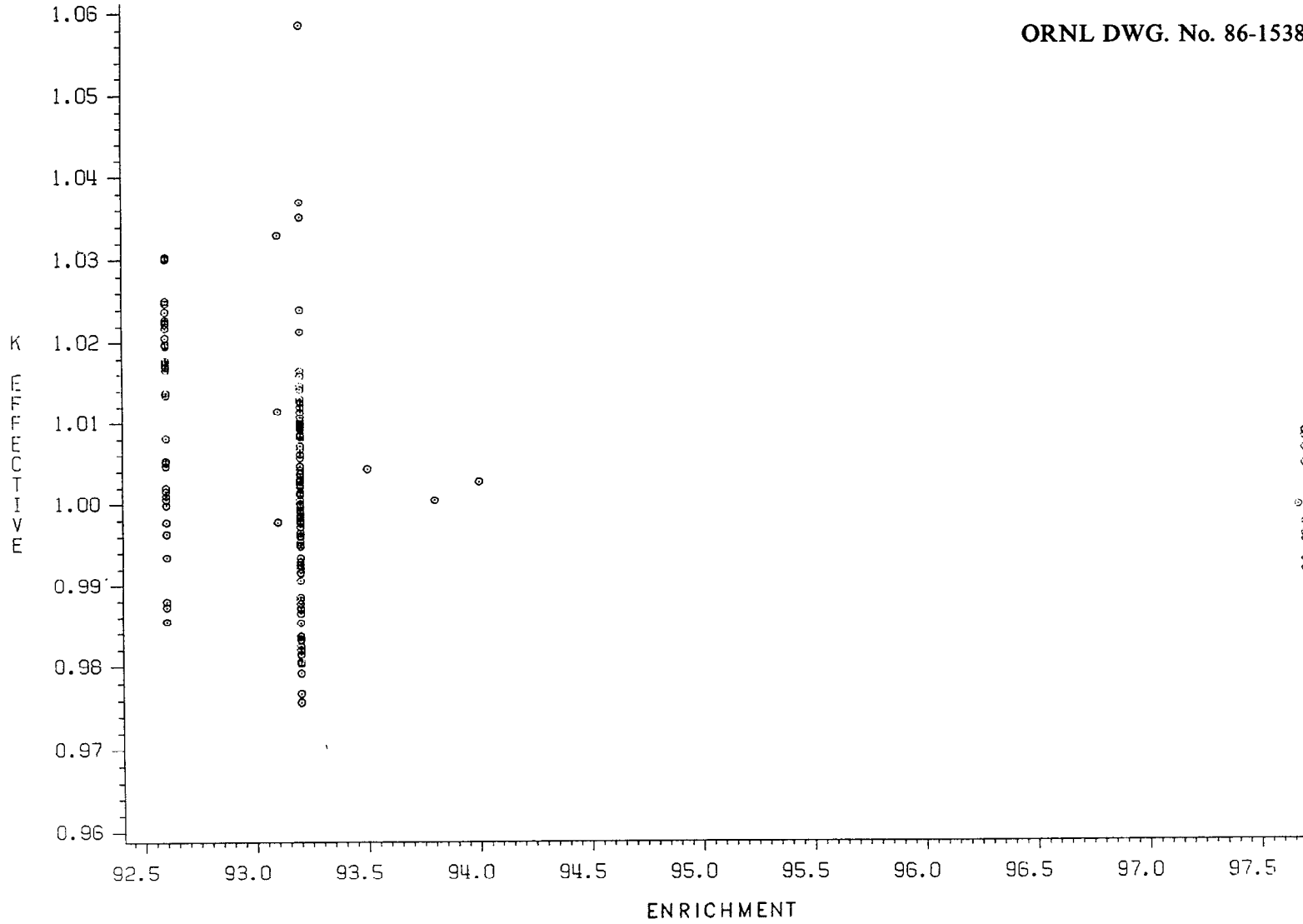


Fig. 7. K-effective vs enrichment level for high enrichment experiments.

K-EFFECTIVE VS AVERAGE ENERGY GROUP
TABLE 1 EXPERIMENTS

ORNL DWG. No. 86-15385

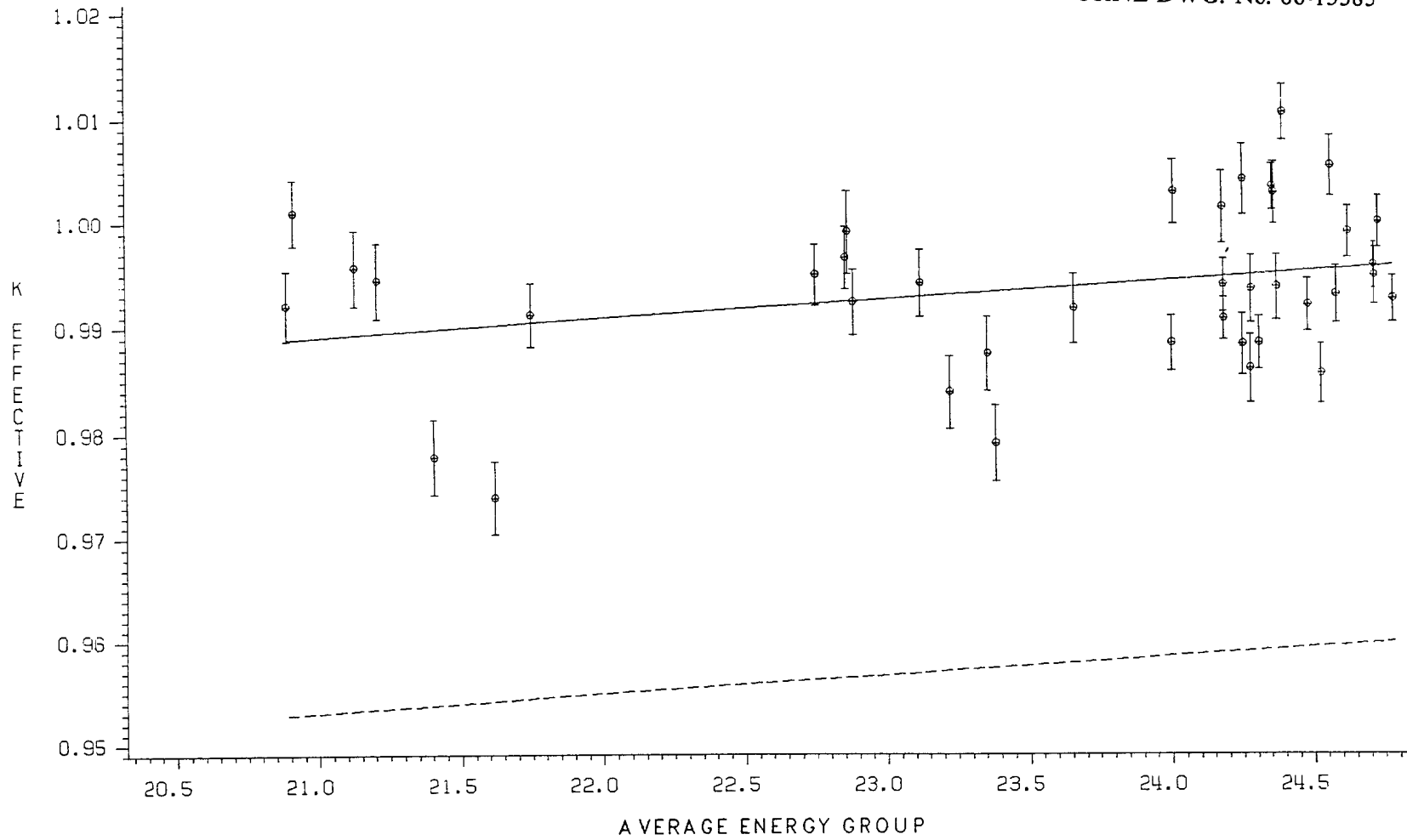


Fig. 8. K-effective vs average energy group for Table 1 experiments.

TABLE 2 EXPERIMENTS

ORNL DWG. No. 86-15386

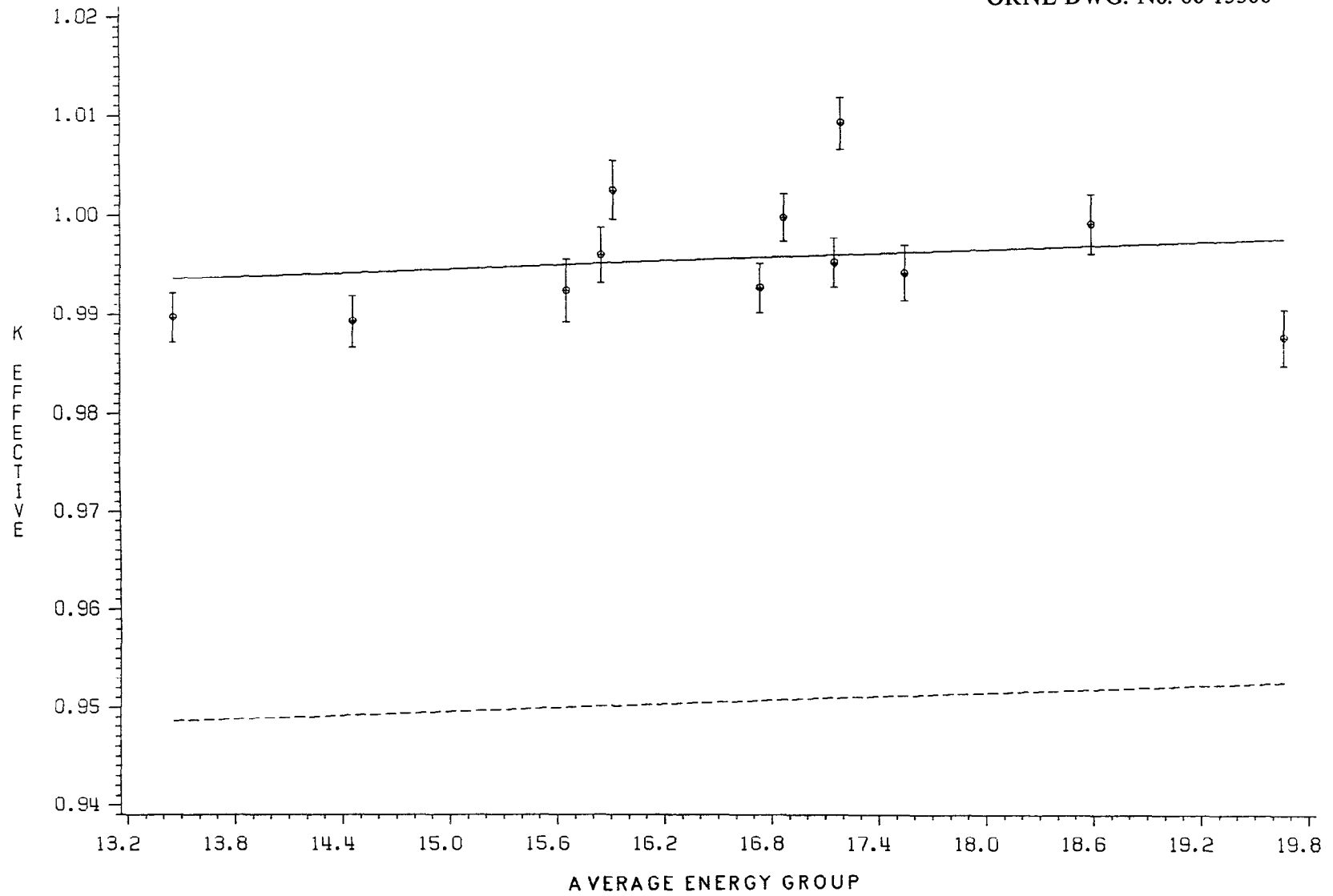


Fig. 9. K-effective vs average energy group for Table 2 experiments.

K-EFFECTIVE VS AVERAGE ENERGY GROUP

TABLE 3 EXPERIMENTS

ORNL DWG. No. 86-15387

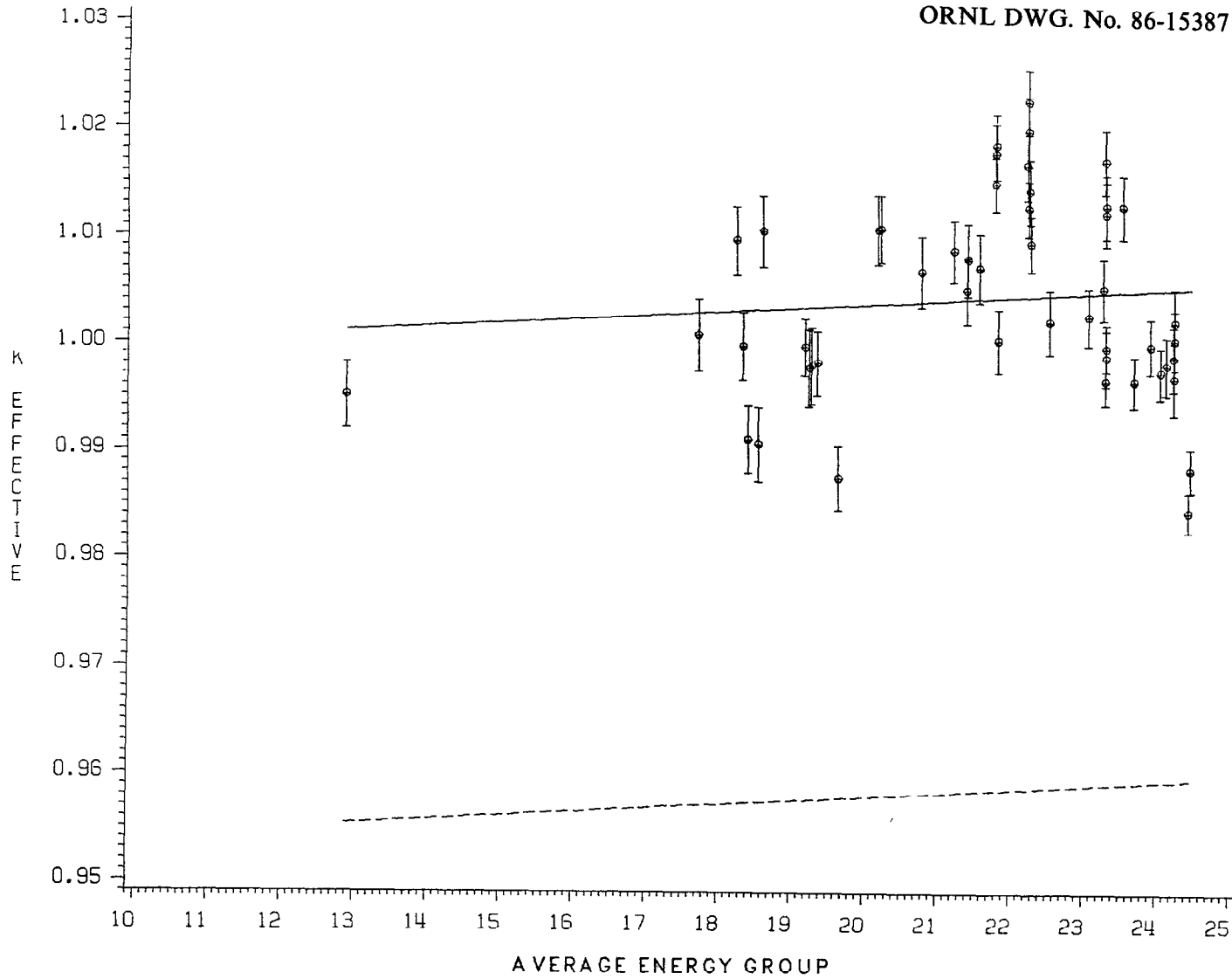


Fig. 10. K-effective vs average energy group for Table 3 experiments.

K-EFFECTIVE VS AVERAGE ENERGY GROUP
TABLE 4 EXPERIMENTS

ORNL DWG. No. 86-15388

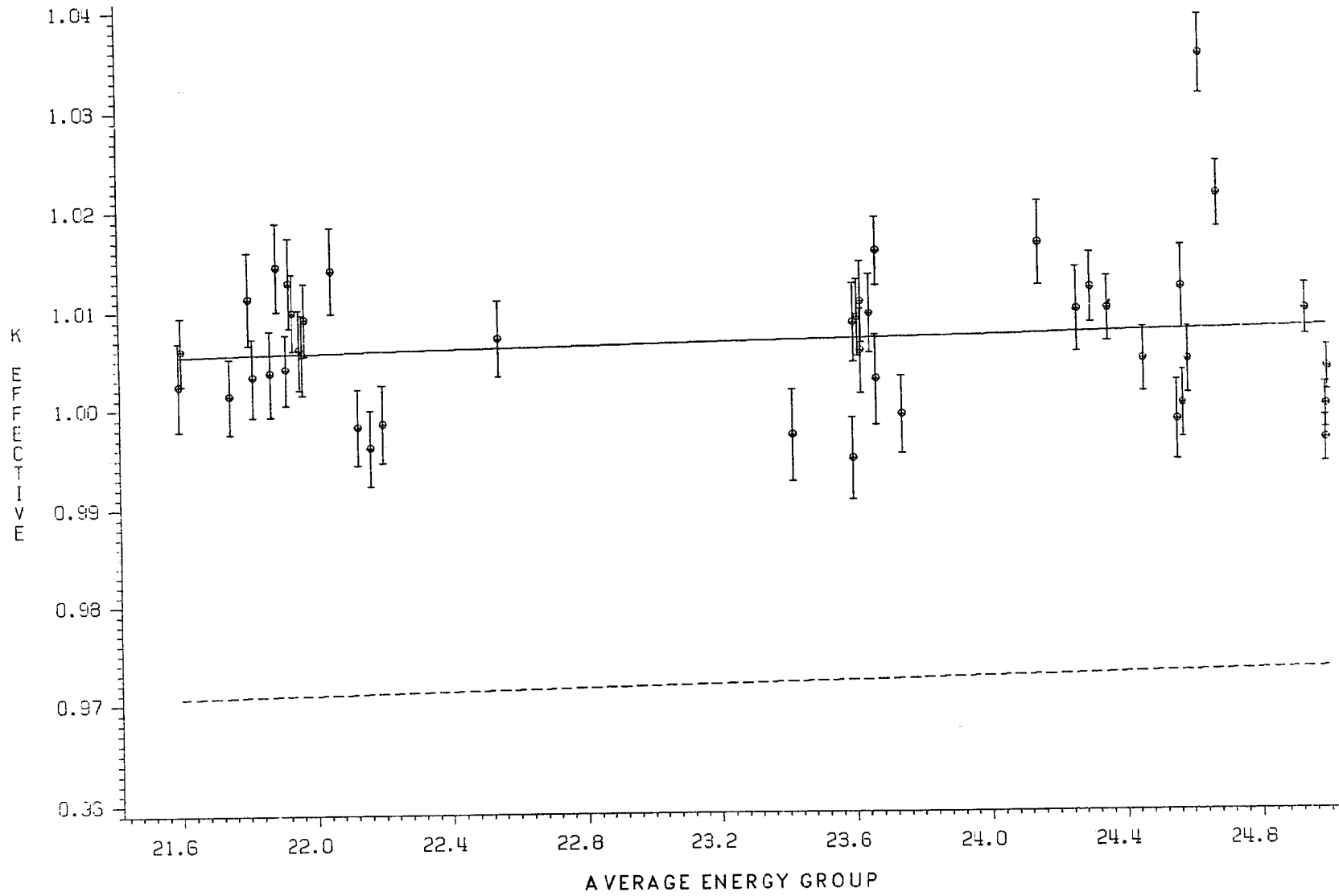


Fig. 11. K-effective vs average energy group for Table 4 experiments.

K-EFFECTIVE VS AVERAGE ENERGY GROUP
TABLE 5 EXPERIMENTS

ORNL DWG. No. 86-15389

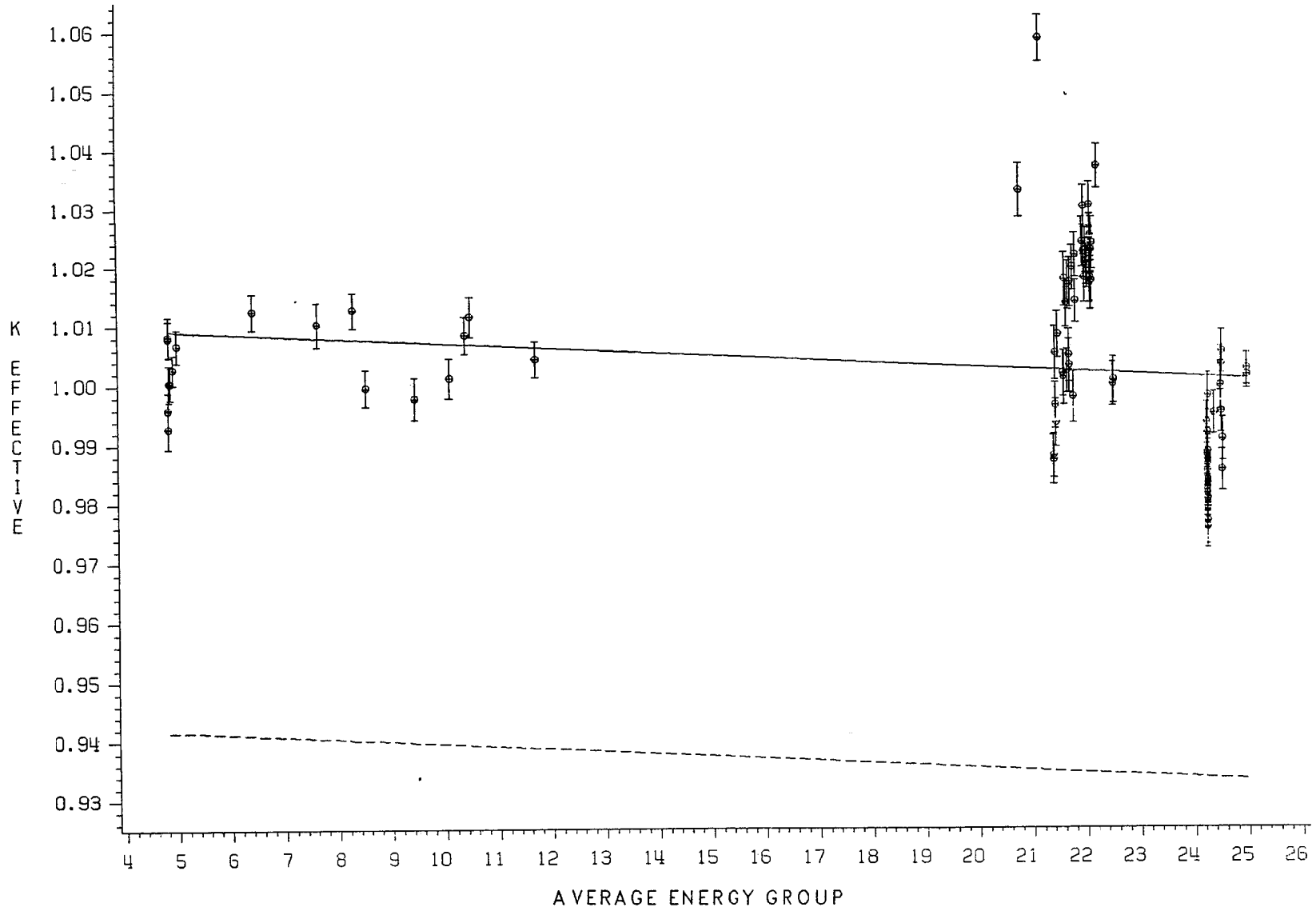


Fig. 12. K-effective vs average energy group for Table 5 experiments.

K-EFFECTIVE VS AVERAGE ENERGY GROUP
TABLE 5 EXPERIMENTS - LOW AVERAGE ENERGY GROUP (4.5 TO 11.5)

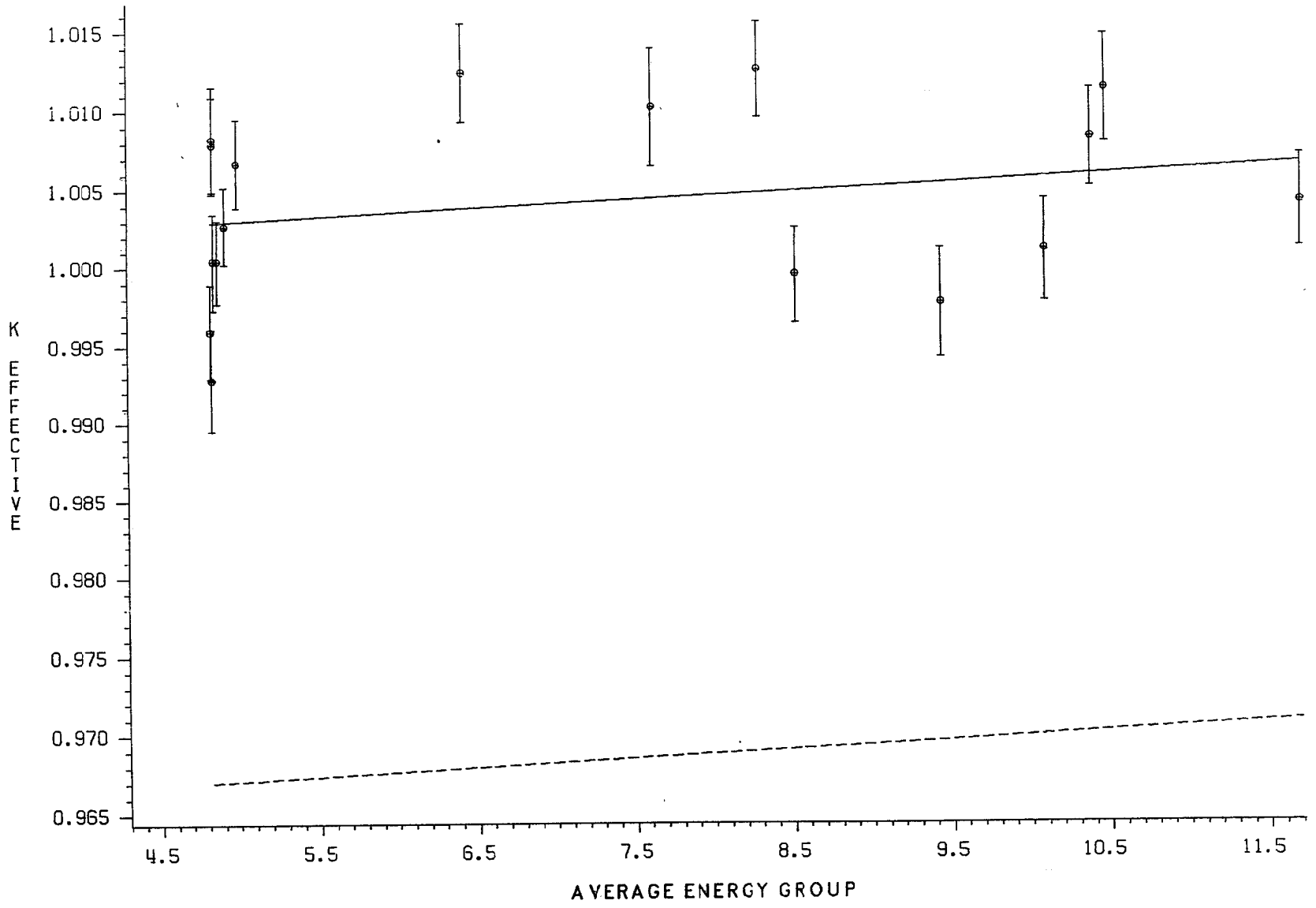


Fig. 12a. K-effective vs average energy group for Table 5 experiments, low average energy group (4.5 to 11.5).

K-EFFECTIVE VS AVERAGE ENERGY GROUP
TABLE 5 EXPERIMENTS - HIGH AVERAGE ENERGY GROUP (20 TO 25)

ORNL DWG. No. 86-15391

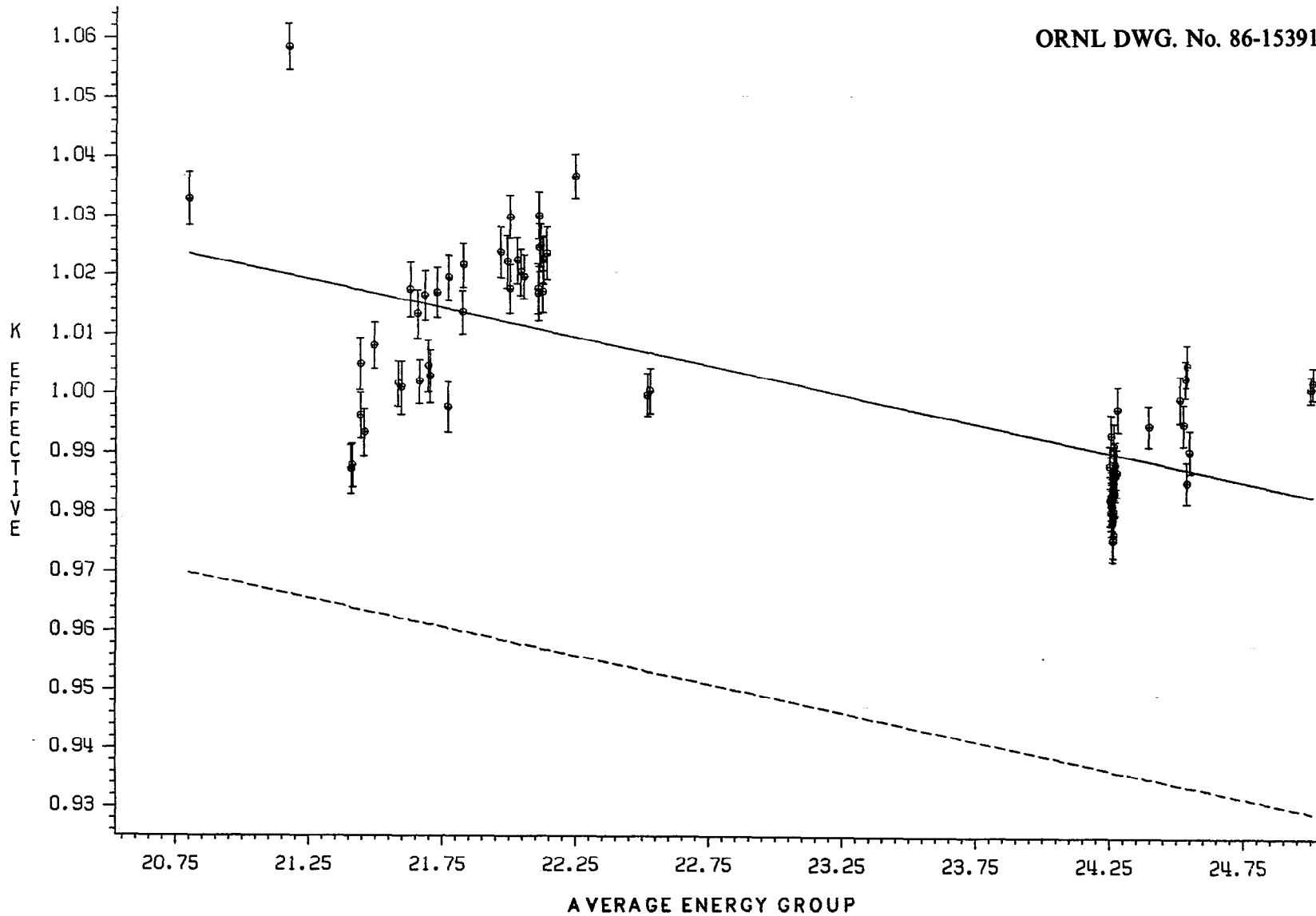


Fig. 12b. K-effective vs average energy group for Table 5 experiments, high average energy group (20 to 25).

K-EFFECTIVE VS AVERAGE ENERGY GROUP

TABLE 6 EXPERIMENTS

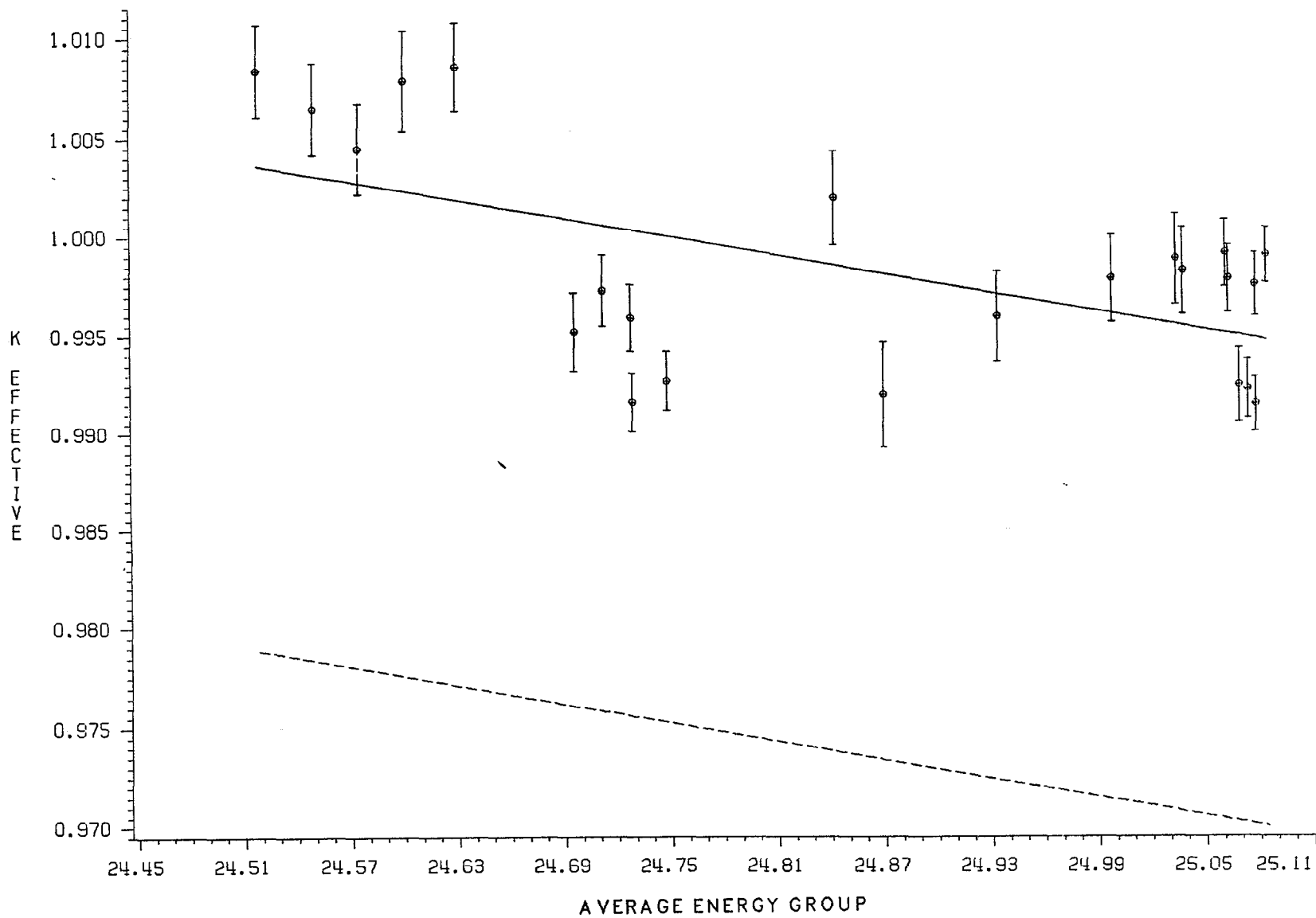


Fig. 13. K-effective vs average energy group for Table 6 experiments.

with great confidence for the design and criticality safety analysis of uranium-containing systems. It appears that slight extensions outside the range of validation would be acceptable. It should be noted that only a fraction of the available options and geometry types have been exercised. Proper performance of the options validated here does not imply that all the options in the code perform as well. It must be emphasized that the calculated k_{eff} from KENO V.a is an estimate of the eigenvalue of the system and has an associated degree of uncertainty due to the statistical nature of the code. Several suggestions are offered to the users of the code.

1. Never base the design or safety of a system on a single calculation. Make at least two calculations in which the random sequence is somehow changed (starting random number, slight change in geometry or materials, etc.) to ensure that the calculated k_{eff} is a reasonable estimate of the calculational mean for the system.
2. Substantial effort may be required to ensure that the problem has converged to a reasonable estimate of the true k_{eff} of the system. Undersampling (insufficient neutrons per generation) or problems with convergence of the source distribution (insufficient generations or a very poor initial starting distribution) are not uncommon.
3. Only validated options and geometry types should be used for the criticality safety design of a system.

2. EVALUATION OF BIAS IN THE KENO V.a VALIDATION

2.1 INTRODUCTION

Several sources of bias were observed during the validation. Most of the validation cases were problems which were already modeled and which had been included in previous validations. A detailed study of all of the experiments included in this validation was not done. Instead, the experimental models were cursorily reviewed against the experimental descriptions in the reference documents. Obvious errors in the experimental models were corrected; otherwise, the models were left unchanged.

The bias, in a series of critical experiments, was studied if (1) the calculated k_{eff} differed from 1.00 by more than about 1% for several of the experiments or, (2) the calculated k_{eff} differed from 1.00 by more than about 2% for a single experiment. For the majority of the calculations, the standard deviation was on the order of ± 0.004 . For a single calculation, it could be expected that about 5% of the time the calculated k_{eff} would be more than 1% above or below 1.00 due to the statistics of the calculation. It would be highly unusual for the statistics to give a 2% bias. For any series of experiments, if more than 5% of the calculations exceed 1% deviation from 1.00, it is an indication that a bias exists.

When bias was suspected, the experimental model was checked against the experimental description. If no discrepancies were observed, then a detailed review of the potential sources of bias was done. The results for the problems reviewed are given in this section. Some recommendations based on the findings of the review are included.

2.2 DISCUSSION

2.2.1 Bias in the 3% Enriched Green Block Calculations from Ref. 18

Cases CAS21-CAS32 in Table 3 all show a positive bias of greater than 1.5%. Review of the reference document did not show major discrepancies between the experimental model and the experimental description. Since the experimental logbook was available for review, a comparison of the logbook description versus the reported description of the experiments was made. It was noted that the reported critical dimensions were not measured dimensions but, rather, were based on nominal block dimensions

with a correction factor applied for stacking voids. The correction factor was obtained from measurements of a very few stacked assemblies which resulted in a conversion factor for nominal size in inches to reported critical size in centimeters. In most cases, the nominal horizontal dimension was increased by 0.61%, and the nominal vertical dimension was increased by 0.45%, as reported in ORNL-CF-59-4-120.⁴⁴ The effects of this approximation were investigated. The results indicated that the potential error in the experimental size did not account for the 1.5% bias in the 3% enriched experiments, and did not explain why the 2% enriched experiments (CAS11-CAS20 in Table 3) gave good results, whereas the 3% calculations were biased.

Case CAS21 was arbitrarily chosen for detailed examination. A 218-group calculation was performed with 120,000 neutron histories yielding a $k_{\text{eff}} = 1.0012 \pm 0.0020$. The difference between the 27-group and 218-group calculations was examined by running XSDRN and collapsing the cross sections by flux weighting to a 27-group structure. The infinite media multiplication factors calculated by the 27- and 218-group cross-section sets were 1.279 and 1.261, respectively, or about 1-1/2% difference. Differences in the U-238 resonance region cross sections accounted for ~91% of the difference between the 27- and 218-group calculations. It was observed that the NITAWL treatment normally accounts for two admixed moderators, whereas, for these experiments, three admixed moderators were present, namely, H, F, and C. The control module was modified to input the second moderator to NITAWL as an effective moderator which approximated the effects of all of the moderating elements. This modification decreased the difference in calculated k_{eff} between the 27-group and 218-group to about 0.6% with values of 1.260 and 1.252, respectively. All of the calculations from ref. 18 were rerun with this modification. A comparison of the results using the standard and modified control modules are given in Table 8. Based on these results, it is recommended that this modification or a comparable one be incorporated into the Y12CSG cross-section processing routines. This would change the random number sequence and would therefore necessitate a subsequent revalidation.

2.2.2 Cross-Section Irregularities in the 27- and 218-Group Cross-Section Sets

During the study of the 3% enriched green block experiments, a RADE⁴⁵ calculation was performed for several elements in the 27- and 218-group cross-section sets. The thermal cross sections for hydrogen were flagged because the absorption cross section (MT-27) did not equal the sum of the neutron disappearance (MT-101) and total fission (MT-18) as it should. The difference was about 1/4% for the entire thermal range. It was determined that this was caused by a systematic error in XLACS2, which failed to account for the presence of oxygen when the thermal data for H₂O was used for the generation of the 218 hydrogen cross-section set from ENDF/B-IV data. The exact impact on the hydrogen data has not as yet been determined. There is good agreement between the calculated k_{eff} for hydrogen-moderated experiments. Therefore, it is not recommended that hydrogen (and all other elements which used thermal kernels based on compounds) be regenerated at this time. However, this should be considered as a potential source of bias in future validations.

The collapsing spectrum used to generate the 27-group cross-section set from the 218 set was also studied. The carbon collapsing function appeared highly irregular with large peaks in the energy ranges of 5 and 500 eV. These peaks should not have occurred considering the Fission-1/E*SIGT-Maxwellian flux spectrum which was used to generate the data, as described in ref. 10. The irregular shape does not affect the total scatter or total absorption cross sections because of carbon's flat cross section, but instead affects the transfer matrix, and, in particular, the within-group scatter. It is not known if the unusual weighting function was caused by a systematic error in XLACS2, or if it was caused by incorrect input data for XLACS2 when the 218 carbon set was generated. A special 218 carbon set was generated using XLACS3 and ENDF/B-IV data, and did not exhibit these irregularities. There is some indication that the existing carbon cross-section set may not be adequate for systems where carbon is the major moderator.

Table 8. Comparison of standard NITAWL treatment vs treating all moderators

| | | | k_{eff} | |
|-------------------------------------|--------------------|--------------|------------------|--------------|
| Case | Standard treatment | | New treatment | |
| CAS11 | 1.0023 | | 0.9965 | |
| 12 | 1.0096 | | 0.9960 | |
| 13 | 1.0054 | | 0.9957 | |
| 14 | 1.0028 | | 0.9929 | |
| 2% | 15 | 0.9967 | 0.9921 | |
| | 16 | 1.0000 | 0.9972 | |
| | 17 | 0.9982 | 0.9951 | |
| | 18 | 0.9975 | 0.9915 | |
| | 19 | 0.9885 | 0.9835 | |
| | 20 | 0.9846 | 0.9874 | |
| | | Avg = 0.9986 | | Avg = 0.9928 |
| | 21 | 1.0145 | 1.0040 | |
| | 22 | 1.0228 | 1.0091 | |
| | 23 | 1.0169 | 1.0097 | |
| | 24 | 1.0129 | 1.0064 | |
| | 25 | 1.0201 | 1.0066 | |
| 3% | 26 | 1.0152 | 1.0043 | |
| | 27 | 1.0187 | 1.0106 | |
| | 28 | 1.0180 | 1.0120 | |
| | 29 | 1.0131 | 1.0040 | |
| | 30 | 1.0173 | 1.0137 | |
| | 31 | 1.0131 | 1.0041 | |
| | 32 | 1.0124 | 1.0064 | |
| | | Avg = 1.0163 | | Avg = 1.0076 |
| Avg of 2% and 3% experiments | 1.0082 | | 1.0008 | |

In general, it appears that the collapsing spectrum for generating the 27-group cross-section set from the 218 cross-section set is not adequate for certain classes of problems. This observation is based on the results of infinite media calculations where up to 7% difference in k_{eff} was observed between the 27- and 218-group calculations. The problem appears to occur for models of experiments which have fairly hard spectrums and contain moderators of intermediate mass. This includes intermediate and highly enriched $\text{UF}_4\text{-CF}_2$ systems and some low enriched $\text{U}_3\text{O}_8\text{-sterotex}$ systems. It should be noted that these observations are based on a study of a very few experiments (which were not included in the validation). The systems studied may not be adequate for inclusion in a validation report. It is recommended that the available experimental information for this class of systems be studied and included in future validations. If these observations are confirmed, there may be a need to incorporate a modification into the Y12CSG sequence to allow a problem-dependent collapse of the fine-group cross sections to a 27-group set.

2.2.3 Code Errors Encountered During Validation

Case CAB09 from Table 2 failed in execution after 42 minutes. It was determined that the cause of failure was due to a divide check in subroutine CROS in KENO V.a. The divide check was traced to a problem with round-off error when a neutron path terminates at the end of a cylinder. This problem is similar to problems which have been previously encountered.

In one study case, differential albedos were used. It was found that turning on the print option PAX in the KENO parameter card caused a change in the random sequence. This problem was traced to an incorrect resetting of a pointer when the print option was triggered.

The correction for both of these problems is straightforward. The proposed corrections should not affect the random sequence on any of the validation runs except for CAB09. It is recommended that these corrections be made to Y12CSG KENO V.a. These corrections would not require a revalidation of the code.

2.2.4 Bias in the 1F Experiments

The complete series of experiments at 415 g U/l, commonly referred to as the 1F arrays, from ref. 38, were included in the validation as cases CAS60-CAS91 in Table 5. Five of these experiments had been included in several previous validations,^{5,6} whereas the complete set of experiments was first included in ref. 6. As a result, two different models of these five cases were included in this validation. Experiments which were included twice are listed in Table 9.

The primary modeling difference is that cases CAS13, CAS19, and CAS29 did not include the experimental room, whereas cases CAS91, CAS64, and CAS63 did. A best estimate of the room was included in the second modeling based on layout drawings of the experiment and descriptions of the experiments from personnel involved in the experiment. When room reflection was included in the model, a 1-1/2% bias for the unreflected cases was eliminated. The two reflected cases are models of the same experiment, except they were prepared by different analysts in a slightly different manner. It is recommended that cases CAS13, CAS16, CAS17, CAS18, and CAS29 be dropped from future validations since they are duplicates and are less accurately modeled.

The balance of the 1F array experiments shows a strong 1-1/2% bias for the reflected cases. These experiments were studied in detail.⁴⁶ The experimental logbook was available, and a comparison of the reported experiments versus the logbook description was done on a case-by-case basis. A number of details had been omitted from the experimental description in ref. 38. The most important of the details seem to be as follows.

Table 9. Duplicate 1F array calculations

| Case | k | Corresponding Case | k | Reflection |
|-------|--------|-----------------------|--------|----------------|
| CAS13 | 0.9854 | CAS91 | 1.0052 | U ^a |
| CAS16 | 0.9879 | CAS64 | 0.9963 | U |
| CAS17 | 1.0250 | CAS74 | 1.0172 | R ^b |
| CAS18 | 1.0010 | CAS72 | 1.0016 | R |
| CAS29 | 0.9872 | CAS63 | 1.0050 | U |

^aU - unreflected^bR - reflected

1. The reported critical arrays are interpolations or extrapolations of the actual experiments. In some cases, a single experiment was used and then extrapolated to an ideal array (an array of identical units equally spaced in three dimensions).
2. Details of the reflector were omitted and only nominal compositions and thicknesses were reported for the experimental materials. In many instances the reflector contained streaming paths (holes) for which no description was given.

Based on the best information available, the experiments were remodeled. Only documentable information was incorporated into these refined models. The results of the calculations for the original and refined models are given in Table 10.

The average of the calculated k_{eff} of the 28 experiments which were remodeled was 1/2% lower for the refined models when compared against the original models. This is considered significant with respect to the statistics of the calculations. The remaining bias is still unexplained.

In the logbook review, it was found that the experiment described in CAS74 was not run. For this experiment, five faces of the array were paraffin-reflected and one was Plexiglas-reflected. (There was insufficient paraffin available to fully reflect the 3x3x3 array with a 15.24-cm reflector.) It is recommended that CAS74 be dropped from future validations, since it is not a model of a critical experiment.

During this sequence of calculations several observations were made.

1. The automatic solution generator in the Y12CSG package caused a small (but noticeable) change in the uranium density and H/U ratio in the nitrate solution. For some cases this caused as much as 1/2% change in the infinite media multiplication factor from XSDRN calculations when compared to results using hand-calculated atomic number densities. It is recommended that the automatic solution generation option not be used if precise detail is available.
2. A comparison was made of the calculated k_{eff} for models in which a default weighting function of 0.5 was used in the reflector versus the use of reflector biasing. For these problems it was found that reflector biasing saved an average of 38% on the CPU time. No irregularities were observed between the full tracking versus "reflector biased" calculations except when paraffin weighting functions were used for thick Plexiglas reflectors. Based on an inspection of adjoint calculations for Plexiglas (as a reflector), it was found that the weighting function for Plexiglas is more like water than paraffin. It is recommended that the paraffin reflector bias not be routinely used for Plexiglas. Plexiglas reflector bias weights may need to be incorporated into the Y12CSG package.
3. It appears that these arrays may be susceptible to undersampling because a different starting random number seed changed the results of several calculations by more than three standard deviations. There was no other apparent indication of undersampling. A neutron batch size of 600 may not be sufficient to hold a good neutron starting distribution for these arrays.
4. A definite trend in k_{eff} in the refined models was observed as the reflector thickness increased. This may be an indication that some important parameter was omitted from the experimental description and/or model. The possibility of poor cross sections or a problem in code physics exists also. At present, the calculated k_{eff} for this series of experiments is considered biased an average of 1 to 1-1/2% high.

2.2.5 Bias in the Slab Experiments from Ref. 43

Cases CAS39-CAS50 of Table 5 are experiments involving 3- and 6-in.-thick slabs of UO_2F_2 solution at 81.8 g U/l. Six of these experiments appeared in Table 5 of ref. 6 and showed no bias. The balance appeared in Table 6 of ref. 6 and showed a strong 2% negative bias but were flagged as "neglecting external scatter that may be significant." A model of a large tank (Big Sid) had been

Table 10. Comparison of calculated k_{eff} for the 1F arrays

| Reflection conditions | Number of units | Original model | Refined model |
|---|-----------------|----------------|---------------|
| Unreflected | (8) | 1.0081 | 1.0039 |
| | (27) | 1.0050 | 0.9940 |
| | (64) | 0.9963 | 0.9969 |
| | (125) | 0.9934 | 0.9983 |
| | | 1.0007 | 0.9983 |
| 1.27 paraffin reflected | (27) | 1.0134 | 1.0000 |
| | (8) | 1.0165 | 1.0084 |
| | | 1.0149 | 1.0042 |
| 1.27 plex reflected | (27) | 1.0016 | 1.0048 |
| | (8) | 1.0175 | 1.0048 |
| | | 1.0095 | 1.0048 |
| 3.81 paraffin reflected | (27) | 1.0300 | 1.0249 |
| | (8) | 1.0177 | 1.0187 |
| | | 1.0239 | 1.0218 |
| 7.62 paraffin reflected | (27) | 1.0302 | 1.0311 |
| | (8) | 1.0169 | 1.0186 |
| | | 1.0236 | 1.0249 |
| 15.24 paraffin reflected | (8) | 1.0177 | 1.0110 |
| | (27) | 1.0117 | 1.0160 |
| | | 1.0202 | 1.0135 |
| 15.24-cm bottom reflector, 5 remaining sides uniform reflector | | | |
| 1.27 paraffin reflected | (27) | 1.0170 | 1.0020 |
| | (8) | 1.0195 | 1.0024 |
| | | 1.0183 | 1.0022 |
| 1.28 plex reflected | (8) | 1.0046 | 1.0023 |
| | (27) | 1.0020 | 1.0159 |
| | | 1.0033 | 1.0091 |
| 2.54 plex reflected | (8) | 1.0137 | 1.0030 |
| | (27) | 1.0217 | 1.0166 |
| | | 1.0177 | 1.0098 |
| 3.81 paraffin reflected | (27) | 1.0205 | 1.0202 |
| | (8) | 1.0225 | 1.0178 |
| | | 1.0215 | 1.019 |
| 4.45 plex reflected | (8) | 1.0223 | 1.0146 |
| 6.35 plex reflected | (8) | 1.0197 | 1.0167 |
| 7.62 paraffin reflected | (8) | 1.0247 | 1.0147 |
| | (27) | 1.0302 | 1.0286 |
| | | 1.0275 | 1.0217 |
| 11.43 plex reflected | (8) | 1.0225 | 1.0179 |
| 15.26 plex reflected | (8) | 1.0237 | 1.0220 |

included in the experimental model for the cases reported in Table 5 of ref. 6. Reference 43 was carefully reviewed, and a model of the experimental room and tank were incorporated as appropriate into all of the models. The room was based on a layout drawing of the experimental facility with a "best estimate" of the actual location of the slabs in the room.

The new models substantially improved the calculations for the experiments done inside Big Sid; however, the experiments done outside of Big Sid still showed a 1-1/2% bias. The experimental logbooks were available and reviewed against the reported experiments. Two items of potential significance were observed:

1. There was no detailed description of the tank support structures including how far from the floor the tanks were positioned during the experiments. There was also no description of a control blade structure which was suspended above at least one of the tanks during all of the experiments.
2. There were fragmented notes made at the time of the experiment, and on two later dates, expressing a concern with the accuracy of the uranium concentration analysis and the possibility that evaporation may have increased the concentration. The experiments were reported as being run at an $H/X=337$; notes in the logbook indicated that the solution concentration was between $H/X=333$ and $H/X=335$ at the end of the experiments.

Table 11 shows a comparison of the original model versus the refined model for these calculations. In the refined models the tanks were 12 in. above the floor (a best estimate based on discussion with personnel involved in the experiments). All calculations included a room model and were at an $H/X=337$. The experiments are reported in the order in which they were performed. All of the experiments done inside Big Sid calculate well. However, all of the experiments done outside of Big Sid still show a bias. Based on the results in Table 11, it appears that the bias in the calculations was either a function of the time at which the experiments were performed or the location at which they were done. The first case could indicate a potential problem with solution concentration; the second would indicate inadequacies in the experimental model. One of the personnel involved in these experiments was questioned as to the possibility of evaporation and an incorrectly reported H/X ratio. It was commented that at the time the experiments were performed, the accuracy of a concentration analysis was usually no better than 1% and that the experiments were reported as "preliminary" because the experimentalists had problems with some of the results. It was suggested that the eta experiments performed some years later be modeled and calculated.

Several infinite media calculations were done using the XSDRN code to study the impact of an incorrect H/X ratio for this solution. The results indicate that the 1-1/2% to 2% bias observed in the experiments done outside Big Sid could have been caused because of an incorrect concentration used in the calculations; however, insufficient evidence is available to discount the possibility of modeling bias.

2.2.6 Bias Caused by the Analyst's Model

When modeling critical experiments, the analyst must decide how much detail to incorporate into his/her model, and, in some cases, how to approximate the various details of the experiment which cannot be modeled explicitly. The amount of detail which is modeled is usually a function of the cost, either time or money, required to include the detail. Many times an analyst calls on past experience in determining what is important and what may be omitted from a model without significantly affecting the results. It was found that cases CAS20 and CAS21 from Table 5 were repeats of Cases CAA30 and CAA38 from Table 4. The calculated k_{eff} for these cases was 1.03654, 1.0239, 0.9961, and 1.0061, respectively. The discrepancies were briefly reviewed. It was found that the cases had been set up by two different analysts at different times. Each experimental model was imprecise in that certain details of the experiment were omitted. It was observed that the major difference between CAS20 and

Table 11. Comparison of calculated k_{eff} for the slab experiments

| k_{eff} | | | |
|---|--|----------------|---------------|
| Case | Comments | Original model | Refined model |
| CAS30 | The first 15 experiments were performed inside Big Sid and took ten days from start to completion | 0.9978 | 0.9950 |
| CAS52 | | 0.9852 | 0.9901 |
| CAS49 | | 0.9831 | 0.9980 |
| CAS50 | | 0.9814 | 0.9941 |
| CAS51 | | 0.9791 | 0.9919 |
| CAS40 | | 0.9824 | 0.9868 |
| CAS34 | | 0.9803 | 0.9878 |
| CAS35 | | 0.9906 | 0.9906 |
| CAS36 | | 0.9933 | 0.9918 |
| CAS37 | | 1.0030 | 1.0030 |
| CAS38 | | 0.9881 | 0.9913 |
| CAS39 | | 0.9952 | 0.9952 |
| CAS32 | | 0.9805 | 0.9921 |
| CAS33 | | 0.9995 | 0.9995 |
| CAS31 | | 0.9949 | 0.9949 |
| 21 days of related experimenting with same solution | | | |
| CAS53 | The last 15 experiments were performed outside of Big Sid and took ten days from start to completion | 0.9884 | 0.9834 |
| CAS41 | | 0.9767 | 0.9821 |
| CAS55 | | 0.9876 | 0.9923 |
| CAS56 | | 0.9869 | 0.9847 |
| CAS43 | | 0.9835 | 0.9803 |
| CAS57 | | 0.9864 | 0.9954 |
| CAS44 | | 0.9757 | 0.9803 |
| CAS58 | | 0.9824 | 0.9793 |
| CAS42 | | 0.9916 | 0.9825 |
| CAS54 | | 0.9831 | 0.9859 |
| CAS59 | | 0.9836 | 0.9852 |
| CAS47 | | 0.9819 | 0.9875 |
| CAS46 | | 0.9832 | 0.9729 |
| CAS45 | | 0.9871 | 0.9946 |
| CAS48 | | 0.9813 | 0.9858 |

Logbook indicates estimated concentration at $H/X=333$ due to evaporation.

CAA30 was that the analyst who set up CAA30 included fire-retardent Plexiglas in the modeling of the upper and lower reflector, whereas the analyst who set up CAS20 used regular Plexiglas for the entire reflector. The result was a 3-1/2% positive bias for CAS20. In CAS21, the analyst chose to ignore a 1.25-cm gap at the junction of the upper and lower reflectors. This omission accounted for approximately 70% of the difference between cases CAS21 and CAA30. Based on these observations, it is recommended that CAS20 and CAS21 be dropped from future validations, and that cases CAA12-CAA43 be reviewed to ensure that sufficient detail has been incorporated into the models. These two cases highlight the importance of accurately modeling reflector compositions and streaming paths in the reflector.

Case CAS14 from Table 5 calculated a k_{eff} of 1.0585. Reference 39 was reviewed, and it was found that several details of the experiment had been omitted from the model. These included the omission of two steel lateral support plates and a detailed model of the stainless-steel slab tank. The model was refined, and the calculated k_{eff} dropped to 1.03. The 3% positive bias has not been accounted for. Reference 39 documents more than 100 critical experiments. Many of the experiments are similar to the 1F array experiments which show a positive bias. Based on this, it is recommended that several more experiments from ref. 39 be included in future validations in order to better establish the bias for these experiments. If possible, additional information beyond what was reported in ref. 39 (such as the experimental logbook and experimentalists' notes) should be reviewed. There is an indication from this experiment (and several others which contain Plexiglas) that the chemical and/or impurity composition of Plexiglas has not been adequately reported. Trace impurities in paraffin or Plexiglas seem to have a strong effect on the calculated k_{eff} . (There is some evidence that high leakage systems, such as arrays, which are reflected by thin reflectors, are biased. This may indicate code or cross-section problems.)

Evidence of analyst bias was also observed in cases CAA08, CAA10, and CAA11 from Table 4. The analyst used a fissile isotope density which was tabulated at 25°C in ref. 27, whereas the experiments were actually done at different temperatures and had different fissile isotope densities. Instead of simply remodeling only the four incorrect experiments, all of the experiments documented in ref. 27 were modeled and run. For these cases, the radius of the "effective" sphere was calculated based on the reported critical volume (since there appeared to be only slight variation due to temperature). The fissile isotope density was based on the reported critical mass and volume. (It was noted that all of the reported masses for experiments performed in the 32-cm-diam tank were flagged as being 2% high; however, the reported masses used.) The concentration and masses were high because a layer of plastic paint used to protect the inside of the tank was not taken into account in the volume measurements. This plastic was not modeled in these calculations. The calculations were done using the modified control module which treats all of the admixed moderators. The results are listed in Table 12.

The results indicate that the U-233 experiments are biased ~2-1/2% high. The U-235 experiments in the 26.4-cm-diam sphere appear to be unbiased, but the experiments in the 32-cm-diam sphere appear to be biased 1-1/2 to 2% high.

Based on these results, it is recommended that cases CAA08-CAA11 be refined or be omitted from future validations. The cause of the bias in the results in Table 12 is not known at this time. If the plastic paint used on the interior surface contained impurities such as chlorine or boron, then omission from the model could explain the results.

2.2.6.1 Bias in CAS19, Table 5

Case CAS19 from Table 5 showed a 3.29% positive bias. The experimental model for the case was compared against the reference document. It was found that the model contained more information than was reported in ref. 41. These arrays have been calculated many times with earlier versions of KENO and the 16-group cross-section set.^{47,48} The input for the earlier calculations was compared. It was found that the automatic solution generator option had been used for the Y12CSG validation, whereas the atomic number densities had been hand calculated and input for previous validations. The

Table 12. UO₂F₂ solution spheres

| H/X | Temp. °C | gm X/l | Calculated k | Original calculation |
|--|-------------|--------|--------------|------------------------------|
| U-233/26.4-cm diam/H₂O reflected | | | | |
| 418.3 | 36.0 | 61.14 | 1.0149 | |
| 414.6 | 39.5 | 61.63 | 1.0287 | |
| 400.5 | 65.5 | 62.96 | 1.0250 | |
| 389.6 | 83.2 | 64.07 | 1.0088 | |
| 378.1 | 96.5 | 65.52 | 1.0231 | |
| U-233/32.0-cm diam/H₂O reflected | | | | |
| 663.1 | 26.3 | 38.72 | 1.0268 | |
| 643.1 | 56.0 | 39.49 | 1.0261 | |
| 602.8 | 99.5 | 41.17 | 1.0411 | |
| U-233/32-cm diam/unreflected | | | | |
| 381.0 | 27.0 | 67.33 | 1.0251 | |
| U-235/26.4-cm diam/H₂O reflected | | | | |
| 268.8 | 27.5 | 95.05 | 1.0028 | |
| 253.3 | 39.5 | 96.67 | 0.9999 | |
| 245.4 | 74.0 | 101.90 | 1.0191 | |
| 239.3 | 85.5 | 103.86 | 1.0055 | CAA10, k = 1.0164 |
| U-235/32.0-cm diam/H₂O reflected | | | | |
| 515.1 | 27.0 | 50.28 | 1.0045 | CAA08, k = 1.0212 |
| 502.6 | 43.0 | 51.20 | 1.0173 | |
| 503.4 | 43.0 | 51.13 | 1.0094 | |
| 496.5 | 54.0 | 51.59 | 1.0131 | |
| 487.6 | 64.5 | 52.22 | 1.0218 | |
| 476.8 | 87.5 | 52.72 | 1.0190 | (averaged) CAA11, k = 1.0351 |
| 459.6 | 87.5 | 54.61 | 1.0220 | |
| U-235/32.0-cm diam/unreflected | | | | |
| 203.5 | 27.0 | 125.08 | 1.0078 | CAA09, k = 0.9991 |

difference was an 0.6% increase in the uranium density and an 8% increase in the H/X ratio for the number densities calculated by the automatic solution generator. It was also found that the composition for stainless steel 304 differed from what the code uses in standard composition SS304.

The KENO output indicated a potential source convergence and/or undersampling problem in that the average value of k_{eff} was 1.0198, where the calculated k with the lowest standard deviation was 1.0329. The plot of k_{eff} by generation skipped showed an unusual trend. The plot of average k_{eff} indicated that the source distribution had not converged after more than 40 generations, and convergence was from low k_{eff} toward the final value. It appears that calculations which approach the final value from below tend to have more difficulty converging the source than those which approach the final value from above. The calculation was rerun using the atomic number densities used in previous validations. In addition, a cosine starting distribution was used over a section at the central portion of the column. The calculated k was 1.0201. Several of the pipe intersection experiments should be included in future validations in order to establish the bias for this type of system.

3. GENERAL COMMENTS ON THE EXPERIMENTS REVIEWED

Based on the study of the experiments which showed some evidence of bias, several observations may be made. The most significant is that a large proportion of the experiments which have been included in this validation and in previous validations should be scrutinized to determine their adequacy for use in validating codes. There is a surprising lack of detail in the descriptions of the experiments, including estimates of the accuracy of concentration in the fissile mixture, the actual dimensions and composition of the materials involved in the experiment and the experimental layout itself. Details such as the description of the experimental room and the location of the experiment in the room have been omitted from most reports. For some systems, these details are extremely important; and their inclusion or omission may bias the calculated results. In some of the experiments studied, the uncertainty in the experimental parameters could easily bias calculated results 2% high or low, but the uncertainties were not reported. This deficiency indicates a need for a set of experiments which has been carefully evaluated specifically for validation purposes such that reporting bias is eliminated (or at least is well known).

In some instances, the modeling of the critical experiment was found to be poor and biased the results by more than 2%. This again shows a lack of attention to detail. In other cases, the models which were set up were incorrect. These deficiencies indicate a need to verify the accuracy of the models used for validation. Reporting bias and/or modeling bias tend to mask potential problems with the code or cross sections being used. Since these forms of bias are not systematic, the inclusion of these results in any trend analysis should be avoided in order to eliminate the possibility of artificial trends. Extrapolation and/or interpolation of critical experiment information based on artificial trends may not be correct.

In order for the codes and cross sections used for criticality safety to be improved, validation efforts should continue. The cause of the bias in the calculations should be determined and eliminated if possible.

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Appendix A

Y12CSG INPUT DATA USED FOR VALIDATION CASES

Input data for the validation appears in the same order as listed in Tables 1-6 of Sect. 1 of this report.

| | |
|-------------------------------------|-------|
| Table A.1. Table 1 input data | A-2 |
| Table A.2. Table 2 input data | A-14 |
| Table A.3. Table 3 input data | A-37 |
| Table A.4. Table 4 input data | A-98 |
| Table A.5. Table 5 input data | A-108 |
| Table A.6. Table 6 input data | A-133 |

Table A.1. Table 1 input data

```

CAA01
=CSAS25
LIBBY EXP. 4.89% RODS 30 CM LONG, .762 CM DIAM, 1.3 CM PITCH
27GROUPNDF4 LATTICECELL
URANIUM 1 .9995 293 92235 4.89 92238 95.11 END
H2O 2 1 END
PLEXIGLASS 3 1 END
END COMP
SQUAREPITCH 1.3 .762 1 2 END
LIBBY EXP. 4.89% RODS 30 CM LONG, .762CM DIAM, 1.3CM PITCH
READ PARAM NPG=600 NUB=YES FDN=YES END PARAM
READ GEOM
UNIT 1
CYLINDER 1 1 .381 5.08 0
CUBOID 2 1 4P.65 5.08 0
UNIT 2
CYLINDER 1 1 .381 1.27 0
CUBOID 3 1 4P.65 1.27 0
UNIT 3
CYLINDER 1 1 .381 17.935 0
CUBOID 2 1 4P.65 17.935 0
UNIT 4
CYLINDER 1 1 .381 .635 0
CUBOID 3 1 4P.65 .635 0
UNIT 5
CUBOID 2 1 4P.65 5.08 0
UNIT 6
CYLINDER 2 1 .381 1.27 0
CUBOID 3 1 4P.65 1.27 0
UNIT 7
CUBOID 2 1 4P.65 17.935 0
UNIT 8
CYLINDER 2 1 .381 .635 0
CUBOID 3 1 4P.65 .635 0
CORE 0 1 3R0
REFLECTOR 3 1 5R0 3.81 1
REFLECTOR 2 2 5R3 0 1
REFLECTOR 2 3 5R3 2.19 1
REFLECTOR 2 4 4R3 3.2 3 1
REFLECTOR 2 5 4R3 0 3 2
END GEOM
READ ARRAY NUX=20 NUY=21 NUZ=5 FILL
19R5 401R1 19R6 401R2 19R7 401R3 19R8 401R4 19R5 401R1
END FILL END ARRAY
READ BIAS ID=500 2 6 END BIAS
END DATA
END

```

```

CAA02
=CSAS25
LIBBY EXP. 4.89% RODS 30 CM LONG, .762 CM DIAM, 1.3CM PITCH
27GROUPNDF4 LATTICECELL
URANIUM 1 .995 293 92235 4.89 92238 95.11 END
H2O 2 1 END
PLEXIGLASS 3 1 END
END COMP
SQUAREPITCH 1.3 .762 1 2 END
LIBBY H2O REFL. CASE 4B_
READ PARAM NPG=600 NUB=YES FDN=YES END PARAM
READ GEOM
UNIT 1
CYLINDER 1 1 .381 30 0
CUBOID 2 1 4P.65 30 0
UNIT 2
CUBOID 2 1 4P.65 30 0
CORE 0 1 3R0
REFLECTOR 2 2 6R3 1
REFLECTOR 2 3 4R3 1 3 1
REFLECTOR 2 4 4R3 0 3 3
END GEOM
READ ARRAY NUX=22 NUY=22 NUZ=1 FILL
10R1 2R2 10R1 9Q22 44R2 10R1 2R2 10R1 9Q22
END FILL END ARRAY
READ BIAS ID=500 2 6 END BIAS
END DATA
END

```

```

CAA03
=CSAS25
LIBBY EXP. 4.89% RODS 30 CM LONG, .762 CM DIAM, 1.3 CM PITCH
27GROUPNDF4 LATTICECELL
URANIUM 1 .9995 293 92235 4.89 92238 95.11 END
H2O 2 1 END
PLEXIGLASS 3 1 END
END COMP
SQUAREPITCH 1.3 .762 1 2 END
LIBBY H2O REFL. CASE 11A
READ PARAM NPG=600 NUB=YES FDN=YES END PARAM
READ GEOM
UNIT 1
CYLINDER 1 1 .381 30 0
CUBOID 2 1 4P.65 30 0
UNIT 2
CUBOID 2 1 4P.65 30 0
CORE 0 1 3R0
REFLECTOR 2 2 6R3 2
REFLECTOR 2 4 4R3 1.9 3 1
REFLECTOR 2 5 4R3 0 3 2
END GEOM
READ ARRAY NUX=23 NUY=23 NUZ=1 FILL
12R2 2R1 2 2Q3 2R1 Q23 23R2 2R1 2 6Q3 2R1 N46 5Q69
2R1 2 6Q3 2R1 Q23
END FILL END ARRAY
READ BIAS ID=500 2 6 END BIAS
END DATA
END

```

Table A.1 (continued)

```

CAA04
=CSAS25
LIBBY EXP. 4.89 RODS 30 CM LONG, .762 CM DIAM, 2.05 CM PITCH
27GROUPNDF4 LATTICECELL
URANIUM 1 .9995 293 92235 4.89 92238 95.11 END
H2O 2 1 END
PLEXIGLASS 3 1 END
END COMP
SQUAREPITCH 2.05 .762 1 2 END
LIBBY H2O REFL. CASE 6A
READ PARAM NPG=600 NUB=YES FDN=YES END PARAM
READ GEOM
UNIT 1
CYLINDER 1 1 .381 30 0
CUBOID 2 1 4P1.025 30 0
UNIT 2
CUBOID 2 1 4P1.025 30 0
CORE 0 1 3R0
REFLECTOR 2 2 6R3 3
REFLECTOR 2 5 4R3 .3 3 1
REFLECTOR 2 6 4R3 0 3 1
END GEOM
READ ARRAY NUX=14 NUY=15 NUZ=1 FILL
7R1 7R2 F1
END FILL END ARRAY
READ BIAS ID=500 2 6 END BIAS
END DATA
END

```

```

CAA05
=CSAS25
LIBBY EXP. 4.89% RODS 30 CM LONG, .762 CM DIAM, 2.05 CM PITCH
27GROUPNDF4 LATTICECELL
URANIUM 1 .9995 293 92235 4.89 92238 95.11 END
H2O 2 1 END
PLEXIGLASS 3 1 END
END COMP
SQUAREPITCH 2.05 .762 1 2 END
LIBBY H2O REFL. CASE 8C
READ PARAM NPG=600 NUB=YES FDN=YES END PARAM
READ GEOM
UNIT 1
CYLINDER 1 1 .381 30 0
CUBOID 2 1 4P1.025 30 0
UNIT 2
CUBOID 2 1 4P1.025 30 0
CORE 0 1 3R0
REFLECTOR 2 2 6R3 1
REFLECTOR 2 3 4R3 .35 3 1
REFLECTOR 2 4 4R3 0 3 3
END GEOM
READ ARRAY NUX=22 NUY=22 NUZ=1 FILL
10R1 2R2 10R1 9Q22 22R2 N242
END FILL END ARRAY
READ BIAS ID=500 2 6 END BIAS
END DATA
END

```

```

CAA06
=CSAS25
LIBBY EXP. 4.89% RODS 30 CM LONG, .762 CM DIAM, 1.3 CM PITCH
27GROUPNDF4 LATTICECELL
URANIUM 1 .9995 293 92235 4.89 92238 95.11 END
H2O 2 1 END
PLEXIGLASS 3 1 END
PB 4 1 END
END COMP
SQUAREPITCH 1.3 .762 1 2 END
LIBBY H2O REFL. CASE 14A PB 1 FACE
READ PARAM NPG=600 NUB=YES PLT=NO FDN=YES END PARAM
READ GEOM
UNIT 1
CYLINDER 1 1 .381 30 0
CUBOID 2 1 4P.65 30 0
UNIT 2
CUBOID 2 1 4P.65 30 0
UNIT 3
ARRAY 1 3R0
REFLECTOR 2 2 2R3 0 3 2R0 2
REFLECTOR 2 4 2R1.32 0 1.32 2R0 1
UNIT 4
CUBOID 4 1 2P20.32 2P10.16 25.4 0
REFLECTOR 2 2 4R0 1.425 0 1
REFLECTOR 3 2 5R0 3.175 1
ARRAY 2 3R0
REFLECTOR 2 4 2R1.68 0 1.68 2R0 1
REFLECTOR 2 5 2R3 0 3 2R0 2
REFLECTOR 2 2 4R0 3 0 1
REFLECTOR 2 3 4R0 2.1 0 1
REFLECTOR 3 2 5R0 3 4
REFLECTOR 3 6 5R0 1.97 1
END GEOM
READ ARRAY ARA=1 NUX=20 NUY=20 NUZ=1 FILL
18R1 2R2 F1
END FILL
ARA=2 NUX=4 NUY=2 NUZ=1 FILL 3 4
END FILL END ARRAY
READ BIAS ID=500 2 6 END BIAS
READ PLOT TTL='14A X-Y' PIC=MIX
XUL=-7.8 YUL=53.8 ZUL=15 XLR=48.8 YLR=-7.8 ZLR=15
UAX=1 VDN=-1 NAX=125 END
TTL='14A X-Y' PIC=WTS END
TTL='14A Y-Z' PIC=MIX
XUL=20 YUL=-7.8 ZUL=35.5 XLR=20 YLR=53.8 ZLR=-14.1
VAX=1 WDN=-1 UAX=0 VDN=0 NAX=125 END
TTL='14A Y-Z' PIC=WTS END
END PLOT
END DATA
END

```

Table A.1 (continued)

```

CAA07
=CSAS25
LIBBY EXP. 4.89% RODS 30 CM LONG, .762 CM DIAM, 1.3 CM PITCH
27GROUPNDF4 LATTICECELL
URANIUM 1 .9995 293 92235 4.89 92238 95.11 END
H2O 2 1 END
PLEXIGLASS 3 1 END
PB 4 1 END
END COMP
SQUAREPITCH 1.3 .762 1 2 END
LIBBY H2O REFL. CASE 23B PB 4 FACES
READ PARAM NPG=600 NUB=YES PLT=NO FDN=YES END PARAM
READ GEOM
UNIT 1
CYLINDER 1 1 .381 27 0
CUBOID 2 1 4P.65 27 0
UNIT 2
CUBOID 2 1 4P.65 27 0
UNIT 7
CYLINDER 1 1 .381 3 0
CUBOID 0 1 4P.65 3 0
UNIT 8
CUBOID 0 1 4P.65 3 0
UNIT 3
ARRAY 1 3R0
REFLECTOR 2 1 4R3.221 2R0 1
UNIT 9
ARRAY 4 3R0
REFLECTOR 0 1 4R3.221 2R0 1
UNIT 10
ARRAY 5 3R0
UNIT 4
CUBOID 4 1 2P10.16 2P16.871 25.4 0
REFLECTOR 0 1 4R0 1.425 0 1
REFLECTOR 3 2 5R0 3.175 1
UNIT 5
ARRAY 2 3R0
UNIT 6
CUBOID 4 1 2P37.191 2P10.16 25.4 0
REFLECTOR 0 1 4R0 1.425 0 1
REFLECTOR 3 2 5R0 3.175 1
ARRAY 3 3R0
REFLECTOR 3 2 5R0 3 4
REFLECTOR 3 6 5R0 1.97 1
END GEOM
READ ARRAY ARA=1 NUX=21 NUY=21 NUZ=1 FILL
10R1 2 10R1 9Q21 21R2 10R1 2 10R1 9Q21
END FILL
ARA=4 NUX=21 NUY=21 NUZ=1 FILL
10R7 8 10R7 9Q21 21R8 10R7 8 10R7 9Q21
END FILL
ARA=2 NUX=3 NUY=1 NUZ=1 FILL 4 10 4 END FILL
ARA=3 NUX=1 NUY=3 NUZ=1 FILL 6 5 6
END FILL
ARA=5 NUX=1 NUY=1 NUZ=2 FILL 3 9
END FILL END ARRAY
READ BIAS ID=500 2 6 END BIAS
READ PLOT TTL=' X-Y' PIC=MIX
XUL=0 YUL=75 ZUL=15 XLR=75 YLR=0 ZLR=15
UAX=1 VDN=-1 NAX=125 END
TTL=' X-Y' PIC=WTS END
TTL=' Y-Z' PIC=MIX
XUL=33 YUL=0 ZUL=31 XLR=33 YLR=75 ZLR=-14.1
VAX=1 WDN=-1 UAX=0 VDN=0 NAX=125 END
TTL=' Y-Z' PIC=WTS END

```

```

END PLOT
END DATA
END

```

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CAA08
=CSAS25
LIBBY EXP. 4.89% RODS 30 CM LONG, .762 CM DIAM, 1.3 CM PITCH
27GROUPNDF4 LATTICECELL
URANIUM 1 .9995 293 92235 4.89 92238 95.11 END
H2O 2 1 END
PLEXIGLASS 3 1 END
PB 4 1 END
END COMP
SQUAREPITCH 1.3 .762 1 2 END
LIBBY H2O REFL. CASE 26A PB 4 FACES
READ PARAM NPG=600 NUB=YES PLT=NO FDN=YES END PARAM
READ GEOM
UNIT 1
CYLINDER 1 1 .381 30 0
CUBOID 2 1 4P.65 30 0
UNIT 2
CUBOID 2 1 4P.65 30 0
UNIT 3
ARRAY 1 3R0
REFLECTOR 2 1 .62 .62 .62 4.52 2R0 1
UNIT 4
CUBOID 4 1 2P10.16 2P15.57 25.4 0
REFLECTOR 2 2 4R0 1.425 0 1
REFLECTOR 3 2 5R0 3.175 1
UNIT 5
ARRAY 2 3R0
UNIT 6
CUBOID 4 1 2P35.89 2P10.16 25.4 0
REFLECTOR 2 2 4R0 1.425 0 1
REFLECTOR 3 2 5R0 3.175 1
ARRAY 3 3R0
REFLECTOR 2 2 4R0 3 0 2
REFLECTOR 2 4 4R0 1.95 0 1
REFLECTOR 3 2 5R0 3 4
REFLECTOR 3 6 5R0 1.97 1
END GEOM
READ ARRAY ARA=1 NUX=23 NUY=20 NUZ=1 FILL
3R2 2R1 2 5Q3 2R1 Q23 23R2 Q69 2 1 2 2R1 2 5Q3 2R1
2R1 2 6Q3 2R1 23R2 2R1 2 6Q3 2R1 Q23 23R2 Q69
2R1 2 6Q3 2R1 Q23
END FILL
ARA=2 NUX=3 NUY=1 NUZ=1 FILL 4 3 4 END FILL
ARA=3 NUX=1 NUY=3 NUZ=1 FILL 6 5 6
END FILL END ARRAY
READ BIAS ID=500 2 6 END BIAS
READ PLOT TTL=' X-Y' PIC=MIX
XUL=0 YUL=72 ZUL=15 XLR=72 YLR=0 ZLR=15
UAX=1 VDN=-1 NAX=125 END
TTL=' X-Y' PIC=WTS END
TTL=' Y-Z' PIC=MIX
XUL=33 YUL=0 ZUL=40 XLR=33 YLR=72 ZLR=-14.1
VAX=1 WDN=-1 UAX=0 VDN=0 NAX=125 END
TTL=' Y-Z' PIC=WTS END
END PLOT
END DATA
END

```

Table A.1 (continued)

```

CAA09
=CSAS25
LIBBY EXP. 4.89% RODS 30 CM LONG, .762 CM DIAM, 1.3 CM PITCH
27GROUPNDF4 LATTICECELL
URANIUM 1 .9995 293 92235 4.89 92238 95.11 END
H2O 2 1 END
PLEXIGLASS 3 1 END
PB 4 1 END
SS304 5 1 END
END COMP
SQUAREPITCH 1.3 .762 1 2 END
LIBBY H2O REFL. CASE 28A PB 4 FACES, SS PLATE IN CENTER
READ PARAM NPG=600 NUB=YES PLT=NO FDN=YES END PARAM
READ GEOM
UNIT 1
CYLINDER 1 1 .381 30 0
CUBOID 2 1 4P.65 30 0
UNIT 2
CUBOID 2 1 4P.65 30 0
UNIT 3
ARRAY 1 3R0
REFLECTOR 2 1 0 3R.62 2R0 1
UNIT 7
ARRAY 4 3R0
REFLECTOR 2 1 .62 0 2R.62 2R0 1
UNIT 8
CUBOID 5 1 2P.3175 2P15.57 25.4 0
REFLECTOR 2 1 2R.3325 2R0 1.425 3.175 1
UNIT 4
CUBOID 4 1 2P10.16 2P15.57 25.4 0
REFLECTOR 2 2 4R0 1.425 0 1
REFLECTOR 3 2 5R0 3.175 1
UNIT 5
ARRAY 2 3R0
UNIT 6
CUBOID 4 1 2P35.89 2P10.16 25.4 0
REFLECTOR 2 2 4R0 1.425 0 1
REFLECTOR 3 2 5R0 3.175 1
ARRAY 3 3R0
REFLECTOR 2 2 4R0 3 0 5
REFLECTOR 2 6 4R0 1 0 1
REFLECTOR 3 2 5R0 3 4
REFLECTOR 3 6 5R0 1.97 1
END GEOM
READ ARRAY ARA=1 NUX=11 NUY=23 NUZ=1 FILL
2 1 2 2R1 2Q3 2R1 2 2R1 2Q3 11R2 2R1 2 2R1 2Q3 Q11 6Q33
END FILL
ARA=4 NUX=11 NUY=23 NUZ=1 FILL
2R1 2 2R1 2Q3 Q11 11R2 2R1 2 2R1 2Q3 Q11 6Q33
END FILL
ARA=2 NUX=5 NUY=1 NUZ=1 FILL 4 3 8 7 4 END FILL
ARA=3 NUX=1 NUY=3 NUZ=1 FILL 6 5 6
END FILL END ARRAY
READ BIAS ID=500 2 6 END BIAS
READ PLOT TTL=' X-Y' PIC=MIX
XUL=0 YUL=72 ZUL=15 XLR=72 YLR=0 ZLR=15
UAX=1 VDN=-1 NAX=125 END
TTL=' X-Y' PIC=WTS END
TTL=' Y-Z' PIC=MIX
XUL=33 YUL=0 ZUL=40 XLR=33 YLR=72 ZLR=-14.1
VAX=1 WDN=-1 UAX=0 VDN=0 NAX=125 END
TTL=' Y-Z' PIC=WTS END
END PLOT
END DATA
END

```

```

CAA10
=CSAS25
LIBBY EXP. 4.89% RODS 30 CM LONG, .762 CM DIAM, 1.3 CM PITCH
27GROUPNDF4 LATTICECELL
URANIUM 1 .9995 293 92235 4.89 92238 95.11 END
H2O 2 1 END
PLEXIGLASS 3 1 END
PB 4 1 END
B-10 5 0 4.617-3 END
B-11 5 0 1.872-2 END
C 5 0 5.750-3 END
AL 5 0 4.765-2 END
END COMP
SQUAREPITCH 1.3 .762 1 2 END
LIBBY H2O REFL. CASE 30C PB 4 FACES, BORAL PLATE 6TH ROW
READ PARAM NPG=600 NUB=YES PLT=NO FDN=YES END PARAM
READ GEOM
UNIT 1
CYLINDER 1 1 .381 30 0
CUBOID 2 1 4P.65 30 0
UNIT 2
CUBOID 2 1 4P.65 30 0
UNIT 3
ARRAY 1 3R0
REFLECTOR 2 1 2R.62 0 .62 2R0 1
UNIT 7
ARRAY 4 3R0
REFLECTOR 2 1 3R.62 0 2R0 1
UNIT 8
CUBOID 5 1 2P15.57 2P.3175 25.4 0
REFLECTOR 2 1 2R0 2R.3325 1.425 3.175 1
UNIT 4
CUBOID 4 1 2P10.16 2P15.57 25.4 0
REFLECTOR 2 2 4R0 1.425 0 1
REFLECTOR 3 2 5R0 3.175 1
UNIT 9
ARRAY 5 3R0
UNIT 5
ARRAY 2 3R0
UNIT 6
CUBOID 4 1 2P35.89 2P10.16 25.4 0
REFLECTOR 2 2 4R0 1.425 0 1
REFLECTOR 3 2 5R0 3.175 1
ARRAY 3 3R0
REFLECTOR 2 2 4R0 3 0 1
REFLECTOR 2 3 4R0 1.8 0 1
REFLECTOR 3 2 5R0 3 4
REFLECTOR 3 6 5R0 1.97 1
END GEOM
READ ARRAY ARA=1 NUX=23 NUY=17 NUZ=1 FILL
2R2 19R1 2R2 2 21R1 2 F1
END FILL
ARA=4 NUX=23 NUY=5 NUZ=1 FILL
69R1 2 21R1 2 2R2 19R1 2R2
END FILL
ARA=5 NUX=1 NUY=3 NUZ=1 FILL 3 8 7 END FILL
ARA=2 NUX=3 NUY=1 NUZ=1 FILL 4 9 4 END FILL
ARA=3 NUX=1 NUY=3 NUZ=1 FILL 6 5 6
END FILL END ARRAY
READ BIAS ID=500 2 6 END BIAS
READ PLOT TTL=' X-Y' PIC=MIX
XUL=0 YUL=72 ZUL=15 XLR=72 YLR=0 ZLR=15
UAX=1 VDN=-1 NAX=125 END
TTL=' X-Y' PIC=WTS END
TTL=' Y-Z' PIC=MIX

```

Table A.1 (continued)

XUL=33 YUL=0 ZUL=40 XLR=33 YLR=72 ZLR=-14.1
 TTL=' Y-Z' PIC=WTS END
 END PLOT
 END DATA
 END

CAA11
 =CSAS25
 LIBBY EXP. 4.89% RODS 30 CM LONG, .762 CM DIAM, 1.3 CM PITCH
 27GROUPNDF4 LATTICECELL
 URANIUM 1 .9995 293 92235 4.89 92238 95.11 END
 H2O 2 1 END
 PLEXIGLASS 3 1 END
 PB 4 1 END
 CD 5 1 END
 END COMP
 SQUAREPITCH 1.3 .762 1 2 END
 LIBBY H2O REFL. CASE 31C PB 4 FACES, CD PLATE 6TH ROW
 READ PARAM NPG=600 NUB=YES PLT=NO FDN=YES END PARAM
 READ GEOM
 UNIT 1
 CYLINDER 1 1 .381 30 0
 CUBOID 2 1 4P.65 30 0
 UNIT 2
 CUBOID 2 1 4P.65 30 0
 UNIT 3
 ARRAY 1 3R0
 REFLECTOR 2 1 2R.62 0 .62 2R0 1
 UNIT 7
 ARRAY 4 3R0
 REFLECTOR 2 1 3R.62 0 2R0 1
 UNIT 8
 CUBOID 5 1 2P15.57 2P.04445 25.4 0
 REFLECTOR 2 1 2R0 2R.60555 1.425 3.175 1
 UNIT 4
 CUBOID 4 1 2P10.16 2P15.57 25.4 0
 REFLECTOR 2 2 4R0 1.425 0 1
 REFLECTOR 3 2 5R0 3.175 1
 UNIT 9
 ARRAY 5 3R0
 UNIT 5
 ARRAY 2 3R0
 UNIT 6
 CUBOID 4 1 2P35.89 2P10.16 25.4 0
 REFLECTOR 2 2 4R0 1.425 0 1
 REFLECTOR 3 2 5R0 3.175 1
 ARRAY 3 3R0
 REFLECTOR 2 2 4R0 .5 0 1
 REFLECTOR 3 2 5R0 3 4
 REFLECTOR 3 6 5R0 1.97 1
 END GEOM
 READ ARRAY ARA=1 NUX=23 NUY=17 NUZ=1 FILL
 11R1 12R2 F1
 END FILL
 ARA=4 NUX=23 NUY=5 NUZ=1 FILL
 F1
 END FILL
 ARA=5 NUX=1 NUY=3 NUZ=1 FILL 3 8 7 END FILL
 ARA=2 NUX=3 NUY=1 NUZ=1 FILL 4 9 4 END FILL
 ARA=3 NUX=1 NUY=3 NUZ=1 FILL 6 5 6
 END FILL END ARRAY

READ BIAS ID=500 2 6 END BIAS
 READ PLOT TTL=' X-Y' PIC=MIX
 XUL=0 YUL=72 ZUL=15 XLR=72 YLR=0 ZLR=15
 UAX=1 VDN=-1 NAX=125 END
 TTL=' X-Y' PIC=WTS END
 TTL=' Y-Z' PIC=MIX
 XUL=33 YUL=0 ZUL=40 XLR=33 YLR=72 ZLR=-14.1
 VAX=1 WDN=-1 UAX=0 VDN=0 NAX=125 END
 TTL=' Y-Z' PIC=WTS END
 END PLOT
 END DATA
 END
 L

CAA12
 =CSAS25
 LIBBY EXP. 4.89% RODS 30 CM LONG, .762 CM DIAM, 2.05 CM PITCH IN UO2F2 SOLN
 27GROUPNDF4 LATTICECELL
 URANIUM 1 .9995 293 92235 4.89 92238 95.11 END
 SOLNUO2F2 2 295.54 0 1 293 92235 4.89 92238 95.11 END
 PLEXIGLASS 3 1 END
 AL 4 1 END
 SOLNUO2F2 5 295.54 0 1 293 92235 4.89 92238 95.11 END
 END COMP
 SQUAREPITCH 2.05 .762 1 2 END
 LIBBY RODS IN UO2F2 SOLN CASE 32S
 READ PARAM NPG=600 NUB=YES FDN=YES END PARAM
 READ GEOM
 UNIT 1
 CYLINDER 1 1 .381 5.08 0
 CUBOID 5 1 4P1.025 5.08 0
 UNIT 2
 CYLINDER 1 1 .381 1.27 0
 CUBOID 3 1 4P1.025 1.27 0
 UNIT 3
 CYLINDER 1 1 .381 17.935 0
 CUBOID 5 1 4P1.025 17.935 0
 UNIT 4
 CYLINDER 1 1 .381 .635 0
 CUBOID 3 1 4P1.025 .635 0
 UNIT 5
 CUBOID 2 1 4P1.025 5.08 0
 UNIT 6
 CYLINDER 2 1 .381 1.27 0
 CUBOID 3 1 4P1.025 1.27 0
 UNIT 7
 CUBOID 2 1 4P1.025 17.935 0
 UNIT 8
 CYLINDER 2 1 .381 .635 0
 CUBOID 3 1 4P1.025 .635 0
 CORE 0 1 -11.275 -12.3 0
 REFLECTOR 3 1 5R0 3.81 1
 CYLINDER 5 1 47.94 30.1 -7.4
 CYLINDER 4 1 48.26 30.1 -7.72
 END GEOM
 READ ARRAY NUX=11 NUY=12 NUZ=5 FILL
 132R1 132R2 132R3 132R4 132R1
 END FILL END ARRAY
 END DATA
 END

Table A.1 (continued)

```

CAA13
=CSAS25
LIBBY EXP. 4.89% RODS 30 CM LONG, .762 CM DIAM, 2.05 CM PITCH IN UO2F2 SOLN
27GROUPNDF4 LATTICECELL
URANIUM 1 .9995 293 92235 4.89 92238 95.11 END
SOLNUO2F2 2 295.54 0 1 293 92235 4.89 92238 95.11 END
PLEXIGLASS 3 1 END
AL 4 1 END
SOLNUO2F2 5 295.54 0 1 293 92235 4.89 92238 95.11 END
END COMP
SQUAREPITCH 2.05 .762 1 2 END
LIBBY RODS IN UO2F2 SOLN CASE 33S
READ PARAM NPG=600 FAR=YES NUB=YES FDN=YES END PARAM
READ GEOM
UNIT 1
CYLINDER 1 1 .381 5.08 0
CUBOID 5 1 4P1.025 5.08 0
UNIT 2
CYLINDER 1 1 .381 1.27 0
CUBOID 3 1 4P1.025 1.27 0
UNIT 3
CYLINDER 1 1 .381 17.935 0
CUBOID 5 1 4P1.025 17.935 0
UNIT 4
CYLINDER 1 1 .381 .635 0
CUBOID 3 1 4P1.025 .635 0
UNIT 5
CUBOID 2 1 4P1.025 5.08 0
UNIT 6
CYLINDER 2 1 .381 1.27 0
CUBOID 3 1 4P1.025 1.27 0
UNIT 7
CUBOID 2 1 4P1.025 17.935 0
UNIT 8
CYLINDER 2 1 .381 .635 0
CUBOID 3 1 4P1.025 .635 0
CORE 0 1 -9.225 -10.25 0
REFLECTOR 3 1 5R0 3.81 1
CYLINDER 5 1 47.94 48.65 -7.4
CYLINDER 4 1 48.26 48.65 -7.72
END GEOM
READ ARRAY NUX=9 NUY=10 NUZ=5 FILL
90R1 90R2 90R3 90R4 90R1
END FILL END ARRAY
END DATA
END

CAA14
=CSAS25
LIBBY EXP. 4.89% RODS 30 CM LONG, .762 CM DIAM, 3.25 CM PITCH IN UO2F2 SOLN
27GROUPNDF4 LATTICECELL
URANIUM 1 .9995 293 92235 4.89 92238 95.11 END
SOLNUO2F2 2 301.16 0 1 293 92235 4.89 92238 95.11 END
PLEXIGLASS 3 1 END
AL 4 1 END
SOLNUO2F2 5 301.16 0 1 293 92235 4.89 92238 95.11 END
END COMP
SQUAREPITCH 3.25 .762 1 2 END
LIBBY RODS IN UO2F2 SOLN CASE 36S
READ PARAM NPG=600 FAR=YES NUB=YES FDN=YES END PARAM
READ GEOM

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```

UNIT 1
CYLINDER 1 1 .381 5.08 0
CUBOID 5 1 4P1.625 5.08 0
UNIT 2
CYLINDER 1 1 .381 1.27 0
CUBOID 3 1 4P1.625 1.27 0
UNIT 3
CYLINDER 1 1 .381 17.935 0
CUBOID 5 1 4P1.625 17.935 0
UNIT 4
CYLINDER 1 1 .381 .635 0
CUBOID 3 1 4P1.625 .635 0
UNIT 5
CUBOID 2 1 4P1.625 5.08 0
UNIT 6
CYLINDER 2 1 .381 1.27 0
CUBOID 3 1 4P1.625 1.27 0
UNIT 7
CUBOID 2 1 4P1.625 17.935 0
UNIT 8
CYLINDER 2 1 .381 .635 0
CUBOID 3 1 4P1.625 .635 0
CORE 0 1 -14.625 -16.25 0
REFLECTOR 3 1 5R0 3.81 1
CYLINDER 5 1 47.94 38.52 -10.16
CYLINDER 4 1 48.26 38.52 -10.48
END GEOM
READ ARRAY NUX=9 NUY=10 NUZ=5 FILL
90R1 90R2 90R3 90R4 90R1
END FILL END ARRAY
END DATA
END

```

```

CAA15
=CSAS25
LIBBY EXP. 4.89% RODS 30 CM LONG, 1.31 CM DIAM, 2.99 CM PITCH IN UO2F2 SOLN
27GROUPNDF4 LATTICECELL
URANIUM 1 .9995 293 92235 4.89 92238 95.11 END
SOLNUO2F2 2 300.24 0 1 293 92235 4.89 92238 95.11 END
PLEXIGLASS 3 1 END
AL 4 1 END
SOLNUO2F2 5 300.24 0 1 293 92235 4.89 92238 95.11 END
END COMP
SQUAREPITCH 2.99 1.31 1 2 END
LIBBY RODS IN UO2F2 SOLN CASE 40S
READ PARAM NPG=600 FAR=YES NUB=YES FDN=YES END PARAM
READ GEOM
UNIT 1
CYLINDER 1 1 .655 5.08 0
CUBOID 5 1 4P1.495 5.08 0
UNIT 2
CYLINDER 1 1 .655 1.27 0
CUBOID 3 1 4P1.495 1.27 0
UNIT 3
CYLINDER 1 1 .655 17.935 0
CUBOID 5 1 4P1.495 17.935 0
UNIT 4
CYLINDER 1 1 .655 .635 0
CUBOID 3 1 4P1.495 .635 0
UNIT 5
CUBOID 2 1 4P1.495 5.08 0

```


Table A.1 (continued)

```

UNIT 6
CYLINDER 2 1 .655 1.27 0
CUBOID 3 1 4P1.495 1.27 0
UNIT 7
CUBOID 2 1 4P1.495 17.935 0
UNIT 8
CYLINDER 2 1 .655 .635 0
CUBOID 3 1 4P1.495 .635 0
CORE 0 1 -8.97 -10.465 0
REFLECTOR 3 1 5R0 3.81 1
CYLINDER 5 1 47.94 43.95 -10.16
CYLINDER 4 1 48.26 43.95 -10.48
END GEOM
READ ARRAY NUX=6 NUY=7 NUZ=5 FILL
42R1 42R2 42R3 42R4 42R1
END FILL END ARRAY
END DATA
END

```

```

CAA16
=CSAS25
LIBBY EXP. 4.89% RODS 30 CM LONG, 1.31 CM DIAM, 3.40 CM PITCH IN UO2F2 SOLN
27GROUPNDF4 LATTICECELL
URANIUM 1 .9995 293 92235 4.89 92238 95.11 END
SOLNUO2F2 2 300.24 0 1 293 92235 4.89 92238 95.11 END
PLEXIGLASS 3 1 END
AL 4 1 END
SOLNUO2F2 5 300.24 0 1 293 92235 4.89 92238 95.11 END
END COMP
SQUAREPITCH 3.40 1.31 1 2 END
LIBBY RODS IN UO2F2 SOLN CASE 42S
READ PARAM NPG=600 FAR=YES NUB=YES FDN=YES END PARAM
READ GEOM
UNIT 1
CYLINDER 1 1 .655 5.08 0
CUBOID 5 1 4P1.70 5.08 0
UNIT 2
CYLINDER 1 1 .655 1.27 0
CUBOID 3 1 4P1.70 1.27 0
UNIT 3
CYLINDER 1 1 .655 17.935 0
CUBOID 5 1 4P1.70 17.935 0
UNIT 4
CYLINDER 1 1 .655 .635 0
CUBOID 3 1 4P1.70 .635 0
UNIT 5
CUBOID 2 1 4P1.70 5.08 0
UNIT 6
CYLINDER 2 1 .655 1.27 0
CUBOID 3 1 4P1.70 1.27 0
UNIT 7
CUBOID 2 1 4P1.70 17.935 0
UNIT 8
CYLINDER 2 1 .655 .635 0
CUBOID 3 1 4P1.70 .635 0
CORE 0 1 -10.2 -11.9 0
REFLECTOR 3 1 5R0 3.81 1
CYLINDER 5 1 47.94 39.1 -10.16
CYLINDER 4 1 48.26 39.1 -10.48
END GEOM
READ ARRAY NUX=6 NUY=7 NUZ=5 FILL
42R1 42R2 42R3 42R4 42R1
END FILL END ARRAY
END DATA
END

```

```

CAA17
=CSAS25
LIBBY EXP. 4.89% RODS 30 CM LONG, 1.31 CM DIAM, 3.940 CM PITCH IN UO2F2 SOLN
27GROUPNDF4 LATTICECELL
URANIUM 1 .9995 293 92235 4.89 92238 95.11 END
SOLNUO2F2 2 300.24 0 1 293 92235 4.89 92238 95.11 END
PLEXIGLASS 3 1 END
AL 4 1 END
SOLNUO2F2 5 300.24 0 1 293 92235 4.89 92238 95.11 END
END COMP
SQUAREPITCH 3.94 1.31 1 2 END
LIBBY RODS IN UO2F2 SOLN CASE 44S
READ PARAM NPG=600 FAR=YES NUB=YES FDN=YES END PARAM
READ GEOM
UNIT 1
CYLINDER 1 1 .655 5.08 0
CUBOID 5 1 4P1.97 5.08 0
UNIT 2
CYLINDER 1 1 .655 1.27 0
CUBOID 3 1 4P1.97 1.27 0
UNIT 3
CYLINDER 1 1 .655 17.935 0
CUBOID 5 1 4P1.97 17.935 0
UNIT 4
CYLINDER 1 1 .655 .635 0
CUBOID 3 1 4P1.97 .635 0
UNIT 5
CUBOID 2 1 4P1.97 5.08 0
UNIT 6
CYLINDER 2 1 .655 1.27 0
CUBOID 3 1 4P1.97 1.27 0
UNIT 7
CUBOID 2 1 4P1.97 17.935 0
UNIT 8
CYLINDER 2 1 .655 .635 0
CUBOID 3 1 4P1.97 .635 0
CORE 0 1 -11.82 -13.79 0
REFLECTOR 3 1 5R0 3.81 1
CYLINDER 5 1 47.94 39.25 -10.16
CYLINDER 4 1 48.26 39.25 -10.48
END GEOM
READ ARRAY NUX=6 NUY=7 NUZ=5 FILL
42R1 42R2 42R3 42R4 42R1
END FILL END ARRAY
END DATA
END

```

Table A.1 (continued)

```

CAA18
=CSAS25
LIBBY EXP. 4.89% RODS 30 CM LONG, 1.31 CM DIAM, 4.40 CM PITCH IN UO2F2 SOLN
27GROUPNDF4 LATTICECELL
URANIUM 1 .9995 293 92235 4.89 92238 95.11 END
SOLNUO2F2 2 301.14 0 1 293 92235 4.89 92238 95.11 END
PLEXIGLASS 3 1 END
AL 4 1 END
SOLNUO2F2 5 301.14 0 1 293 92235 4.89 92238 95.11 END
END COMP
SQUAREPITCH 4.40 1.31 1 2 END
LIBBY RODS IN UO2F2 SOLN CASE 458
READ PARAM NPG=600 FAR=YES NUB=YES FDN=YES END PARAM
READ GEOM
UNIT 1
CYLINDER 1 1 .655 5.08 0
CUBOID 5 1 4P2.20 5.08 0
UNIT 2
CYLINDER 1 1 .655 1.27 0
CUBOID 3 1 4P2.20 1.27 0
UNIT 3
CYLINDER 1 1 .655 17.935 0
CUBOID 5 1 4P2.20 17.935 0
UNIT 4
CYLINDER 1 1 .655 .635 0
CUBOID 3 1 4P2.20 .635 0
UNIT 5
CUBOID 2 1 4P2.20 5.08 0
UNIT 6
CYLINDER 2 1 .655 1.27 0
CUBOID 3 1 4P2.20 1.27 0
UNIT 7
CUBOID 2 1 4P2.20 17.935 0
UNIT 8
CYLINDER 2 1 .655 .635 0
CUBOID 3 1 4P2.20 .635 0
CORE 0 1 -13.2 -15.4 0
REFLECTOR 3 1 5R0 3.81 1
CYLINDER 5 1 47.94 41.45 -10.16
CYLINDER 4 1 48.26 41.45 -10.48
END GEOM
READ ARRAY NUX=6 NUY=7 NUZ=5 FILL
42R1 42R2 42R3 42R4 42R1
END FILL END ARRAY
END DATA
END

```

```

CAA19
=CSAS25
4.89% GREEN BLOCKS H/U-235=244.6 55.5G U-235/L
27GROUPNDF4 MULTIREGION
U-234 1 0 5.8000-7 END
U-235 1 0 1.4220-4 END
U-238 1 0 2.7302-3 END
H 1 0 3.4782-2 END
C 1 0 1.8023-2 END
O 1 0 9.5585-3 END
AL 2 1 END
END COMP
SPHERICAL END
1 28 NOEXTERMOD END ZONE
4.89% GREEN BLOCKS UNREFLECTED CASE 1
READ PARAM NPG=600 NUB=YES FDN=YES END PARAM
READ GEOM

```

```

UNIT 1
CUBE 1 1 2P10.16
UNIT 2
CUBOID 1 1 4P10.16 2P6.604
END GEOM
READ ARRAY NUX=3 NUY=3 NUZ=3 FILL 18R1 9R2 END FILL END ARRAY
END DATA
END

```

```

CAA20
=CSAS25
4.89% GREEN BLOCKS H/U-235=395.0 40.6 G U-235/L
27GROUPNDF4 MULTIREGION
U-234 1 0 4.3000-7 END
U-235 1 0 1.0402-4 END
U-238 1 0 1.9972-3 END
H 1 0 4.1088-2 END
C 1 0 2.1291-2 END
O 1 0 7.8456-3 END
AL 2 1 END
END COMP
SPHERICAL END
1 28 NOEXTERMOD END ZONE
4.89% GREEN BLOCKS UNREFLECTED CASE 2
READ PARAM NPG=600 NUB=YES FDN=YES END PARAM
READ GEOM
CUBOID 1 1 50.8 0 60.96 0 60.452 0
END GEOM
END DATA
END

```

```

CAA21
=CSAS25
4.89% GREEN BLOCKS H/U-235=757.0 22.1 G U-235/L
27GROUPNDF4 MULTIREGION
U-234 1 0 2.3000-7 END
U-235 1 0 5.6624-5 END
U-238 1 0 1.0872-3 END
H 1 0 4.2864-2 END
C 1 0 2.2212-2 END
O 1 0 5.3889-3 END
AL 2 1 END
END COMP
SPHERICAL END
1 28 NOEXTERMOD END ZONE
4.89% GREEN BLOCKS UNREFLECTED CASE 3
READ PARAM NPG=600 NUB=YES FDN=YES END PARAM
READ GEOM
CUBOID 1 1 71.12 0 71.12 0 70.358 0
END GEOM
END DATA
END

```

Table A.1 (continued)

```

CAA22
=CSAS25
4.89% GREEN BLOCKS H/U-235=503.5 33.3 G U-235/L
27GROUPNDF4 MULTIREGION
U-234 1 0 3.5000-7 END
U-235 1 0 8.5320-5 END
U-238 1 0 1.6381-3 END
H 1 0 4.2959-2 END
C 1 0 2.2261-2 END
O 1 0 6.9399-3 END
AL 2 1 END
END COMP
SPHERICAL END
1 36 NOEXTERMOD END ZONE
4.89% GREEN BLOCKS UNREFLECTED CASE 4
READ PARAM NPG=600 NUB=YES FDN=YES END PARAM
READ GEOM
CUBOID 1 1 60.96 0 60.96 0 52.832 0
END GEOM
END DATA
END

CAA23
=CSAS25
4.89% GREEN BLOCKS H/U-235=199.3 64.9 G U-235/L
27GROUPNDF4 MULTIREGION
U-234 1 0 6.8000-7 END
U-235 1 0 1.6628-4 END
U-238 1 0 3.1926-3 END
H 1 0 3.3140-2 END
C 1 0 1.7173-2 END
O 1 0 1.0766-2 END
AL 2 1 END
H2O 3 1 END
PARAFFIN 4 1 END
END COMP
SPHERICAL END
1 22 ONEXTERMOD 3 40 NOEXTERMOD END ZONE
4.89% GREEN BLOCKS REFLECTED CASE 1
READ PARAM NPG=600 NUB=YES FDN=YES END PARAM
READ GEOM
UNIT 1
CUBE 1 1 2P10.16
UNIT 2
CUBOID 1 1 4P10.16 2P8.763
CORE 0 1 3R0.
REFLECTOR 4 8 4R0 3.048 0 5
REFLECTOR 3 2 4R3 0 3 6
END GEOM
READ ARRAY NUX=2 NUY=2 NUZ=3 FILL 8R1 4R2 END FILL END ARRAY
READ BIAS ID=500 2 7 ID=400 8 12 END BIAS
END DATA
END

```

```

CAA24
=CSAS25
4.89% GREEN BLOCKS H/U-235=244.8 56.2 G U-235/L
27GROUPNDF4 MULTIREGION
U-234 1 0 5.9000-7 END
U-235 1 0 1.4399-4 END
U-238 1 0 2.7647-3 END
H 1 0 3.5249-2 END
C 1 0 1.8265-2 END
O 1 0 9.6807-3 END
AL 2 1 END
H2O 3 1 END
PARAFFIN 4 1 END
END COMP
SPHERICAL END
1 22 ONEXTERMOD 3 40 NOEXTERMOD END ZONE
4.89% GREEN BLOCKS REFLECTED CASE 2
READ PARAM NPG=600 NUB=YES FDN=YES END PARAM
READ GEOM
CUBOID 1 1 40.64 0 40.64 0 57.912 0
REFLECTOR 4 8 4R0 3.048 0 5
REFLECTOR 3 2 4R3 0 3 6
END GEOM
READ BIAS ID=500 2 7 ID=400 8 12 END BIAS
END DATA
END

```

```

CAA25
=CSAS25
4.89 GREEN BLOCKS H/U-235=396.7 40.6 G U-235/L
27GROUPNDF4 MULTIREGION
U-234 1 0 4.3000-7 END
U-235 1 0 1.0402-4 END
U-238 1 0 1.9972-3 END
H 1 0 4.1265-2 END
C 1 0 2.1383-2 END
O 1 0 7.8552-3 END
AL 2 1 END
H2O 3 1 END
PARAFFIN 4 1 END
END COMP
SPHERICAL END
1 20 ONEXTERMOD 3 38 NOEXTERMOD END ZONE
4.89% GREEN BLOCKS REFLECTED CASE 3
READ PARAM NPG=600 NUB=YES FDN=YES END PARAM
READ GEOM
CUBOID 1 1 40.64 0 40.64 0 57.658 0
REFLECTOR 4 8 4R0 3.048 0 5
REFLECTOR 3 2 4R3 0 3 6
END GEOM
READ BIAS ID=500 2 7 ID=400 8 12 END BIAS
END DATA
END

```

Table A.1 (continued)

```

CAA27
=CSAS25
4.89% GREEN BLOCKS H/U-235=146.8 81.1 G U-235/L
27GROUPNDF4 MULTIREGION
U-234 1 0 8.5000-7 END
U-235 1 0 2.0779-4 END
U-238 1 0 3.9896-3 END
H 1 0 3.0504-2 END
C 1 0 1.5807-2 END
O 1 0 1.2859-2 END
AL 2 1 END
H2O 3 1 END
PARAFFIN 4 1 END
END COMP
SPHERICAL END
1 22 ONEXTERMOD 3 40 NOEXTERMOD END ZONE
4.89% GREEN BLOCKS REFLECTED CASE 5
READ PARAM NPG=600 NUB=YES FDN=YES END PARAM
READ GEOM
CUBOID 1 1 50.8 0 50.8 0 42.164 0
REFLECTOR 4 8 4R0 3.048 0 5
REFLECTOR 3 2 4R3 0 3 6
END GEOM
READ BIAS ID=500 2 7 ID=400 8 12 END BIAS
END DATA
END
    
```

```

CAA28
=CSAS25
4.89% GREEN BLOCKS H/U-235=82.7 107. G U-235/L
27GROUPNDF4 MULTIREGION
U-234 1 0 1.1300-6 END
U-235 1 0 2.7415-4 END
U-238 1 0 5.2637-3 END
H 1 0 2.2672-2 END
C 1 0 1.1748-2 END
O 1 0 1.6007-2 END
AL 2 1 END
H2O 3 1 END
PARAFFIN 4 1 END
END COMP
SPHERICAL END
1 26 ONEXTERMOD 3 44 NOEXTERMOD END ZONE
4.89% GREEN BLOCKS REFLECTED CASE 6
READ PARAM NPG=600 NUB=YES FDN=YES END PARAM
READ GEOM
CUBOID 1 1 50.8 0 60.96 0 56.134 0
REFLECTOR 4 8 4R0 3.048 0 5
REFLECTOR 3 2 4R3 0 3 6
END GEOM
READ BIAS ID=500 2 7 ID=400 8 12 END BIAS
END DATA
END
    
```

```

CAA26
=CSAS25
4.89% GREEN BLOCKS H/U-235=756.6 22.2 G U-235/L
27GROUPNDF4 MULTIREGION
U-234 1 0 2.3000-7 END
U-235 1 0 5.6880-5 END
U-238 1 0 1.0921-3 END
H 1 0 4.3035-2 END
C 1 0 2.2300-2 END
O 1 0 5.4119-3 END
AL 2 1 END
H2O 3 1 END
PARAFFIN 4 1 END
END COMP
SPHERICAL END
1 28 ONEXTERMOD 3 46 NOEXTERMOD END ZONE
4.89% GREEN BLOCKS REFLECTED CASE 4
READ PARAM NPG=600 NUB=YES FDN=YES END PARAM
READ GEOM
CUBOID 1 1 71.12 0 60.96 0 51.562 0
REFLECTOR 4 8 4R0 3.048 0 5
REFLECTOR 3 2 4R3 0 3 6
END GEOM
READ BIAS ID=500 2 7 ID=400 8 12 END BIAS
END DATA
END
    
```

```

CAA29
=CSAS25
4.89% GREEN BLOCKS H/U-235=504.1 33.3 G U-235/L
27GROUPNDF4 MULTIREGION
U-234 1 0 3.5000-7 END
U-235 1 0 8.5320-5 END
U-238 1 0 1.6381-3 END
H 1 0 4.3010-2 END
C 1 0 2.2287-2 END
O 1 0 6.9427-3 END
AL 2 1 END
H2O 3 1 END
PARAFFIN 4 1 END
END COMP
SPHERICAL END
1 29 ONEXTERMOD 3 47 NOEXTERMOD END ZONE
4.89% GREEN BLOCKS REFLECTED CASE 7
READ PARAM NPG=600 NUB=YES FDN=YES END PARAM
READ GEOM
CUBOID 1 1 50.8 0 50.8 0 41.148 0
REFLECTOR 4 8 4R0 3.048 0 5
REFLECTOR 3 2 4R3 0 3 6
END GEOM
READ BIAS ID=500 2 7 ID=400 8 12 END BIAS
END DATA
END
    
```

Table A.1 (continued)

```

CAA30
=CSAS25
4.89% UO2F2 H/U-235=524
27GROUPNDF4 MULTIREGION
SOLNUO2F2 1 869.9 0 1 293 92234 .02 92235 4.89
92238 95.09 END
SS304 2 1 END
END COMP
CYLINDRICAL END
1 25.4 NOEXTERMOD 2 25.56 NOEXTERMOD END ZONE
4.89% UO2F2 20 IN DIAM SS CYL BARE 1
READ PARAM NPG=600 NUB=YES FDN=YES END PARAM
READ GEOM
CYLINDER 1 1 25.4 38.66 0
CYLINDER 2 1 25.559 38.66 -.159
END GEOM
END DATA
END
    
```

```

CAA31
=CSAS25
4.89% UO2F2 H/U-235=524
27GROUPNDF4 MULTIREGION
SOLNUO2F2 1 869.9 0 1 293 92234 .02 92235 4.89
92238 95.09 END
AL 2 1 END
END COMP
CYLINDRICAL END
1 25.4 NOEXTERMOD 2 25.56 NOEXTERMOD END ZONE
4.89% UO2F2 20X20 IN AL BOX BARE 2
READ PARAM NPG=600 NUB=YES FDN=YES END PARAM
READ GEOM
CUBOID 1 1 4P25.25 35.9 0
CUBOID 2 1 4P25.409 35.9 -.159
END GEOM
END DATA
END
    
```

```

CAA32
=CSAS25
4.89% UO2F2 H/U-235=735
27GROUPNDF4 MULTIREGION
SOLNUO2F2 1 650.1 0 1 293 92234 .02 92235 4.89
92238 95.09 END
SS304 2 1 END
END COMP
CYLINDRICAL END
1 25.4 NOEXTERMOD 2 25.56 NOEXTERMOD END ZONE
4.89% UO2F2 20 IN DIAM SS CYL BARE 3
READ PARAM NPG=600 NUB=YES FDN=YES END PARAM
READ GEOM
CYLINDER 1 1 25.4 54.35 0
CYLINDER 2 1 25.559 54.35 -.159
END GEOM
END DATA
END
    
```

```

CAA33
=CSAS25
4.89% UO2F2 H/U-235=1002
27GROUPNDF4 MULTIREGION
SOLNUO2F2 1 491.6 0 1 293 92234 .02 92235 4.89
92238 95.09 END
AL 2 1 END
END COMP
SPHERICAL END
1 34.6 NOEXTERMOD 2 34.76 NOEXTERMOD END ZONE
4.89% UO2F2 27.3 IN DIAM AL SPHERE BARE 4
READ PARAM NPG=600 NUB=YES FDN=YES END PARAM
READ GEOM
HEMISPHE-Z 1 1 34.6 CHORD 30.
SPHERE 0 1 34.6
SPHERE 2 1 34.759
END GEOM
END DATA
END
    
```

```

CAA34
=CSAS25
4.89% UO2F2 H/U-235=991
27GROUPNDF4 MULTIREGION
SOLNUO2F2 1 496.5 0 1 293 92234 .02 92235 4.89
92238 95.09 END
AL 2 1 END
FLEXIGLASS 3 1 END
END COMP
CYLINDRICAL END
1 38.1 NOEXTERMOD 2 38.26 NOEXTERMOD END ZONE
4.89% UO2F2 30 IN DIAM SS CYL BARE 5
READ PARAM NPG=600 NUB=YES FDN=YES END PARAM
READ GEOM
CYLINDER 1 1 38.1 44.75 0
CYLINDER 2 1 38.259 44.75 -.159
CUBOID 0 1 4P60.96 44.75 -.159
REFLECTOR 3 1 5R0 2.54 1
END GEOM
END DATA
END
    
```

Table A.1 (continued)

```

CAA35
=CSAS25
4.89% UO2F2 H/U-235=524
27GROUPNDF4 MULTIREGION
SOLNUO2F2 1 869.9 0 1 293 92234 .02 92235 4.89
92238 95.09 END
SS304 2 1 END
H2O 3 1 END
END COMP
CYLINDRICAL END
1 19 ONEXTERMOD 2 19.2 NOEXTERMOD 3 37.2 NOEXTERMOD END ZONE
4.89% UO2F2 15 IN DIAM SS CYL REFL 1
READ PARAM NPG=600 NUB=YES FDN=YES END PARAM
READ GEOM
CYLINDER 1 1 19.05 50.37 0
CYLINDER 2 1 19.209 50.529 -.159
REFLECTOR 3 2 3R3 6
END GEOM
READ BIAS ID=500 2 7 END BIAS
END DATA
END

CAA36
=CSAS25
4.89% UO2F2 H/U-235=524
27GROUPNDF4 MULTIREGION
SOLNUO2F2 1 869.9 0 1 293 92234 .02 92235 4.89
92238 95.09 END
AL 2 1 END
H2O 3 1 END
END COMP
CYLINDRICAL END
1 25.4 ONEXTERMOD 2 25.56 NOEXTERMOD 3 43.56 NOEXTERMOD END ZONE
4.89% UO2F2 20X20 IN AL BOX REFL 2
READ PARAM NPG=600 NUB=YES FDN=YES END PARAM
READ GEOM
CUBOID 1 1 4P25.25 25.4 0
CUBOID 2 1 4P25.409 25.559 -.159
REFLECTOR 3 2 6R3 6
END GEOM
READ BIAS ID=500 2 7 END BIAS
END DATA
END

CAA37
=CSAS25
4.89% UO2F2 H/U-235=735
27GROUPNDF4 MULTIREGION
SOLNUO2F2 1 650.1 0 1 293 92234 .02 92235 4.89
92238 95.09 END
SS304 2 1 END
H2O 3 1 END
END COMP
CYLINDRICAL END
1 19 ONEXTERMOD 2 19.2 NOEXTERMOD 3 37.2 NOEXTERMOD END ZONE
4.89% UO2F2 15 IN DIAM SS CYL REFL 3
READ PARAM NPG=600 NUB=YES FDN=YES END PARAM
READ GEOM
CYLINDER 1 1 19.05 153.01 0
CYLINDER 2 1 19.209 153.169 -.159
REFLECTOR 3 2 3R3 6
END GEOM

```

```

READ BIAS ID=500 2 7 END BIAS
END DATA
END

```

```

CAA38
=CSAS25
4.89% UO2F2 H/U-235=1099
27GROUPNDF4 MULTIREGION
SOLNUO2F2 1 452.1 0 1 293 92234 .02 92235 4.89
92238 95.09 END
AL 2 1 END
H2O 3 1 END
END COMP
SPHERICAL END
1 34.6 ONEXTERMOD 2 34.76 NOEXTERMOD 3 52.76 NOEXTERMOD END ZONE
4.89% UO2F2 27.3 IN DIAM AL SPHERE REFL 4
READ PARAM NPG=600 NUB=YES FDN=YES END PARAM
READ GEOM
HEMISPHE-Z 1 1 34.6 CHORD 27.9
SPHERE 0 1 34.6
SPHERE 2 1 34.759
REFLECTOR 3 2 3. 6
END GEOM
READ BIAS ID=500 2 7 END BIAS
END DATA
END

```

```

CAA39
=CSAS25
4.89% UO2F2 H/U-235=994
27GROUPNDF4 MULTIREGION
SOLNUO2F2 1 495.3 0 1 293 92234 .02 92235 4.89
92238 95.09 END
SS304 2 1 END
H2O 3 1 END
END COMP
CYLINDRICAL END
1 25.4 ONEXTERMOD 2 25.56 NOEXTERMOD 3 43.56 NOEXTERMOD END ZONE
4.89% UO2F2 20 IN DIAM SS CYL REFL 5
READ PARAM NPG=600 NUB=YES FDN=YES END PARAM
READ GEOM
CYLINDER 1 1 25.4 85.72 0
CYLINDER 2 1 25.559 85.879 -.159
REFLECTOR 3 2 3R3 6
END GEOM
READ BIAS ID=500 2 7 END BIAS
END DATA
END

```

Table A.2. Table 2 input data

```

CAB01
=CSAS25
CASE EBJ.1 U(3.85) 15 @ 7.2"/0"/0"/77.8CM, SQUARE
27GROUPNDF4 INFHOMMEDIUM

' U(3.85) METAL
U-235      1 0.  1.8643E-3 END
U-238      1 0.  4.5971E-2 END

' FULL DENSITY WATER MODERATOR/REFLECTOR
H2O        2 1.0      END

' FIR TIMBER MODEL
C          3 0.  1.06802E-2 END
H          3 0.  2.21713E-2 END
O          3 0.  1.10850E-2 END

' STEEL FOR GRATING, TANK WALLS AND FLOOR
CARBONSTEEL 4 1.0      END

' STAINLESS STEEL LINING FOR TANK
SS304      5 1.0      END

END COMP
CASE EBJ.1 U(3.85) 15 @ 7.2"/0"/0"/77.8CM, SQUARE
READ PARM
NPG=600 PLT=NO FDN=YES NUB=YES TME=90 TBA=2
END PARM
READ GEOM

UNIT 1
COM=* FIR TIMBER 7.25" X 72" X 7.25" *
CUBOID 3 1 182.88 0. 18.415 0. 18.415 0.

UNIT 2
COM=* WATER GAP 3.5" X 72" X 7.25" BETWEEN TIMBERS *
CUBOID 2 1 182.88 0. 8.89 0. 18.415 0.

UNIT 3
COM=* ARRAY OF TIMBERS 72" X 72" X 7.25" *
ARRAY 1 3*0.0
REPLICATE 2 1 2R0. 2R0.3175 2R0. 1

UNIT 4
COM=* SECTION OF STEEL GRATING *
CUBOID 4 1 2.778125 .238125 .396875 -.396875 3.175 2.38125
CUBOID 2 1 2.778125 .238125 4.524375 -4.524375 3.175 0.
CUBOID 4 1 3.01625 0. 4.524375 -4.524375 3.175 0.

UNIT 5
COM=* ARRAY OF STEEL GRATING *
ARRAY 2 3*0.0
REPLICATE 2 1 4R0.9525 2R0.0 1

UNIT 6
COM=* U(3.85) ANNULUS WITH INSERT *
CYLINDER 1 1 3.175 76.2 0.
CYLINDER 2 1 3.302 76.2 0.
CYLINDER 1 1 9.144 76.2 0.
CUBOID 2 1 4P9.144 76.2 0.

```

```

UNIT 7
COM=* WATER CUBOID TO COMPLETE ANNULI ARRAY *
CUBOID 2 1 4P9.144 76.2 0.

UNIT 8
COM=* ARRAY OF 15 ANNULI WITH U(3.85) INSERTS *
ARRAY 3 3*0.0
REPLICATE 2 1 4R54.864 1.6 0. 1

CORE 4 1 -91.44 -91.44 0.
REPLICATE 2 1 4R30.48 2R0. 1
REPLICATE 5 1 5R0.0 0.1905 1
REPLICATE 4 1 5R0.0 2.54 1
END GEOM
READ ARRAY
ARA=1 NUX=1 NUY=13 NUZ=1
FILL 1 2 5Q2 1 END FILL
ARA=2 NUX=60 NUY=20 NUZ=1
FILL P4 END FILL
ARA=3 NUX=4 NUY=4 NUZ=1
LOOP 6 1 4 1 1 4 1 1 1 1
      7 4 4 1 1 1 1 1 1 1 END LOOP
GBL=4
ARA=4 NUX=1 NUY=1 NUZ=3
FILL 3 5 8 END FILL
END ARRAY
READ START
XSM=-36.576 XSP=36.576 YSM=-36.576 YSP=36.576 ZSM=21.59 ZSP=97.79
END START
READ PLOT

TTL="PLAN VIEW 1/6 SCALE OF CORE, Z=MIDLEVEL OF ANNULI/INSERTS"
XUL=-91.44 YUL=91.44 ZUL=59.69
XLR=91.44 YLR=-91.44 ZLR=59.69
UAX=1. VDN=-1. DLX=1.524 NCH=* U.WGSC* END

TTL="PLAN VIEW 1/6 SCALE OF CORE, Z=MIDLEVEL OF GRATING"
XUL=-91.44 YUL=91.44 ZUL=20.0025
XLR=91.44 YLR=-91.44 ZLR=20.0025
UAX=1. VDN=-1. DLX=1.524 NCH=* U.WGSC* END

TTL="PLAN VIEW 1/6 SCALE OF CORE, Z=MIDLEVEL OF FIR TIMBERS"
XUL=-91.44 YUL=91.44 ZUL=9.2075
XLR=91.44 YLR=-91.44 ZLR=9.2075
UAX=1. VDN=-1. DLX=1.524 NCH=* U.WGSC* END

TTL="PLAN VIEW 1/10 SCALE OF MOCKUP, Z=MIDLEVEL OF U UNITS"
XUL=-121.92 YUL=121.92 ZUL=59.69
XLR=121.92 YLR=-121.92 ZLR=59.69
UAX=1. VDN=-1. DLX=2.54 NCH=* U.WGSC* END

TTL="PLAN VIEW 2X SCALE OF SINGLE U UNIT, Z=MIDLEVEL OF UNIT"
XUL=0. YUL=18.288 ZUL=59.69
XLR=18.288 YLR=0. ZLR=59.69
UAX=1. VDN=-1. DLX=0.127 NCH=* U.WGSC* END

TTL="CROSS SECTION OF CORE 1/6 SCALE, Y=9.144"
XUL=-91.44 YUL=9.144 ZUL=102.
XLR=91.44 YLR=9.144 ZLR=0.
UAX=1. WDN=-1. DLX=1.524 NCH=* U.WGSC* END

```

Table A.2 (continued)

```
TTL="CROSS SECTION OF MOCKUP 1/10 SCALE,Y=9.144"
XUL=-121.92 YUL=9.144 ZUL=105.
XLR=121.92 YLR=9.144 ZLR=-65.
UAX=1. WDN=-1. DLX=2.54 NCH=* U.WGSC* END

TTL="CROSS SECTION OF GRATING/FIR TIMBERS, FULL SCALE"
XUL=0. YUL=0. ZUL=24.13
XLR=25.4 YLR=0. ZLR=-3.0
UAX=1. WDN=-1. DLX=.254 NCH=* U.WGSC* END

TTL="PLAN VIEW OF GRATING THRU TIEBARS, FULL SCALE"
XUL=0. YUL=25.4 ZUL=21.193
XLR=25.4 YLR=0. ZLR=21.193
UAX=1. VDN=-1. DLX=.254 NCH=* U.WGSC* END

TTL="PLAN VIEW OF GRATING @ GRATING MIDLEVEL, FULL SCALE"
XUL=0. YUL=25.4 ZUL=20.0025
XLR=25.4 YLR=0. ZLR=20.0025
UAX=1. VDN=-1. DLX=.254 NCH=* U.WGSC* END

TTL="PLAN VIEW OF TIMBERS @ TIMBER MIDLEVEL, FULL SCALE"
XUL=0. YUL=25.4 ZUL=9.2075
XLR=25.4 YLR=-25.4 ZLR=9.2075
UAX=1. VDN=-1. DLX=.254 NCH=* U.WGSC* END
END PLOT
END DATA
END

CABO2
=CSAS25
CASE EBJ.2X ( U(3.85) 11 @ 7.2"/0"/0.75"/72.4CM, SQUARE)
27GROUPNDF4 INFHOMMEDIUM

' U(3.85) METAL
U-235 1 0. 1.8643E-3 END
U-238 1 0. 4.5971E-2 END

' FULL DENSITY WATER MODERATOR/REFLECTOR
H2O 2 1.0 END

' FIR TIMBER MODEL
C 3 0. 1.06802E-2 END
H 3 0. 2.21713E-2 END
O 3 0. 1.10850E-2 END

' STEEL FOR GRATING, TANK WALLS AND FLOOR
CARBONSTEEL 4 1.0 END

' STAINLESS STEEL LINING FOR TANK
SS304 5 1.0 END

END COMP
CASE EBJ.2X RESTART EBJ.2 @ GENERATION # 11
READ PARM
NPG=600 PLT=NO NUB=YES FDN=YES TME=90 TBA=2
END PARM
READ GEOM
```

```
UNIT 1
COM=* FIR TIMBER 7.25" X 72" X 7.25" *
CUBOID 3 1 182.88 0. 18.415 0. 18.415 0.

UNIT 2
COM=* WATER GAP 3.5" X 72" X 7.25" BETWEEN TIMBERS *
CUBOID 2 1 182.88 0. 8.89 0. 18.415 0.

UNIT 3
COM=* ARRAY OF TIMBERS 72" X 72" X 7.25" PLUS 12" H2O *
ARRAY 1 3*0.0
REPLICATE 2 1 2R0. 2R0.3175 2R0. 1
REPLICATE 2 1 4R30.48 2R0. 1

UNIT 4
COM=* SECTION OF STEEL GRATING *
CUBOID 4 1 2.778125 .238125 .396875 -.396875 3.175 2.38125
CUBOID 2 1 2.778125 .238125 4.524375 -4.524375 3.175 0.
CUBOID 4 1 3.01625 0. 4.524375 -4.524375 3.175 0.

UNIT 5
COM=* ARRAY OF STEEL GRATING PLUS 12" H2O *
ARRAY 2 3*0.0
REPLICATE 2 1 4R0.9525 2R0.0 1
REPLICATE 2 1 4R30.48 2R0.0 1

UNIT 6
COM=* U(3.85) ANNULUS WITH INSERT (72.4 CM H) *
CYLINDER 1 1 3.175 72.4 0.
CYLINDER 2 1 3.302 72.4 0.
CYLINDER 1 1 9.144 72.4 0.
CUBOID 2 1 4P10.0965 72.4 0.

UNIT 7
COM=* WATER CUBOID TO COMPLETE ANNULI ARRAY (72.4 CM H) *
CUBOID 2 1 4P10.0965 72.4 0.

UNIT 8
COM=* ARRAY OF 11 ANNULI WITH U(3.85) INSERTS (72.4 CM H) *
ARRAY 3 3*0.0
REPLICATE 2 1 4R51.054 2R0. 1
REPLICATE 2 1 4R30.48 2R0.0 1

UNIT 9
COM=* U(3.85) ANNULUS WITH INSERT (3.8 CM H) *
CYLINDER 1 1 3.175 3.8 0.
CYLINDER 0 1 3.302 3.8 0.
CYLINDER 1 1 9.144 3.8 0.
CUBOID 0 1 4P10.0965 3.8 0.

UNIT 10
COM=* VOID CUBOID TO COMPLETE ANNULI ARRAY (3.8 CM H) *
CUBOID 0 1 4P10.0965 3.8 0.

UNIT 11
COM=* ARRAY OF 11 ANNULI WITH U(3.85) INSERTS (3.8 CM H) *
ARRAY 4 3*0.0
REPLICATE 0 1 4R51.054 2R0.0 1
REPLICATE 0 1 4R30.48 2R0.0 1
```


Table A.2 (continued)

```

CORE 5 1 -121.92 -121.92 0.
REPLICATE 5 1 5R0.0 0.1905 1
REPLICATE 4 1 5R0.0 2.54 1
END GEOM
READ ARRAY
ARA=1 NUX=1 NUY=13 NUZ=1
FILL 1 2 5Q2 1 END FILL
ARA=2 NUX=60 NUY=20 NUZ=1
FILL P4 BND FILL
ARA=3 NUX=4 NUY=4 NUZ=1
LOOP 6 1 4 1 1 4 1 1 1 1
      7 1 4 1 1 1 1 1 1 1
      7 4 4 1 2 2 1 1 1 1 END LOOP
ARA=4 NUX=4 NUY=4 NUZ=1
LOOP 9 1 4 1 1 4 1 1 1 1
      10 1 4 1 1 1 1 1 1 1
      10 4 4 1 2 2 1 1 1 1 END LOOP
GBL=5
ARA=5 NUX=1 NUY=1 NUZ=4
FILL 3 5 8 11 END FILL
END ARRAY
READ START
NST=6
LNU=200 TFX= 10.0965 TFY= 10.0965 TFZ=59.69
LNU=400 TFX=-10.0965 TFY= 10.0965 TFZ=59.69
LNU=470 TFX= 10.0965 TFY=-10.0965 TFZ=59.69
LNU=540 TFX=-10.0965 TFY=-10.0965 TFZ=59.59
LNU=610 TFX=-40.3856 TFY=-10.0965 TFZ=59.69
LNU=680 TFX=-40.3856 TFY= 10.0965 TFZ=59.69
LNU=750 TFX=-40.3856 TFY= 40.3856 TFZ=59.69
LNU=820 TFX=-10.0965 TFY= 40.3856 TFZ=59.69
LNU=890 TFX= 10.0965 TFY= 40.3856 TFZ=59.69
LNU=960 TFX= 40.3856 TFY= 40.3856 TFZ=59.69
LNU=1000 TFX= 40.3856 TFY= 10.0965 TFZ=59.69
END START
READ PLOT

TTL="PLAN VIEW 1/6 SCALE OF PALLET, Z=MIDLEVEL OF ANNULI/INSERTS"
XUL=-91.44 YUL=91.44 ZUL=59.69
XLR=91.44 YLR=-91.44 ZLR=59.69
UAX=1. VDN=-1. DLX=1.524 NCH=* U.WGSC* END

TTL="PLAN VIEW 1/6 SCALE OF PALLET, Z=MIDLEVEL OF GRATING"
XUL=-91.44 YUL=91.44 ZUL=20.0025
XLR=91.44 YLR=-91.44 ZLR=20.0025
UAX=1. VDN=-1. DLX=1.524 NCH=* U.WGSC* END

TTL="PLAN VIEW 1/6 SCALE OF PALLET, Z=MIDLEVEL OF FIR TIMBERS"
XUL=-91.44 YUL=91.44 ZUL=9.2075
XLR=91.44 YLR=-91.44 ZLR=9.2075
UAX=1. VDN=-1. DLX=1.524 NCH=* U.WGSC* END

TTL="PLAN VIEW 1/10 SCALE OF MOCKUP, Z=MIDLEVEL OF U UNITS"
XUL=-137. YUL=137. ZUL=59.69
XLR=137. YLR=-137. ZLR=59.69
UAX=1. VDN=-1. DLX=2.54 NCH=* U.WGSC* END

TTL="PLAN VIEW 2X SCALE OF SINGLE U UNIT, Z=MIDLEVEL OF UNIT"
XUL=0. YUL=20.193 ZUL=59.69
XLR=20.193 YLR=0. ZLR=59.69
UAX=1. VDN=-1. DLX=0.127 NCH=* U.WGSC* END

TTL="CROSS SECTION OF PALLET 1/6 SCALE,Y=10.0965"
XUL=-91.44 YUL=10.0965 ZUL=113.
XLR=91.44 YLR=10.0965 ZLR=-18.
UAX=1. WDN=-1. DLX=1.524 NCH=* U.WGSC* END

TTL="CROSS SECTION OF MOCKUP 1/10 SCALE,Y=10.0965"
XUL=-137. YUL=10.0965 ZUL=113.
XLR=137. YLR=10.0965 ZLR=-18.
UAX=1. WDN=-1. DLX=2.54 NCH=* U.WGSC* END

TTL="CROSS SECTION OF FLOOR/GRATING/FIR TIMBERS, FULL SCALE"
XUL=0. YUL=0. ZUL=24.13
XLR=25.4 YLR=0. ZLR=-5.4
UAX=1. WDN=-1. DLX=.254 NCH=* U.WGSC* END

TTL="PLAN VIEW OF GRATING THRU TIEBARS, FULL SCALE"
XUL=0. YUL=25.4 ZUL=21.193
XLR=25.4 YLR=0. ZLR=21.193
UAX=1. VDN=-1. DLX=.254 NCH=* U.WGSC* END

TTL="PLAN VIEW OF GRATING @ GRATING MIDLEVEL, FULL SCALE"
XUL=0. YUL=25.4 ZUL=20.0025
XLR=25.4 YLR=0. ZLR=20.0025
UAX=1. VDN=-1. DLX=.254 NCH=* U.WGSC* END

TTL="PLAN VIEW OF TIMBERS @ TIMBER MIDLEVEL, FULL SCALE"
XUL=0. YUL=25.4 ZUL=9.2075
XLR=25.4 YLR=-25.4 ZLR=9.2075
UAX=1. VDN=-1. DLX=.254 NCH=* U.WGSC* END

TTL="CROSS SECTION AT TOP OF UNITS, 2X SCALE"
XUL=0. YUL=10.0965 ZUL=105.
XLR=12.7 YLR=10.0965 ZLR=90.
UAX=1. WDN=-1. DLX=.127 NCH=* U.WGSC* END
END PLOT
END DATA
END

```

Table A.2 (continued)

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CAB03
=CSAS25
CASE EBJ.3X ( U(3.85) 24 @ 7.2"/0"/1.5"/75.0CM, SQUARE)
27GROUPNDF4 INFHOMMEDIUM

' U(3.85) METAL
U-235      1 0.  1.8643E-3 END
U-238      1 0.  4.5971E-2 END

' FULL DENSITY WATER MODERATOR/REFLECTOR
H2O        2 1.0      END

' FIR TIMBER MODEL
C           3 0.  1.06802E-2 END
H           3 0.  2.21713E-2 END
O           3 0.  1.10850E-2 END

' STEEL FOR GRATING, TANK WALLS AND FLOOR
CARBONSTEEL 4 1.0      END

' STAINLESS STEEL LINING FOR TANK
SS304      5 1.0      END

END COMP
CASE EBJ.3X
READ PARM
NPG=600 NUB=YES PLT=NO FDN=YES TME=90 TBA=2
END PARM
READ GEOM

UNIT 1
COM=* FIR TIMBER 7.25" X 72" X 7.25" *
CUBOID 3 1 182.88 0. 18.415 0. 18.415 0.

UNIT 2
COM=* WATER GAP 3.5" X 72" X 7.25" BETWEEN TIMBERS *
CUBOID 2 1 182.88 0. 8.89 0. 18.415 0.

UNIT 3
COM=* ARRAY OF TIMBERS 72" X 72" X 7.25" PLUS 12" H2O *
ARRAY 1 3*0.0
REPLICATE 2 1 2R0. 2R0.3175 2R0. 1
REPLICATE 2 1 4R30.48 2R0. 1

UNIT 4
COM=* SECTION OF STEEL GRATING *
CUBOID 4 1 2.778125 .238125 .396875 -.396875 3.175 2.38125
CUBOID 2 1 2.778125 .238125 4.524375 -4.524375 3.175 0.
CUBOID 4 1 3.01625 0. 4.524375 -4.524375 3.175 0.

UNIT 5
COM=* ARRAY OF STEEL GRATING PLUS 12" H2O *
ARRAY 2 3*0.0
REPLICATE 2 1 4R0.9525 2R0.0 1
REPLICATE 2 1 4R30.48 2R0.0 1

UNIT 6
COM=* U(3.85) ANNULUS WITH INSERT (75.0 CM H) *
CYLINDER 1 1 3.175 75.0 0.
CYLINDER 2 1 3.302 75.0 0.
CYLINDER 1 1 9.144 75.0 0.
CUBOID 2 1 4P11.049 75.0 0.

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UNIT 7
COM=* WATER CUBOID TO COMPLETE ANNULI ARRAY (75.0 CM H) *
CUBOID 2 1 4P11.049 75.0 0.

UNIT 8
COM=* ARRAY OF 24 ANNULI WITH U(3.85) INSERTS (75.0 CM H) *
ARRAY 3 3*0.0
REPLICATE 2 1 4R36.195 2R0. 1
REPLICATE 2 1 4R30.48 2R0.0 1

UNIT 9
COM=* U(3.85) ANNULUS WITH INSERT (1.2 CM H) *
CYLINDER 1 1 3.175 1.2 0.
CYLINDER 0 1 3.302 1.2 0.
CYLINDER 1 1 9.144 1.2 0.
CUBOID 0 1 4P11.049 1.2 0.

UNIT 10
COM=* VOID CUBOID TO COMPLETE ANNULI ARRAY (1.2 CM H) *
CUBOID 0 1 4P11.049 1.2 0.

UNIT 11
COM=* ARRAY OF 24 ANNULI WITH U(3.85) INSERTS (1.2 CM H) *
ARRAY 4 3*0.0
REPLICATE 0 1 4R36.195 2R0.0 1
REPLICATE 0 1 4R30.48 2R0.0 1

CORE 5 1 -121.92 -121.92 0.
REPLICATE 5 1 5R0.0 0.1905 1
REPLICATE 4 1 5R0.0 2.54 1
END GEOM
READ ARRAY
ARA=1 NUX=1 NUY=13 NUZ=1
FILL 1 2 5Q2 1 END FILL
ARA=2 NUX=60 NUY=20 NUZ=1
FILL F4 END FILL
ARA=3 NUX=5 NUY=5 NUZ=1
LOOP 6 1 5 1 1 5 1 1 1 1
7 5 5 1 1 1 1 1 1 1 END LOOP
ARA=4 NUX=5 NUY=5 NUZ=1
LOOP 9 1 5 1 1 5 1 1 1 1
10 5 5 1 1 1 1 1 1 1 1 END LOOP
GBL=5
ARA=5 NUX=1 NUY=1 NUZ=4
FILL 3 5 8 11 END FILL
END ARRAY
READ START
NST=1
XSM=-55.245 XSP=55.245 YSM=-55.245 YSP=55.245 ZSM=21.59 ZSP=97.79
END START
READ PLOT

TTL="PLAN VIEW 1/6 SCALE OF PALLET, Z=MIDLEVEL OF ANNULI/INSERTS"
XUL=-91.44 YUL=91.44 ZUL=59.69
XLR=91.44 YLR=-91.44 ZLR=59.69
UAX=1. VDN=-1. DLX=1.524 NCH=* U.WGSC* END

TTL="PLAN VIEW 1/6 SCALE OF PALLET, Z=MIDLEVEL OF GRATING"
XUL=-91.44 YUL=91.44 ZUL=20.0025
XLR=91.44 YLR=-91.44 ZLR=20.0025
UAX=1. VDN=-1. DLX=1.524 NCH=* U.WGSC* END

```

Table A.2 (continued)

TTL="PLAN VIEW 1/6 SCALE OF PALLET, Z=MIDLEVEL OF FIR TIMBERS"
 XUL=-91.44 YUL=91.44 ZUL=9.2075
 XLR=91.44 YLR=-91.44 ZLR=9.2075
 UAX=1. VDN=-1. DLX=1.524 NCH=* U.WGSC* END

TTL="PLAN VIEW 1/10 SCALE OF MOCKUP, Z=MIDLEVEL OF U UNITS"
 XUL=-137. YUL=137. ZUL=59.69
 XLR=137. YLR=-137. ZLR=59.69
 UAX=1. VDN=-1. DLX=2.54 NCH=* U.WGSC* END

TTL="PLAN VIEW 2X SCALE OF SINGLE U UNIT, Z=MIDLEVEL OF UNIT"
 XUL=-11.049 YUL=11.049 ZUL=59.69
 XLR=11.049 YLR=-11.049 ZLR=59.69
 UAX=1. VDN=-1. DLX=0.127 NCH=* U.WGSC* END

TTL="CROSS SECTION OF PALLET 1/6 SCALE,Y=0.0"
 XUL=-91.44 YUL=0.0 ZUL=113.
 XLR=91.44 YLR=0.0 ZLR=-18.
 UAX=1. WDN=-1. DLX=1.524 NCH=* U.WGSC* END

TTL="CROSS SECTION OF MOCKUP 1/10 SCALE,Y=0.0"
 XUL=-137. YUL=0.0 ZUL=113.
 XLR=137. YLR=0.0 ZLR=-18.
 UAX=1. WDN=-1. DLX=2.54 NCH=* U.WGSC* END

TTL="CROSS SECTION OF FLOOR/GRATING/FIR TIMBERS, FULL SCALE"
 XUL=0. YUL=0. ZUL=24.13
 XLR=25.4 YLR=0. ZLR=-5.4
 UAX=1. WDN=-1. DLX=.254 NCH=* U.WGSC* END

TTL="PLAN VIEW OF GRATING THRU TIEBARS, FULL SCALE"
 XUL=0. YUL=25.4 ZUL=21.193
 XLR=25.4 YLR=0. ZLR=21.193
 UAX=1. VDN=-1. DLX=.254 NCH=* U.WGSC* END

TTL="PLAN VIEW OF GRATING @ GRATING MIDLEVEL, FULL SCALE"
 XUL=0. YUL=25.4 ZUL=20.0025
 XLR=25.4 YLR=0. ZLR=20.0025
 UAX=1. VDN=-1. DLX=.254 NCH=* U.WGSC* END

TTL="PLAN VIEW OF TIMBERS @ TIMBER MIDLEVEL, FULL SCALE"
 XUL=0. YUL=25.4 ZUL=9.2075
 XLR=25.4 YLR=-25.4 ZLR=9.2075
 UAX=1. VDN=-1. DLX=.254 NCH=* U.WGSC* END

TTL="CROSS SECTION AT TOP OF UNITS, 2X SCALE"
 XUL=-11.049 YUL=0. ZUL=105.
 XLR=11.049 YLR=0. ZLR=90.
 UAX=1. WDN=-1. DLX=.127 NCH=* U.WGSC* END
 END PLOT
 END DATA
 END

CAB07
 =CSAS25
 CASE EBJ.4 U(3.85) 16 @ 7.2"/0"/0.25"/79.3CM, TRIANGULAR
 27GROUPNDF4 INPHOMMEDIUM

' U(3.85) METAL
 U-235 1 0. 1.8643E-3 END
 U-238 1 0. 4.5971E-2 END

' FULL DENSITY WATER MODERATOR/REFLECTOR
 H2O 2 1.0 END

' FIR TIMBER MODEL
 C 3 0. 1.06802E-2 END
 H 3 0. 2.21713E-2 END
 O 3 0. 1.10850E-2 END

' STEEL FOR GRATING, TANK WALLS AND FLOOR
 CARBONSTEEL 4 1.0 END

' STAINLESS STEEL LINING FOR TANK
 SS304 5 1.0 END

END COMP
 CASE EBJ.4 U(3.85) 16 @ 7.2"/0"/0.25"/79.3CM, TRIANGULAR
 READ PARM
 TBA=3 NPG=600 NUB=YES PLT=NO FDN=YES TME=90
 END PARM
 READ GEOM

UNIT 1
 COM=* FIR TIMBER 7.25" X 72" X 7.25" *
 CUBOID 3 1 182.88 0. 18.415 0. 18.415 0.

UNIT 2
 COM=* WATER GAP 3.5" X 72" X 7.25" BETWEEN TIMBERS *
 CUBOID 2 1 182.88 0. 8.89 0. 18.415 0.

UNIT 3
 COM=* ARRAY OF TIMBERS 72" X 72" X 7.25" *
 ARRAY 1 3*0.0
 REPLICATE 2 1 2R0. 2R0.3175 2R0. 1

UNIT 4
 COM=* SECTION OF STEEL GRATING *
 CUBOID 4 1 2.778125 .238125 .396875 -.396875 3.175 2.38125
 CUBOID 2 1 2.778125 .238125 4.524375 -4.524375 3.175 0.
 CUBOID 4 1 3.01625 0. 4.524375 -4.524375 3.175 0.

UNIT 5
 COM=* ARRAY OF STEEL GRATING *
 ARRAY 2 3*0.0
 REPLICATE 2 1 4R0.9525 2R0.0 1

UNIT 6
 COM=* U(3.85) ANNULUS WITH INSERT *
 CYLINDER 1 1 3.175 76.2 0.
 CYLINDER 2 1 3.302 76.2 0.
 CYLINDER 1 1 9.144 76.2 0.

Table A.2 (continued)

```

UNIT 7
COM=* ARRAY OF 16 ANNULI WITH U(3.85) INSERTS *
CUBOID 2 1 4P91.44 79.3 0.
HOLE 6 0.0 0.0 0.0
HOLE 6 -18.923 0.0 0.0
HOLE 6 -9.4615 16.3878 0.0
HOLE 6 9.4615 16.3878 0.0
HOLE 6 18.923 0.0 0.0
HOLE 6 9.4615 -16.3878 0.0
HOLE 6 -9.4615 -16.3878 0.0
HOLE 6 -28.3845 16.3878 0.0
HOLE 6 -18.923 32.7756 0.0
HOLE 6 0.0 32.7756 0.0
HOLE 6 28.3845 16.3878 0.0
HOLE 6 37.846 0.0 0.0
HOLE 6 28.3845 -16.3878 0.0
HOLE 6 0.0 -32.7756 0.0
HOLE 6 -18.923 -32.7756 0.0
HOLE 6 -28.3845 -16.3878 0.0

CORE 3 1 -91.44 -91.44 0.
REPLICATE 2 1 4R30.48 2R0. 1
REPLICATE 5 1 5R0.0 0.1905 1
REPLICATE 4 1 5R0.0 2.54 1
END GEOM
READ ARRAY
ARA=1 NUX=1 NUY=13 NUZ=1
FILL 1 2 5Q2 1 END FILL
ARA=2 NUX=60 NUY=20 NUZ=1
FILL F4 END FILL
GBL=3
ARA=3 NUX=1 NUY=1 NUZ=3
FILL 3 5 7 END FILL
END ARRAY
READ START
NST=1
XSM=-37.5285 XSP=46.99
YSM=-41.9196 YSP=41.9196
ZSM= 21.59 ZSP=97.79
END START
READ PLOT

TTL="PLAN VIEW 1/6 SCALE OF CORE, Z=MIDLEVEL OF ANNULI/INSERTS"
XUL=-91.44 YUL=91.44 ZUL=59.69
XLR=91.44 YLR=-91.44 ZLR=59.69
UAX=1. VDN=-1. DLX=1.524 NCH=* U.WGSC* END

TTL="PLAN VIEW 1/6 SCALE OF CORE, Z=MIDLEVEL OF GRATING"
XUL=-91.44 YUL=91.44 ZUL=20.0025
XLR=91.44 YLR=-91.44 ZLR=20.0025
UAX=1. VDN=-1. DLX=1.524 NCH=* U.WGSC* END

TTL="PLAN VIEW 1/6 SCALE OF CORE, Z=MIDLEVEL OF FIR TIMBERS"
XUL=-91.44 YUL=91.44 ZUL=9.2075
XLR=91.44 YLR=-91.44 ZLR=9.2075
UAX=1. VDN=-1. DLX=1.524 NCH=* U.WGSC* END

TTL="PLAN VIEW 1/10 SCALE OF MOCKUP, Z=MIDLEVEL OF U UNITS"
XUL=-121.92 YUL=121.92 ZUL=59.69
XLR=121.92 YLR=-121.92 ZLR=59.69
UAX=1. VDN=-1. DLX=2.54 NCH=* U.WGSC* END

TTL="PLAN VIEW FULL SCALE OF SINGLE U UNIT, Z=MIDLEVEL OF UNIT"
XUL=-16.75 YUL=16.75 ZUL=59.69
XLR=16.75 YLR=-16.75 ZLR=59.69
UAX=1. VDN=-1. DLX=0.254 NCH=* U.WGSC* END

TTL="CROSS SECTION OF CORE 1/6 SCALE,Y=0.0"
XUL=-91.44 YUL=0.0 ZUL=102.
XLR=91.44 YLR=0.0 ZLR=0.
UAX=1. WDN=-1. DLX=1.524 NCH=* U.WGSC* END

TTL="CROSS SECTION OF MOCKUP 1/10 SCALE,Y=0.0"
XUL=-121.92 YUL=0.0 ZUL=105.
XLR=121.92 YLR=0.0 ZLR=-65.
UAX=1. WDN=-1. DLX=2.54 NCH=* U.WGSC* END

TTL="CROSS SECTION OF GRATING/FIR TIMBERS, FULL SCALE"
XUL=0. YUL=0. ZUL=24.13
XLR=25.4 YLR=0. ZLR=-3.0
UAX=1. WDN=-1. DLX=.254 NCH=* U.WGSC* END

TTL="PLAN VIEW OF GRATING THRU TIEBARS, FULL SCALE"
XUL=0. YUL=25.4 ZUL=21.193
XLR=25.4 YLR=0. ZLR=21.193
UAX=1. VDN=-1. DLX=.254 NCH=* U.WGSC* END

TTL="PLAN VIEW OF GRATING @ GRATING MIDLEVEL, FULL SCALE"
XUL=0. YUL=25.4 ZUL=20.0025
XLR=25.4 YLR=0. ZLR=20.0025
UAX=1. VDN=-1. DLX=.254 NCH=* U.WGSC* END

TTL="PLAN VIEW OF TIMBERS @ TIMBER MIDLEVEL, FULL SCALE"
XUL=0. YUL=25.4 ZUL=9.2075
XLR=25.4 YLR=-25.4 ZLR=9.2075
UAX=1. VDN=-1. DLX=.254 NCH=* U.WGSC* END
END PLOT
END DATA
END

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Table A.2 (continued)

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CAB08
=CSAS25
CASE EBJ.5X ( U(3.85) 7 @ 7.2"/0"/1.0"/53.1CM, TRIANGULAR)
27GROUPNDF4 INFHOMMEDIUM

' U(3.85) METAL
U-235      1 0.  1.8643E-3 END
U-238      1 0.  4.5971E-2 END

' FULL DENSITY WATER MODERATOR/REFLECTOR
H2O        2 1.0      END

' FIR TIMBER MODEL
C           3 0.  1.06802E-2 END
H           3 0.  2.21713E-2 END
O           3 0.  1.10850E-2 END

' STEEL FOR GRATING, TANK WALLS AND FLOOR
CARBONSTEEL 4 1.0      END

' STAINLESS STEEL LINING FOR TANK
SS304      5 1.0      END

END COMP
CASE EBJ.5X
READ PARM
TBA=3 NPG=600 NUB=YES PLT=NO FDN=YES TME=90
END PARM
READ GEOM

UNIT 1
COM=* FIR TIMBER 7.25" X 72" X 7.25" *
CUBOID 3 1 182.88 0. 18.415 0. 18.415 0.

UNIT 2
COM=* WATER GAP 3.5" X 72" X 7.25" BETWEEN TIMBERS *
CUBOID 2 1 182.88 0. 8.89 0. 18.415 0.

UNIT 3
COM=* ARRAY OF TIMBERS 72" X 72" X 7.25" *
ARRAY 1 3*0.0
REPLICATE 2 1 2R0. 2R0.3175 2R0. 1
REPLICATE 2 1 4R30.48 2R0.0 1

UNIT 4
COM=* SECTION OF STEEL GRATING *
CUBOID 4 1 2.778125 .238125 .396875 -.396875 3.175 2.38125
CUBOID 2 1 2.778125 .238125 4.524375 -4.524375 3.175 0.
CUBOID 4 1 3.01625 0. 4.524375 -4.524375 3.175 0.

UNIT 5
COM=* ARRAY OF STEEL GRATING *
ARRAY 2 3*0.0
REPLICATE 2 1 4R0.9525 2R0.0 1
REPLICATE 2 1 4R30.48 2R0.0 1

UNIT 6
COM=* U(3.85) UNIT, FLOODED, H=1.905, LEVELS 1 AND 3 *
CYLINDER 1 1 3.175 1.905 0.
CYLINDER 2 1 3.302 1.905 0.
CYLINDER 1 1 9.144 1.905 0.

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UNIT 7
COM=* ARRAY OF 7 UNITS, FLOODED, H=1.905, LEVELS 1 AND 3 *
CUBOID 3 1 4P91.44 1.905 0.
HOLE 6 0.0 0.0 0.0
HOLE 6 -20.828 0.0 0.0
HOLE 6 -10.414 18.037577 0.0
HOLE 6 10.414 18.037577 0.0
HOLE 6 20.828 0.0 0.0
HOLE 6 10.414 -18.037577 0.0
HOLE 6 -10.414 -18.037577 0.0
REPLICATE 2 1 4R30.48 2R0.0 1

UNIT 8
COM=* U(3.85) UNIT, FLOODED, H=35.2425, LEVEL 2 *
CYLINDER 1 1 3.175 35.2425 0.
CYLINDER 2 1 3.302 35.2425 0.
CYLINDER 1 1 9.144 35.2425 0.

UNIT 9
COM=* ARRAY OF 7 UNITS, FLOODED, H=35.2425, LEVEL 2 *
CUBOID 2 1 4P91.44 35.2425 0.
HOLE 8 0.0 0.0 0.0
HOLE 8 -20.828 0.0 0.0
HOLE 8 -10.414 18.037577 0.0
HOLE 8 10.414 18.037577 0.0
HOLE 8 20.828 0.0 0.0
HOLE 8 10.414 -18.037577 0.0
HOLE 8 -10.414 -18.037577 0.0
REPLICATE 2 1 4R30.48 2R0.0 1

UNIT 10
COM=* U(3.85) UNIT, FLOODED, H=14.0475, LEVEL 4 *
CYLINDER 1 1 3.175 14.0475 0.
CYLINDER 2 1 3.302 14.0475 0.
CYLINDER 1 1 9.144 14.0475 0.

UNIT 11
COM=* ARRAY OF 7 UNITS, FLOODED, H=14.0475, LEVEL 4 *
CUBOID 2 1 4P91.44 14.0475 0.
HOLE 10 0.0 0.0 0.0
HOLE 10 -20.828 0.0 0.0
HOLE 10 -10.414 18.037577 0.0
HOLE 10 10.414 18.037577 0.0
HOLE 10 20.828 0.0 0.0
HOLE 10 10.414 -18.037577 0.0
HOLE 10 -10.414 -18.037577 0.0
REPLICATE 2 1 4R30.48 2R0.0 1

UNIT 12
COM=* U(3.85) UNIT, DRY, H=11.9875, LEVEL 5 *
CYLINDER 1 1 3.175 11.9875 0.
CYLINDER 0 1 3.302 11.9875 0.
CYLINDER 1 1 9.144 11.9875 0.

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Table A.2 (continued)

UNIT 13
 COM=* ARRAY OF 7 UNITS, DRY, H=11.9875, LEVEL 5 *
 CUBOID 0 1 4P91.44 11.9875 0.
 HOLE 12 0.0 0.0 0.0
 HOLE 12 -20.828 0.0 0.0
 HOLE 12 -10.414 18.037577 0.0
 HOLE 12 10.414 18.037577 0.0
 HOLE 12 20.828 0.0 0.0
 HOLE 12 10.414 -18.037577 0.0
 HOLE 12 -10.414 -18.037577 0.0
 REPLICATE 0 1 4R30.48 2R0.0 1

UNIT 14
 COM=* U(3.85) UNIT, DRY, H=1.905, LEVEL 6 *
 CYLINDER 1 1 3.175 1.905 0.
 CYLINDER 0 1 3.302 1.905 0.
 CYLINDER 1 1 9.144 1.905 0.

UNIT 15
 COM=* ARRAY OF 7 UNITS, DRY, H=1.905, LEVEL 6 *
 CUBOID 3 1 4P91.44 1.905 0.
 HOLE 14 0.0 0.0 0.0
 HOLE 14 -20.828 0.0 0.0
 HOLE 14 -10.414 18.037577 0.0
 HOLE 14 10.414 18.037577 0.0
 HOLE 14 20.828 0.0 0.0
 HOLE 14 10.414 -18.037577 0.0
 HOLE 14 -10.414 -18.037577 0.0
 REPLICATE 0 1 4R30.48 2R0.0 1

UNIT 16
 COM=* U(3.85) UNIT, DRY, H=9.2075, LEVEL 7 *
 CYLINDER 1 1 3.175 9.2075 0.
 CYLINDER 0 1 3.302 9.2075 0.
 CYLINDER 1 1 9.144 9.2075 0.

UNIT 17
 COM=* ARRAY OF 7 UNITS, DRY, H=9.2075, LEVEL 7 *
 CUBOID 0 1 4P91.44 9.2075 0.
 HOLE 16 0.0 0.0 0.0
 HOLE 16 -20.828 0.0 0.0
 HOLE 16 -10.414 18.037577 0.0
 HOLE 16 10.414 18.037577 0.0
 HOLE 16 20.828 0.0 0.0
 HOLE 16 10.414 -18.037577 0.0
 HOLE 16 -10.414 -18.037577 0.0
 REPLICATE 0 1 4R30.48 2R0.0 1

CORE 3 1 -121.92 -121.92 0.
 REPLICATE 5 1 5R0.0 0.1905 1
 REPLICATE 4 1 5R0.0 2.54 1
 END GEOM
 READ ARRAY
 ARA=1 NUX=1 NUY=13 NUZ=1
 FILL 1 2 5Q2 1 END FILL
 ARA=2 NUX=60 NUY=20 NUZ=1
 FILL #4 END FILL
 GBL=3
 ARA=3 NUX=1 NUY=1 NUZ=9
 FILL 3 5 7 9 7 11 13 15 17 END FILL
 END ARRAY

READ START
 NST=1
 XSM=-20.828 XSP=20.828
 YSM=-20.828 YSP=20.828
 ZSM= 21.59 ZSP=74.69
 END START
 READ PLOT

TTL="PLAN VIEW 1/6 SCALE OF CORE, Z=MIDLEVEL OF ANNULI/INSERTS"
 XUL=-100. YUL=100. ZUL=59.69
 XLR=100. YLR=-100. ZLR=59.69
 UAX=1. VDN=-1. DLX=1.524 NCH=* U.WGSC* END

TTL="PLAN VIEW 1/6 SCALE OF CORE, Z=MIDLEVEL OF GRATING"
 XUL=-100. YUL=100. ZUL=20.0025
 XLR=100. YLR=-100. ZLR=20.0025
 UAX=1. VDN=-1. DLX=1.524 NCH=* U.WGSC* END

TTL="PLAN VIEW 1/6 SCALE OF CORE, Z=MIDLEVEL OF FIR TIMBERS"
 XUL=-100. YUL=100. ZUL=9.2075
 XLR=100. YLR=-100. ZLR=9.2075
 UAX=1. VDN=-1. DLX=1.524 NCH=* U.WGSC* END

TTL="PLAN VIEW 1/10 SCALE OF MOCKUP, Z=MIDLEVEL OF U UNITS"
 XUL=-130. YUL=130. ZUL=59.69
 XLR=130. YLR=-130. ZLR=59.69
 UAX=1. VDN=-1. DLX=2.54 NCH=* U.WGSC* END

TTL="PLAN VIEW, FULL SCALE AT CENTER OF ARRAY, Z=MIDLEVEL "
 XUL=-16.75 YUL=16.75 ZUL=59.69
 XLR=16.75 YLR=-16.75 ZLR=59.69
 UAX=1. VDN=-1. DLX=0.254 NCH=* U.WGSC* END

TTL="CROSS SECTION OF CORE 1/6 SCALE, Y=0.0"
 XUL=-100. YUL=0.0 ZUL=102.
 XLR=100. YLR=0.0 ZLR=0.
 UAX=1. WDN=-1. DLX=1.524 NCH=* U.WGSC* END

TTL="CROSS SECTION OF MOCKUP 1/10 SCALE, Y=0.0"
 XUL=-130. YUL=0.0 ZUL=105.
 XLR=130. YLR=0.0 ZLR=-65.
 UAX=1. WDN=-1. DLX=2.54 NCH=* U.WGSC* END

TTL="CROSS SECTION OF GRATING/FIR TIMBERS, FULL SCALE"
 XUL=0. YUL=0. ZUL=24.13
 XLR=25.4 YLR=0. ZLR=-5.0
 UAX=1. WDN=-1. DLX=.254 NCH=* U.WGSC* END

TTL="PLAN VIEW OF GRATING THRU TIEBARS, FULL SCALE"
 XUL=0. YUL=25.4 ZUL=21.193
 XLR=25.4 YLR=0. ZLR=21.193
 UAX=1. VDN=-1. DLX=.254 NCH=* U.WGSC* END

TTL="PLAN VIEW OF GRATING @ GRATING MIDLEVEL, FULL SCALE"
 XUL=0. YUL=25.4 ZUL=20.0025
 XLR=25.4 YLR=0. ZLR=20.0025
 UAX=1. VDN=-1. DLX=.254 NCH=* U.WGSC* END

TTL="PLAN VIEW OF TIMBERS @ TIMBER MIDLEVEL, FULL SCALE"
 XUL=0. YUL=25.4 ZUL=9.2075
 XLR=25.4 YLR=-25.4 ZLR=9.2075
 UAX=1. VDN=-1. DLX=.254 NCH=* U.WGSC* END

Table A.2 (continued)

TTL="CROSS SECTION OF CENTRAL UNIT, 2X SCALE"
 XUL=0.0 YUL=0.0 ZUL=102.
 XLR=15.24 YLR=0.0 ZLR=-5.
 UAX=1. WDN=-1. DLX=0.127 NCH=* U.WGSC* END

END PLOT
 END DATA
 END

CAB09
 =CSAS25
 CASE EBJ.6X (U(3.85) 22 @ 7.2"/0"/2.35"/77.2CM, TRIANGULAR)
 27GROUPNDF4 INFHOMMEDIUM

' U(3.85) METAL
 U-235 1 0. 1.8643E-3 END
 U-238 1 0. 4.5971E-2 END

' FULL DENSITY WATER MODERATOR/REFLECTOR
 H2O 2 1.0 END

' FIR TIMBER MODEL
 C 3 0. 1.06802E-2 END
 H 3 0. 2.21713E-2 END
 O 3 0. 1.10850E-2 END

' STEEL FOR GRATING, TANK WALLS AND FLOOR
 CARBONSTEEL 4 1.0 END

' STAINLESS STEEL LINING FOR TANK
 SS304 5 1.0 END

END COMP
 CASE EBJ.6X
 READ FARM
 TBA=3 NPG=600 NUB=YES PLT=NO PDN=YES TME=90
 END FARM
 READ GEOM

UNIT 1
 COM=* FIR TIMBER 7.25" X 72" X 7.25" *
 CUBOID 3 1 182.88 0. 18.415 0. 18.415 0.

UNIT 2
 COM=* WATER GAP 3.5" X 72" X 7.25" BETWEEN TIMBERS *
 CUBOID 2 1 182.88 0. 8.89 0. 18.415 0.

UNIT 3
 COM=* ARRAY OF TIMBERS 72" X 72" X 7.25" *
 ARRAY 1 3*0.0
 REPLICATE 2 1 2R0. 2R0.3175 2R0. 1
 REPLICATE 2 1 4R30.48 2R0.0 1

UNIT 4
 COM=* SECTION OF STEEL GRATING *
 CUBOID 4 1 2.778125 .238125 .396875 -.396875 3.175 2.38125
 CUBOID 2 1 2.778125 .238125 4.524375 -4.524375 3.175 0.
 CUBOID 4 1 3.01625 0. 4.524375 -4.524375 3.175 0.

UNIT 5
 COM=* ARRAY OF STEEL GRATING *
 ARRAY 2 3*0.0
 REPLICATE 2 1 4R0.9525 2R0.0 1
 REPLICATE 2 1 4R30.48 2R0.0 1

UNIT 6
 COM=* U(3.85) UNIT, FLOODED, H=1.905, LEVELS 1, 3, AND 5 *
 CYLINDER 1 1 3.175 1.905 0.
 CYLINDER 2 1 3.302 1.905 0.
 CYLINDER 1 1 9.144 1.905 0.

UNIT 7
 COM=* ARRAY OF 22 UNITS, FLOODED, H=1.905, LEVELS 1, 3, AND 5 *
 CUBOID 3 1 4P91.44 1.905 0.
 HOLE 6 0.0 0.0 0.0
 HOLE 6 -24.257 0.0 0.0
 HOLE 6 -12.1285 21.007178 0.0
 HOLE 6 12.1285 21.007178 0.0
 HOLE 6 24.257 0.0 0.0
 HOLE 6 12.1285 -21.007178 0.0
 HOLE 6 -12.1285 -21.007178 0.0
 HOLE 6 -36.3855 -21.007178 0.0
 HOLE 6 -48.514 0.0 0.0
 HOLE 6 -36.3855 21.007178 0.0
 HOLE 6 -24.257 42.014356 0.0
 HOLE 6 0.0 42.014356 0.0
 HOLE 6 24.257 42.014356 0.0
 HOLE 6 36.3855 21.007178 0.0
 HOLE 6 48.514 0.0 0.0
 HOLE 6 36.3855 -21.007178 0.0
 HOLE 6 24.257 -42.014356 0.0
 HOLE 6 0.0 -42.014356 0.0
 HOLE 6 -24.257 -42.014356 0.0
 HOLE 6 -48.514 -42.014356 0.0
 HOLE 6 -12.1285 63.021534 0.0
 HOLE 6 60.6425 -21.007178 0.0
 REPLICATE 2 1 4R30.48 2R0.0 1

UNIT 8
 COM=* U(3.85) UNIT, FLOODED, H=35.2425, LEVEL 2 *
 CYLINDER 1 1 3.175 35.2425 0.
 CYLINDER 2 1 3.302 35.2425 0.
 CYLINDER 1 1 9.144 35.2425 0.

UNIT 9
 COM=* ARRAY OF 22 UNITS, FLOODED, H=35.2425, LEVEL 2 *
 CUBOID 2 1 4P91.44 35.2425 0.
 HOLE 8 0.0 0.0 0.0
 HOLE 8 -24.257 0.0 0.0
 HOLE 8 -12.1285 21.007178 0.0
 HOLE 8 12.1285 21.007178 0.0
 HOLE 8 24.257 0.0 0.0
 HOLE 8 12.1285 -21.007178 0.0
 HOLE 8 -12.1285 -21.007178 0.0
 HOLE 8 -36.3855 -21.007178 0.0
 HOLE 8 -48.514 0.0 0.0
 HOLE 8 -36.3855 21.007178 0.0
 HOLE 8 -24.257 42.014356 0.0
 HOLE 8 0.0 42.014356 0.0
 HOLE 8 24.257 42.014356 0.0
 HOLE 8 36.3855 21.007178 0.0

Table A.2 (continued)

HOLE 8 48.514 0.0 0.0
HOLE 8 36.3855 -21.007178 0.0
HOLE 8 24.257 -42.014356 0.0
HOLE 8 0.0 -42.014356 0.0
HOLE 8 -24.257 -42.014356 0.0
HOLE 8 -48.514 -42.014356 0.0
HOLE 8 -12.1285 63.021534 0.0
HOLE 8 60.6425 -21.007178 0.0
REPLICATE 2 1 4R30.48 2R0.0 1

UNIT 10

COM=* U(3.85) UNIT, FLOODED, H=26.035, LEVEL 4 *
CYLINDER 1 1 3.175 26.035 0.
CYLINDER 2 1 3.302 26.035 0.
CYLINDER 1 1 9.144 26.035 0.

UNIT 11

COM=* ARRAY OF 22 UNITS, FLOODED, H=26.035, LEVEL 4 *
CUBOID 2 1 4P91.44 26.035 0.
HOLE 10 0.0 0.0 0.0
HOLE 10 -24.257 0.0 0.0
HOLE 10 -12.1285 21.007178 0.0
HOLE 10 12.1285 21.007178 0.0
HOLE 10 24.257 0.0 0.0
HOLE 10 12.1285 -21.007178 0.0
HOLE 10 -12.1285 -21.007178 0.0
HOLE 10 -36.3855 -21.007178 0.0
HOLE 10 -48.514 0.0 0.0
HOLE 10 -36.3855 21.007178 0.0
HOLE 10 -24.257 42.014356 0.0
HOLE 10 0.0 42.014356 0.0
HOLE 10 24.257 42.014356 0.0
HOLE 10 36.3855 21.007178 0.0
HOLE 10 48.514 0.0 0.0
HOLE 10 36.3855 -21.007178 0.0
HOLE 10 24.257 -42.014356 0.0
HOLE 10 0.0 -42.014356 0.0
HOLE 10 -24.257 -42.014356 0.0
HOLE 10 -48.514 -42.014356 0.0
HOLE 10 -12.1285 63.021534 0.0
HOLE 10 60.6425 -21.007178 0.0
REPLICATE 2 1 4R30.48 2R0.0 1

UNIT 12

COM=* U(3.85) UNIT, FLOODED, H=9.2075, LEVEL 6 *
CYLINDER 1 1 3.175 9.2075 0.
CYLINDER 2 1 3.302 9.2075 0.
CYLINDER 1 1 9.144 9.2075 0.

UNIT 13

COM=* ARRAY OF 22 UNITS, FLOODED, H=9.2075, LEVEL 6 *
CUBOID 2 1 4P91.44 9.2075 0.
HOLE 12 0.0 0.0 0.0
HOLE 12 -24.257 0.0 0.0
HOLE 12 -12.1285 21.007178 0.0
HOLE 12 12.1285 21.007178 0.0
HOLE 12 24.257 0.0 0.0
HOLE 12 12.1285 -21.007178 0.0
HOLE 12 -12.1285 -21.007178 0.0
HOLE 12 -36.3855 -21.007178 0.0
HOLE 12 -48.514 0.0 0.0
HOLE 12 -36.3855 21.007178 0.0

HOLE 12 -24.257 42.014356 0.0
HOLE 12 0.0 42.014356 0.0
HOLE 12 24.257 42.014356 0.0
HOLE 12 36.3855 21.007178 0.0
HOLE 12 48.514 0.0 0.0
HOLE 12 36.3855 -21.007178 0.0
HOLE 12 24.257 -42.014356 0.0
HOLE 12 0.0 -42.014356 0.0
HOLE 12 -24.257 -42.014356 0.0
HOLE 12 -48.514 -42.014356 0.0
HOLE 12 -12.1285 63.021534 0.0
HOLE 12 60.6425 -21.007178 0.0
REPLICATE 2 1 4R30.48 2R0.0 1

CORE 3 1 -121.92 -121.92 0.
REPLICATE 2 1 4R0.0 1.0 0.0 1
REPLICATE 5 1 5R0.0 0.1905 1
REPLICATE 4 1 5R0.0 2.54 1

END GEOM
READ ARRAY
ARA=1 NUX=1 NUY=13 NUZ=1
FILL 1 2 5Q2 1 END FILL
ARA=2 NUX=60 NUY=20 NUZ=1
FILL F4 END FILL
GBL=3
ARA=3 NUX=1 NUY=1 NUZ=8
FILL 3 5 7 9 7 11 7 13 END FILL
END ARRAY
READ START
NST=1
XSM=-57.658 XSP=57.658
YSM=-51.158356 YSP=51.158356
ZSM= 21.59 ZSP=97.79
END START
READ PLOT

TTL="PLAN VIEW 1/6 SCALE OF CORE, Z=MIDLEVEL OF ANNULI/INSERTS"
XUL=-100. YUL=100. ZUL=59.69
XLR=100. YLR=-100. ZLR=59.69
UAX=1. VDN=-1. DLX=1.524 NCH=* U.WGSC* END

TTL="PLAN VIEW 1/6 SCALE OF CORE, Z=MIDLEVEL OF GRATING"
XUL=-100. YUL=100. ZUL=20.0025
XLR=100. YLR=-100. ZLR=20.0025
UAX=1. VDN=-1. DLX=1.524 NCH=* U.WGSC* END

TTL="PLAN VIEW 1/6 SCALE OF CORE, Z=MIDLEVEL OF FIR TIMBERS"
XUL=-100. YUL=100. ZUL=9.2075
XLR=100. YLR=-100. ZLR=9.2075
UAX=1. VDN=-1. DLX=1.524 NCH=* U.WGSC* END

TTL="PLAN VIEW 1/10 SCALE OF MOCKUP, Z=MIDLEVEL OF U UNITS"
XUL=-130. YUL=130. ZUL=59.69
XLR=130. YLR=-130. ZLR=59.69
UAX=1. VDN=-1. DLX=2.54 NCH=* U.WGSC* END

TTL="PLAN VIEW, FULL SCALE AT CENTER OF ARRAY, Z=MIDLEVEL "
XUL=-16.75 YUL=16.75 ZUL=59.69
XLR=16.75 YLR=-16.75 ZLR=59.69
UAX=1. VDN=-1. DLX=0.254 NCH=* U.WGSC* END

Table A.2 (continued)

TTL="CROSS SECTION OF CORE 1/6 SCALE,Y=0.0"
 XUL=-100. YUL=0.0 ZUL=102.
 XLR=100. YLR=0.0 ZLR=0.
 UAX=1. WDN=-1. DLX=1.524 NCH=* U.WGSC* END

TTL="CROSS SECTION OF MOCKUP 1/10 SCALE,Y=0.0"
 XUL=-130. YUL=0.0 ZUL=105.
 XLR=130. YLR=0.0 ZLR=-65.
 UAX=1. WDN=-1. DLX=2.54 NCH=* U.WGSC* END

TTL="CROSS SECTION OF GRATING/FIR TIMBERS, FULL SCALE"
 XUL=0. YUL=0. ZUL=24.13
 XLR=25.4 YLR=0. ZLR=-5.0
 UAX=1. WDN=-1. DLX=.254 NCH=* U.WGSC* END

TTL="PLAN VIEW OF GRATING THRU TIEBARS, FULL SCALE"
 XUL=0. YUL=25.4 ZUL=21.193
 XLR=25.4 YLR=0. ZLR=21.193
 UAX=1. VDN=-1. DLX=.254 NCH=* U.WGSC* END

TTL="PLAN VIEW OF GRATING @ GRATING MIDLEVEL, FULL SCALE"
 XUL=0. YUL=25.4 ZUL=20.0025
 XLR=25.4 YLR=0. ZLR=20.0025
 UAX=1. VDN=-1. DLX=.254 NCH=* U.WGSC* END

TTL="PLAN VIEW OF TIMBERS @ TIMBER MIDLEVEL, FULL SCALE"
 XUL=0. YUL=25.4 ZUL=9.2075
 XLR=25.4 YLR=-25.4 ZLR=9.2075
 UAX=1. VDN=-1. DLX=.254 NCH=* U.WGSC* END

TTL="CROSS SECTION OF CENTRAL UNIT, 2X SCALE"
 XUL=0.0 YUL=0.0 ZUL=102.
 XLR=15.24 YLR=0.0 ZLR=-5.
 UAX=1. WDN=-1. DLX=0.127 NCH=* U.WGSC* END

END PLOT
 END DATA
 END

CAB10
 =CSAS25
 CASE EBJ.8 U(3.85) 6 @ 7.2"/2.6"/0.75"/91.4CM, SQUARE
 27GROUPNDP4 INPHOMMEDIUM

' U(3.85) METAL
 U-235 1 0. 1.8643E-3 END
 U-238 1 0. 4.5971E-2 END

' FULL DENSITY WATER MODERATOR/REFLECTOR
 H2O 2 1.0 END

' FIR TIMBER MODEL
 C 3 0. 1.06802E-2 END
 H 3 0. 2.21713E-2 END
 O 3 0. 1.10850E-2 END

' STEEL FOR GRATING, TANK WALLS AND FLOOR
 CARBONSTEEL 4 1.0 END

' STAINLESS STEEL LINING FOR TANK
 SS304 5 1.0 END

END COMP
 CASE EBJ.8 U(3.85) 6 @ 7.2"/2.6"/0.75"/91.4CM, SQUARE
 READ PARM
 NPG=600 NUB=YES PLT=NO FDN=YES TME=90 TBA=2
 END PARM
 READ GEOM

UNIT 1
 COM=* FIR TIMBER 7.25" X 72" X 7.25" *
 CUBOID 3 1 182.88 0. 18.415 0. 18.415 0.

UNIT 2
 COM=* WATER GAP 3.5" X 72" X 7.25" BETWEEN TIMBERS *
 CUBOID 2 1 182.88 0. 8.89 0. 18.415 0.

UNIT 3
 COM=* ARRAY OF TIMBERS 72" X 72" X 7.25" *
 ARRAY 1 3*0.0
 REPLICATE 2 1 2R0. 2R0.3175 2R0. 1
 REPLICATE 2 1 4R30.48 2R0. 1

UNIT 4
 COM=* SECTION OF STEEL GRATING *
 CUBOID 4 1 2.778125 .238125 .396875 -.396875 3.175 2.38125
 CUBOID 2 1 2.778125 .238125 4.524375 -4.524375 3.175 0.
 CUBOID 4 1 3.01625 0. 4.524375 -4.524375 3.175 0.

UNIT 5
 COM=* ARRAY OF STEEL GRATING *
 ARRAY 2 3*0.0
 REPLICATE 2 1 4R0.9525 2R0.0 1
 REPLICATE 2 1 4R30.48 2R0. 1

Table A.2 (continued)

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UNIT 6
COM=* U(3.85) ANNULUS, H=76.2, SUBMERGED, ON CORNER *
CYLINDER 2 1 3.302 76.2 0.
CYLINDER 1 1 4.614139 76.2 0.
CYLINDER 1 1 5.628264 76.2 0.
CYLINDER 1 1 6.485710 76.2 0.
CYLINDER 1 1 7.242341 76.2 0.
CYLINDER 1 1 7.927079 76.2 0.
CYLINDER 1 1 8.557199 76.2 0.
CYLINDER 1 1 9.144000 76.2 0.
CUBOID 2 1 4P10.0965 91.4 0.

UNIT 7
COM=* U(3.85) ANNULUS, H=76.2, SUBMERGED, ON SIDE *
CYLINDER 2 1 3.302 76.2 0.
CYLINDER 1 1 4.614139 76.2 0.
CYLINDER 1 1 5.628264 76.2 0.
CYLINDER 1 1 6.485710 76.2 0.
CYLINDER 1 1 7.242341 76.2 0.
CYLINDER 1 1 7.927079 76.2 0.
CYLINDER 1 1 8.557199 76.2 0.
CYLINDER 1 1 9.144000 76.2 0.
CUBOID 2 1 4P10.0965 91.4 0.

UNIT 8
COM=* ARRAY OF 6 ANNULI, H=76.2, SUBMERGED *
ARRAY 3 3*0.0
REPLICATE 2 1 2R61.1505 2R71.247 2R0. 1
REPLICATE 2 1 4R30.48 2R0. 1

CORE 4 1 -121.92 -121.92 0.
REPLICATE 5 1 5R0.0 0.1905 1
REPLICATE 4 1 5R0.0 2.54 1
END GEOM
READ ARRAY
ARA=1 NUX=1 NUY=13 NUZ=1
FILL 1 2 5Q2 1 END FILL
ARA=2 NUX=60 NUY=20 NUZ=1
FILL F4 END FILL
ARA=3 NUX=3 NUY=2 NUZ=1
FILL 6 7 6 6 7 6 END FILL
GBL=4
ARA=4 NUX=1 NUY=1 NUZ=3
FILL 3 5 8 END FILL
END ARRAY
READ START
NST=1
XSM=-30.2895 XSP=30.2895
YSM=-20.193 YSP=20.193
ZSM=21.59 ZSP=97.79
END START
READ PLOT

TTL="PLAN VIEW 1/6 SCALE OF CORE, Z=MIDLEVEL OF ANNULI/INSERTS"
XUL=-91.44 YUL=91.44 ZUL=59.69
XLR=91.44 YLR=-91.44 ZLR=59.69
UAX=1. VDN=-1. DLX=1.524 NCH=* U.WGS* END

TTL="PLAN VIEW 1/6 SCALE OF CORE, Z=MIDLEVEL OF GRATING"
XUL=-91.44 YUL=91.44 ZUL=20.0025
XLR=91.44 YLR=-91.44 ZLR=20.0025
UAX=1. VDN=-1. DLX=1.524 NCH=* U.WGS* END

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TTL="PLAN VIEW 1/6 SCALE OF CORE, Z=MIDLEVEL OF FIR TIMBERS"
XUL=-91.44 YUL=91.44 ZUL=9.2075
XLR=91.44 YLR=-91.44 ZLR=9.2075
UAX=1. VDN=-1. DLX=1.524 NCH=* U.WGS* END

TTL="PLAN VIEW 1/10 SCALE OF MOCKUP, Z=MIDLEVEL OF U UNITS"
XUL=-135. YUL=135. ZUL=59.69
XLR=135. YLR=-135. ZLR=59.69
UAX=1. VDN=-1. DLX=2.54 NCH=* U.WGS* END

TTL="PLAN VIEW 2X SCALE OF SINGLE U UNIT, Z=MIDLEVEL OF UNIT"
XUL=0.0 YUL=20.193 ZUL=59.69
XLR=20.193 YLR=0.0 ZLR=59.69
UAX=1. VDN=-1. DLX=0.127 NCH=* U.WGS* END

TTL="CROSS SECTION OF CORE 1/6 SCALE, Y=10.0965"
XUL=-91.44 YUL=10.0965 ZUL=125.
XLR=91.44 YLR=10.0965 ZLR=-10.
UAX=1. WDN=-1. DLX=1.524 NCH=* U.WGS* END

TTL="CROSS SECTION OF MOCKUP 1/10 SCALE, Y=10.0965"
XUL=-135. YUL=10.0965 ZUL=125.
XLR=135. YLR=10.0965 ZLR=-10.
UAX=1. WDN=-1. DLX=2.54 NCH=* U.WGS* END

TTL="CROSS SECTION OF GRATING/FIR TIMBERS, FULL SCALE"
XUL=0. YUL=0. ZUL=24.13
XLR=25.4 YLR=0. ZLR=-3.0
UAX=1. WDN=-1. DLX=.254 NCH=* U.WGS* END

TTL="PLAN VIEW OF GRATING THRU TIEBARS, FULL SCALE"
XUL=0. YUL=25.4 ZUL=21.193
XLR=25.4 YLR=0. ZLR=21.193
UAX=1. VDN=-1. DLX=.254 NCH=* U.WGS* END

TTL="PLAN VIEW OF GRATING @ GRATING MIDLEVEL, FULL SCALE"
XUL=0. YUL=25.4 ZUL=20.0025
XLR=25.4 YLR=0. ZLR=20.0025
UAX=1. VDN=-1. DLX=.254 NCH=* U.WGS* END

TTL="PLAN VIEW OF TIMBERS @ TIMBER MIDLEVEL, FULL SCALE"
XUL=0. YUL=25.4 ZUL=9.2075
XLR=25.4 YLR=-25.4 ZLR=9.2075
UAX=1. VDN=-1. DLX=.254 NCH=* U.WGS* END

TTL="CROSS SECTION OF CENTRAL UNIT, FULL SCALE, Y=10.0965"
XUL=-10.0965 YUL=10.0965 ZUL=125.
XLR=10.0965 YLR=10.0965 ZLR=-10.
UAX=1. WDN=-1. DLX=.254 NCH=* U.WGS* END

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END PLOT
END DATA
END

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Table A.2 (continued)

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CAB11
=CSAS25
CASE EBJ.9 U(3.85) 16 @ 7.2"/2.6"/1.50"/49.2CM, SQUARE
27GROUPNDF4 INFHOMMEDIUM

' U(3.85) METAL
U-235      1 0.  1.8643E-3 END
U-238      1 0.  4.5971E-2 END

' FULL DENSITY WATER MODERATOR/REFLECTOR
H2O        2 1.0      END

' FIR TIMBER MODEL
C           3 0.  1.06802E-2 END
H           3 0.  2.21713E-2 END
O           3 0.  1.10850E-2 END

' STEEL FOR GRATING, TANK WALLS AND FLOOR
CARBONSTEEL 4 1.0      END

' STAINLESS STEEL LINING FOR TANK
SS304      5 1.0      END

END COMP
CASE EBJ.9 U(3.85) 16 @ 7.2"/2.6"/1.50"/49.2CM, SQUARE
READ PARM
NPG=600 NUB=YES PLT=NO FDN=YES TME=90 TBA=2
END PARM
READ GEOM

UNIT 1
COM=* FIR TIMBER 7.25" X 72" X 7.25" *
CUBOID 3 1 182.88 0. 18.415 0. 18.415 0.

UNIT 2
COM=* WATER GAP 3.5" X 72" X 7.25" BETWEEN TIMBERS *
CUBOID 2 1 182.88 0. 8.89 0. 18.415 0.

UNIT 3
COM=* ARRAY OF TIMBERS 72" X 72" X 7.25" *
ARRAY 1 3*0.0
REPLICATE 2 1 2R0. 2R0.3175 2R0. 1
REPLICATE 2 1 4R30.48 2R0. 1

UNIT 4
COM=* SECTION OF STEEL GRATING *
CUBOID 4 1 2.778125 .238125 .396875 -.396875 3.175 2.38125
CUBOID 2 1 2.778125 .238125 4.524375 -4.524375 3.175 0.
CUBOID 4 1 3.01625 0. 4.524375 -4.524375 3.175 0.

UNIT 5
COM=* ARRAY OF STEEL GRATING *
ARRAY 2 3*0.0
REPLICATE 2 1 4R0.9525 2R0.0 1
REPLICATE 2 1 4R30.48 2R0. 1

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UNIT 6
COM=* U(3.85) ANNULUS, H=49.2, SUBMERGED, ON CORNER *
CYLINDER 2 1 3.302 49.2 0.
CYLINDER 1 1 4.614139 49.2 0.
CYLINDER 1 1 5.628264 49.2 0.
CYLINDER 1 1 6.485710 49.2 0.
CYLINDER 1 1 7.242341 49.2 0.
CYLINDER 1 1 7.927079 49.2 0.
CYLINDER 1 1 8.557199 49.2 0.
CYLINDER 1 1 9.144000 49.2 0.
CUBOID 2 1 4P11.049 49.2 0.

UNIT 7
COM=* U(3.85) ANNULUS, H=49.2, SUBMERGED, ON SIDE *
CYLINDER 2 1 3.302 49.2 0.
CYLINDER 1 1 4.614139 49.2 0.
CYLINDER 1 1 5.628264 49.2 0.
CYLINDER 1 1 6.485710 49.2 0.
CYLINDER 1 1 7.242341 49.2 0.
CYLINDER 1 1 7.927079 49.2 0.
CYLINDER 1 1 8.557199 49.2 0.
CYLINDER 1 1 9.144000 49.2 0.
CUBOID 2 1 4P11.049 49.2 0.

UNIT 8
COM=* U(3.85) ANNULUS, H=49.2, SUBMERGED, IN MIDDLE *
CYLINDER 2 1 3.302 49.2 0.
CYLINDER 1 1 4.614139 49.2 0.
CYLINDER 1 1 5.628264 49.2 0.
CYLINDER 1 1 6.485710 49.2 0.
CYLINDER 1 1 7.242341 49.2 0.
CYLINDER 1 1 7.927079 49.2 0.
CYLINDER 1 1 8.557199 49.2 0.
CYLINDER 1 1 9.144000 49.2 0.
CUBOID 2 1 4P11.049 49.2 0.

UNIT 9
COM=* U(3.85) ANNULUS, H=27.0, DRY, ON CORNER *
CYLINDER 0 1 3.302 27.0 0.
CYLINDER 1 1 4.614139 27.0 0.
CYLINDER 1 1 5.628264 27.0 0.
CYLINDER 1 1 6.485710 27.0 0.
CYLINDER 1 1 7.242341 27.0 0.
CYLINDER 1 1 7.927079 27.0 0.
CYLINDER 1 1 8.557199 27.0 0.
CYLINDER 1 1 9.144000 27.0 0.
CUBOID 0 1 4P11.049 27.0 0.

UNIT 10
COM=* U(3.85) ANNULUS, H=27.0, DRY, ON SIDE *
CYLINDER 0 1 3.302 27.0 0.
CYLINDER 1 1 4.614139 27.0 0.
CYLINDER 1 1 5.628264 27.0 0.
CYLINDER 1 1 6.485710 27.0 0.
CYLINDER 1 1 7.242341 27.0 0.
CYLINDER 1 1 7.927079 27.0 0.
CYLINDER 1 1 8.557199 27.0 0.
CYLINDER 1 1 9.144000 27.0 0.
CUBOID 0 1 4P11.049 27.0 0.

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Table A.2 (continued)

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UNIT 11
COM=* U(3.85) ANNULUS, H=27.0, DRY, IN MIDDLE *
CYLINDER 0 1 3.302 27.0 0.
CYLINDER 1 1 4.614139 27.0 0.
CYLINDER 1 1 5.628264 27.0 0.
CYLINDER 1 1 6.485710 27.0 0.
CYLINDER 1 1 7.242341 27.0 0.
CYLINDER 1 1 7.927079 27.0 0.
CYLINDER 1 1 8.557199 27.0 0.
CYLINDER 1 1 9.144000 27.0 0.
CUBOID 0 1 4P11.049 27.0 0.

UNIT 12
COM=* ARRAY OF 16 ANNULI, H=49.2, SUBMERGED *
ARRAY 3 3*0.0
REPLICATE 2 1 4R47.244 2R0. 1
REPLICATE 2 1 4R30.48 2R0. 1

UNIT 13
COM=* ARRAY OF 16 ANNULI, H=27.0, DRY *
ARRAY 4 3*0.0
REPLICATE 0 1 4R47.244 2R0. 1
REPLICATE 0 1 4R30.48 2R0. 1

CORE 5 1 -121.92 -121.92 0.
REPLICATE 5 1 5R0.0 0.1905 1
REPLICATE 4 1 5R0.0 2.54 1
END GEOM
READ ARRAY
ARA=1 NUX=1 NUY=13 NUZ=1
FILL 1 2 5Q2 1 END FILL
ARA=2 NUX=60 NUY=20 NUZ=1
FILL F4 END FILL
ARA=3 NUX=4 NUY=4 NUZ=1
FILL 6 7 7 6 7 8 8 7 7 8 8 7 6 7 7 6 END FILL
ARA=4 NUX=4 NUY=4 NUZ=1
FILL 9 10 10 9 10 11 11 10 10 11 11 10 9 10 10 9 END FILL
GBL=5
ARA=5 NUX=1 NUY=1 NUZ=4
FILL 3 5 12 13 END FILL
END ARRAY
READ START
NST=1
XSM=-44.196 XSP=44.196
YSM=-44.196 YSP=44.196
ZSM=21.59 ZSP=70.79
END START
READ PLOT

TTL="PLAN VIEW 1/6 SCALE OF CORE, Z=MIDLEVEL OF ANNULI/INSERTS"
XUL=-91.44 YUL=91.44 ZUL=59.69
XLR=91.44 YLR=-91.44 ZLR=59.69
UAX=1. VDN=-1. DLX=1.524 NCH=* U.WGS* END

TTL="PLAN VIEW 1/6 SCALE OF CORE, Z=MIDLEVEL OF GRATING"
XUL=-91.44 YUL=91.44 ZUL=20.0025
XLR=91.44 YLR=-91.44 ZLR=20.0025
UAX=1. VDN=-1. DLX=1.524 NCH=* U.WGS* END

TTL="PLAN VIEW 1/6 SCALE OF CORE, Z=MIDLEVEL OF FIR TIMBERS"
XUL=-91.44 YUL=91.44 ZUL=9.2075
XLR=91.44 YLR=-91.44 ZLR=9.2075
UAX=1. VDN=-1. DLX=1.524 NCH=* U.WGS* END

TTL="PLAN VIEW 1/10 SCALE OF MOCKUP, Z=MIDLEVEL OF U UNITS"
XUL=-135. YUL=135. ZUL=59.69
XLR=135. YLR=-135. ZLR=59.69
UAX=1. VDN=-1. DLX=2.54 NCH=* U.WGS* END

TTL="PLAN VIEW 2X SCALE OF SINGLE U UNIT, Z=MIDLEVEL OF UNIT"
XUL=0.0 YUL=22.098 ZUL=59.69
XLR=22.098 YLR=0. ZLR=59.69
UAX=1. VDN=-1. DLX=0.127 NCH=* U.WGS* END

TTL="CROSS SECTION OF CORE 1/6 SCALE, Y=11.049"
XUL=-91.44 YUL=11.049 ZUL=110.
XLR=91.44 YLR=11.049 ZLR=-10.
UAX=1. WDN=-1. DLX=1.524 NCH=* U.WGS* END

TTL="CROSS SECTION OF MOCKUP 1/10 SCALE, Y=11.049"
XUL=-135. YUL=11.049 ZUL=125.
XLR=135. YLR=11.049 ZLR=-10.
UAX=1. WDN=-1. DLX=2.54 NCH=* U.WGS* END

TTL="CROSS SECTION OF GRATING/FIR TIMBERS, FULL SCALE"
XUL=0. YUL=0. ZUL=24.13
XLR=25.4 YLR=0. ZLR=-3.0
UAX=1. WDN=-1. DLX=.254 NCH=* U.WGS* END

TTL="PLAN VIEW OF GRATING THRU TIEBARS, FULL SCALE"
XUL=0. YUL=25.4 ZUL=21.193
XLR=25.4 YLR=0. ZLR=21.193
UAX=1. VDN=-1. DLX=.254 NCH=* U.WGS* END

TTL="PLAN VIEW OF GRATING @ GRATING MIDLEVEL, FULL SCALE"
XUL=0. YUL=25.4 ZUL=20.0025
XLR=25.4 YLR=0. ZLR=20.0025
UAX=1. VDN=-1. DLX=.254 NCH=* U.WGS* END

TTL="PLAN VIEW OF TIMBERS @ TIMBER MIDLEVEL, FULL SCALE"
XUL=0. YUL=25.4 ZUL=9.2075
XLR=25.4 YLR=-25.4 ZLR=9.2075
UAX=1. VDN=-1. DLX=.254 NCH=* U.WGS* END

TTL="CROSS SECTION OF CENTRAL UNIT, FULL SCALE, Y=11.049"
XUL=0.0 YUL=22.098 ZUL=110.
XLR=22.098 YLR=0.0 ZLR=-10.
UAX=1. WDN=-1. DLX=.254 NCH=* U.WGS* END

END PLOT
END DATA
END

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Table A.2 (continued)

CAB12
 =CSA525
 CASE EBJ.10 U(3.85) 20 @ 7.2"/2.6"/1.87"/79.0CM, SQUARE
 27GROUPNDP4 INFHOMMEDIUM

' U(3.85) METAL
 U-235 1 0. 1.8643E-3 END
 U-238 1 0. 4.5971E-2 END

' FULL DENSITY WATER MODERATOR/REFLECTOR
 H2O 2 1.0 END

' FIR TIMBER MODEL
 C 3 0. 1.06802E-2 END
 H 3 0. 2.21713E-2 END
 O 3 0. 1.10850E-2 END

' STEEL FOR GRATING, TANK WALLS AND FLOOR
 CARBONSTEEL 4 1.0 END

' STAINLESS STEEL LINING FOR TANK
 SS304 5 1.0 END

END COMP
 CASE EBJ.10 U(3.85) 20 @ 7.2"/2.6"/1.87"/79.0CM, SQUARE
 READ PARM
 NPG=600 NUB=YES PLT=NO FDN=YES TME=90 TBA=2
 END PARM
 READ GEOM

UNIT 1
 COM=* FIR TIMBER 7.25" X 72" X 7.25" *
 CUBOID 3 1 182.88 0. 18.415 0. 18.415 0.

UNIT 2
 COM=* WATER GAP 3.5" X 72" X 7.25" BETWEEN TIMBERS *
 CUBOID 2 1 182.88 0. 8.89 0. 18.415 0.

UNIT 3
 COM=* ARRAY OF TIMBERS 72" X 72" X 7.25" *
 ARRAY 1 3*0.0
 REPLICATE 2 1 2R0. 2R0.3175 2R0. 1
 REPLICATE 2 1 4R30.48 2R0. 1

UNIT 4
 COM=* SECTION OF STEEL GRATING *
 CUBOID 4 1 2.778125 .238125 .396875 -.396875 3.175 2.38125
 CUBOID 2 1 2.778125 .238125 4.524375 -4.524375 3.175 0.
 CUBOID 4 1 3.01625 0. 4.524375 -4.524375 3.175 0.

UNIT 5
 COM=* ARRAY OF STEEL GRATING *
 ARRAY 2 3*0.0
 REPLICATE 2 1 4R0.9525 2R0.0 1
 REPLICATE 2 1 4R30.48 2R0. 1

UNIT 6
 COM=* U(3.85) ANNULUS, H=76.2, SUBMERGED *
 CYLINDER 2 1 3.302 76.2 0.
 CYLINDER 1 1 9.144 76.2 0.
 CUBOID 2 1 4P11.5189 79.0 0.

UNIT 7
 COM=* U(3.85) ANNULUS, H=76.2, SUBMERGED *
 CYLINDER 2 1 3.302 76.2 0.
 CYLINDER 1 1 9.144 76.2 0.
 CUBOID 2 1 4P11.5189 79.0 0.

UNIT 8
 COM=* U(3.85) ANNULUS, H=76.2, SUBMERGED *
 CYLINDER 2 1 3.302 76.2 0.
 CYLINDER 1 1 9.144 76.2 0.
 CUBOID 2 1 4P11.5189 79.0 0.

UNIT 9
 COM=* U(3.85) ANNULUS, H=76.2, SUBMERGED *
 CYLINDER 2 1 3.302 76.2 0.
 CYLINDER 1 1 9.144 76.2 0.
 CUBOID 2 1 4P11.5189 79.0 0.

UNIT 10
 CYLINDER 2 1 3.302 76.2 0.
 CYLINDER 1 1 9.144 76.2 0.
 CUBOID 2 1 4P11.5189 79.0 0.

UNIT 11
 CYLINDER 2 1 3.302 76.2 0.
 CYLINDER 1 1 9.144 76.2 0.
 CUBOID 2 1 4P11.5189 79.0 0.

UNIT 12
 COM=* U(3.85) ANNULUS, H=76.2, SUBMERGED *
 CYLINDER 2 1 3.302 76.2 0.
 CYLINDER 1 1 9.144 76.2 0.
 CUBOID 2 1 4P11.5189 79.0 0.

UNIT 13
 COM=* U(3.85) ANNULUS, H=76.2, SUBMERGED *
 CYLINDER 2 1 3.302 76.2 0.
 CYLINDER 1 1 9.144 76.2 0.
 CUBOID 2 1 4P11.5189 79.0 0.

UNIT 14
 COM=* U(3.85) ANNULUS, H=76.2, SUBMERGED *
 CYLINDER 2 1 3.302 76.2 0.
 CYLINDER 1 1 9.144 76.2 0.
 CUBOID 2 1 4P11.5189 79.0 0.

UNIT 15
 COM=* U(3.85) ANNULUS, H=76.2, SUBMERGED *
 CYLINDER 2 1 3.302 76.2 0.
 CYLINDER 1 1 9.144 76.2 0.
 CUBOID 2 1 4P11.5189 79.0 0.

UNIT 16
 COM=* U(3.85) ANNULUS, H=76.2, SUBMERGED *
 CYLINDER 2 1 3.302 76.2 0.
 CYLINDER 1 1 9.144 76.2 0.
 CUBOID 2 1 4P11.5189 79.0 0.

UNIT 17
 COM=* U(3.85) ANNULUS, H=76.2, SUBMERGED *
 CYLINDER 2 1 3.302 76.2 0.
 CYLINDER 1 1 9.144 76.2 0.
 CUBOID 2 1 4P11.5189 79.0 0.

Table A.2 (continued)

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UNIT 18
COM=* U(3.85) ANNULUS, H=76.2, SUBMERGED *
CYLINDER 2 1 3.302 76.2 0.
CYLINDER 1 1 9.144 76.2 0.
CUBOID 2 1 4P11.5189 79.0 0.

UNIT 19
COM=* U(3.85) ANNULUS, H=76.2, SUBMERGED *
CYLINDER 2 1 3.302 76.2 0.
CYLINDER 1 1 9.144 76.2 0.
CUBOID 2 1 4P11.5189 79.0 0.

UNIT 20
COM=* U(3.85) ANNULUS, H=76.2, SUBMERGED *
CYLINDER 2 1 3.302 76.2 0.
CYLINDER 1 1 9.144 76.2 0.
CUBOID 2 1 4P11.5189 79.0 0.

UNIT 21
COM=* U(3.85) ANNULUS, H=76.2, SUBMERGED *
CYLINDER 2 1 3.302 76.2 0.
CYLINDER 1 1 9.144 76.2 0.
CUBOID 2 1 4P11.5189 79.0 0.

UNIT 22
COM=* U(3.85) ANNULUS, H=76.2, SUBMERGED *
CYLINDER 2 1 3.302 76.2 0.
CYLINDER 1 1 9.144 76.2 0.
CUBOID 2 1 4P11.5189 79.0 0.

UNIT 23
COM=* U(3.85) ANNULUS, H=76.2, SUBMERGED *
CYLINDER 2 1 3.302 76.2 0.
CYLINDER 1 1 9.144 76.2 0.
CUBOID 2 1 4P11.5189 79.0 0.

UNIT 24
COM=* U(3.85) ANNULUS, H=76.2, SUBMERGED *
CYLINDER 2 1 3.302 76.2 0.
CYLINDER 1 1 9.144 76.2 0.
CUBOID 2 1 4P11.5189 79.0 0.

UNIT 25
COM=* U(3.85) ANNULUS, H=76.2, SUBMERGED *
CYLINDER 2 1 3.302 76.2 0.
CYLINDER 1 1 9.144 76.2 0.
CUBOID 2 1 4P11.5189 79.0 0.

UNIT 26
COM=* WATER CUBOID TO COMPLETE ARRAY *
CUBOID 2 1 4P11.5189 79.0 0.

UNIT 27
COM=* ARRAY OF 20 ANNULI, H=76.2, SUBMERGED *
ARRAY 3 3*0.0
REPLICATE 2 1 4R33.8455 2R0. 1
REPLICATE 2 1 4R30.48 2R0. 1

CORE 4 1 -121.92 -121.92 0.
REPLICATE 5 1 5R0.0 0.1905 1
REPLICATE 4 1 5R0.0 2.54 1
END GEOM

READ ARRAY
ARA=1 NUX=1 NUY=13 NUZ=1
FILL 1 2 5Q2 1 END FILL
ARA=2 NUX=60 NUY=20 NUZ=1
FILL F4 END FILL
ARA=3 NUX=5 NUY=5 NUZ=1
FILL 26 26 6 7 26 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22
26 23 24 25 26 END FILL
GBL=4
ARA=4 NUX=1 NUY=1 NUZ=3
FILL 3 5 27 END FILL
END ARRAY
READ START
NST=1
XSM=-57.5945 XSP=57.5945
YSM=-57.5945 YSP=57.5945
ZSM=21.59 ZSP=97.79
END START
READ PLOT

TTL="PLAN VIEW 1/6 SCALE OF CORE, Z=MIDLEVEL OF ANNULI/INSERTS"
XUL=-91.44 YUL=91.44 ZUL=59.69
XLR=91.44 YLR=-91.44 ZLR=59.69
UAX=1. VDN=-1. DLX=1.524 NCH=* U.WGS* END

TTL="PLAN VIEW 1/6 SCALE OF CORE, Z=MIDLEVEL OF GRATING"
XUL=-91.44 YUL=91.44 ZUL=20.0025
XLR=91.44 YLR=-91.44 ZLR=20.0025
UAX=1. VDN=-1. DLX=1.524 NCH=* U.WGS* END

TTL="PLAN VIEW 1/6 SCALE OF CORE, Z=MIDLEVEL OF FIR TIMBERS"
XUL=-91.44 YUL=91.44 ZUL=9.2075
XLR=91.44 YLR=-91.44 ZLR=9.2075
UAX=1. VDN=-1. DLX=1.524 NCH=* U.WGS* END

TTL="PLAN VIEW 1/10 SCALE OF MOCKUP, Z=MIDLEVEL OF U UNITS"
XUL=-135. YUL=135. ZUL=59.69
XLR=135. YLR=-135. ZLR=59.69
UAX=1. VDN=-1. DLX=2.54 NCH=* U.WGS* END

TTL="PLAN VIEW 2X SCALE OF SINGLE U UNIT, Z=MIDLEVEL OF UNIT"
XUL=-11.5189 YUL=11.5189 ZUL=59.69
XLR=11.5189 YLR=-11.5189 ZLR=59.69
UAX=1. VDN=-1. DLX=0.127 NCH=* U.WGS* END

TTL="CROSS SECTION OF CORE 1/6 SCALE, Y=0.0"
XUL=-91.44 YUL=0.0 ZUL=110.
XLR=91.44 YLR=0.0 ZLR=-10.
UAX=1. WDN=-1. DLX=1.524 NCH=* U.WGS* END

TTL="CROSS SECTION OF MOCKUP 1/10 SCALE, Y=0.0"
XUL=-135. YUL=0.0 ZUL=125.
XLR=135. YLR=0.0 ZLR=-10.
UAX=1. WDN=-1. DLX=2.54 NCH=* U.WGS* END

TTL="CROSS SECTION OF GRATING/FIR TIMBERS, FULL SCALE"
XUL=0. YUL=0. ZUL=24.13
XLR=25.4 YLR=0. ZLR=-3.0
UAX=1. WDN=-1. DLX=.254 NCH=* U.WGS* END

TTL="PLAN VIEW OF GRATING THRU TIEBARS, FULL SCALE"
XUL=0. YUL=25.4 ZUL=21.193
XLR=25.4 YLR=0. ZLR=21.193
UAX=1. VDN=-1. DLX=.254 NCH=* U.WGS* END

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Table A.2 (continued)

TTL="PLAN VIEW OF GRATING @ GRATING MIDLEVEL, FULL SCALE"
 XUL=0. YUL=25.4 ZUL=20.0025
 XLR=25.4 YLR=0. ZLR=20.0025
 UAX=1. VDN=-1. DLX=.254 NCH=* U.WGS* END

TTL="PLAN VIEW OF TIMBERS @ TIMBER MIDLEVEL, FULL SCALE"
 XUL=0. YUL=25.4 ZUL=9.2075
 XLR=25.4 YLR=-25.4 ZLR=9.2075
 UAX=1. VDN=-1. DLX=.254 NCH=* U.WGS* END

TTL="CROSS SECTION OF CENTRAL UNIT, FULL SCALE, Y=0.0"
 XUL=-11.5189 YUL=0.0 ZUL=110.
 XLR=11.5189 YLR=0.0 ZLR=-10.
 UAX=1. WDN=-1. DLX=.254 NCH=* U.WGS* END

END PLOT
 END DATA
 END

CAB13
 =CSAS25
 CASE EBJ.11 U(3.85) 8 @ 7.2"/2.6"/0.0"/72.5CM, SQUARE
 27GROUPNDF4 INFHOMMEDIUM

' U(3.85) METAL
 U-235 1 0. 1.8643E-3 END
 U-238 1 0. 4.5971E-2 END

' FULL DENSITY WATER MODERATOR/REFLECTOR
 H2O 2 1.0 END

' FIR TIMBER MODEL
 C 3 0. 1.06802E-2 END
 H 3 0. 2.21713E-2 END
 O 3 0. 1.10850E-2 END

' STEEL FOR GRATING, TANK WALLS AND FLOOR
 CARBONSTEEL 4 1.0 END

' STAINLESS STEEL LINING FOR TANK
 SS304 5 1.0 END

END COMP
 CASE EBJ.11 U(3.85) 8 @ 7.2"/2.6"/0.0"/72.5CM, SQUARE
 READ PARM
 NPG=600 NUB=YES PLT=NO PDN=YES TME=90 TBA=2
 END PARM
 READ GEOM

UNIT 1
 COM=* FIR TIMBER 7.25" X 72" X 7.25" *
 CUBOID 3 1 182.88 0. 18.415 0. 18.415 0.

UNIT 2
 COM=* WATER GAP 3.5" X 72" X 7.25" BETWEEN TIMBERS *
 CUBOID 2 1 182.88 0. 8.89 0. 18.415 0.

UNIT 3
 COM=* ARRAY OF TIMBERS 72" X 72" X 7.25" *
 ARRAY 1 3*0.0
 REPLICATE 2 1 2R0. 2R0.3175 2R0. 1
 REPLICATE 2 1 4R30.48 2R0. 1

UNIT 4
 COM=* SECTION OF STEEL GRATING *
 CUBOID 4 1 2.778125 .238125 .396875 -.396875 3.175 2.38125
 CUBOID 2 1 2.778125 .238125 4.524375 -4.524375 3.175 0.
 CUBOID 4 1 3.01625 0. 4.524375 -4.524375 3.175 0.

UNIT 5
 COM=* ARRAY OF STEEL GRATING *
 ARRAY 2 3*0.0
 REPLICATE 2 1 4R0.9525 2R0.0 1
 REPLICATE 2 1 4R30.48 2R0. 1

UNIT 6
 COM=* U(3.85) ANNULUS, H=72.5, SUBMERGED, ON CORNER *
 CYLINDER 2 1 3.302 72.5 0.
 CYLINDER 1 1 4.614139 72.5 0.
 CYLINDER 1 1 5.628264 72.5 0.
 CYLINDER 1 1 6.485710 72.5 0.
 CYLINDER 1 1 7.242341 72.5 0.
 CYLINDER 1 1 7.927079 72.5 0.
 CYLINDER 1 1 8.557199 72.5 0.
 CYLINDER 1 1 9.144000 72.5 0.
 CUBOID 2 1 4P9.144 72.5 0.

UNIT 7
 COM=* U(3.85) ANNULUS, H=72.5, SUBMERGED, ON SIDE *
 CYLINDER 2 1 3.302 72.5 0.
 CYLINDER 1 1 4.614139 72.5 0.
 CYLINDER 1 1 5.628264 72.5 0.
 CYLINDER 1 1 6.485710 72.5 0.
 CYLINDER 1 1 7.242341 72.5 0.
 CYLINDER 1 1 7.927079 72.5 0.
 CYLINDER 1 1 8.557199 72.5 0.
 CYLINDER 1 1 9.144000 72.5 0.
 CUBOID 2 1 4P9.144 72.5 0.

UNIT 8
 COM=* U(3.85) ANNULUS, H=3.7, DRY, ON CORNER *
 CYLINDER 0 1 3.302 3.7 0.
 CYLINDER 1 1 4.614139 3.7 0.
 CYLINDER 1 1 5.628264 3.7 0.
 CYLINDER 1 1 6.485710 3.7 0.
 CYLINDER 1 1 7.242341 3.7 0.
 CYLINDER 1 1 7.927079 3.7 0.
 CYLINDER 1 1 8.557199 3.7 0.
 CYLINDER 1 1 9.144000 3.7 0.
 CUBOID 0 1 4P9.144 3.7 0.

UNIT 9
 COM=* U(3.85) ANNULUS, H=3.7, DRY, ON SIDE *
 CYLINDER 0 1 3.302 3.7 0.
 CYLINDER 1 1 4.614139 3.7 0.
 CYLINDER 1 1 5.628264 3.7 0.
 CYLINDER 1 1 6.485710 3.7 0.
 CYLINDER 1 1 7.242341 3.7 0.
 CYLINDER 1 1 7.927079 3.7 0.
 CYLINDER 1 1 8.557199 3.7 0.
 CYLINDER 1 1 9.144000 3.7 0.
 CUBOID 0 1 4P9.144 3.7 0.

Table A.2 (continued)

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UNIT 10
COM=* ARRAY OF 8 ANNULI, H=72.5, SUBMERGED *
ARRAY 3 3*0.0
REPLICATE 2 1 2R54.864 2R73.152 2R0. 1
REPLICATE 2 1 4R30.48 2R0. 1

UNIT 11
COM=* ARRAY OF 8 ANNULI, H=3.7, DRY *
ARRAY 4 3*0.0
REPLICATE 0 1 2R54.864 2R73.152 2R0. 1
REPLICATE 0 1 4R30.48 2R0. 1

CORE 5 1 -121.92 -121.92 0.
REPLICATE 5 1 5R0.0 0.1905 1
REPLICATE 4 1 5R0.0 2.54 1
END GROM
READ ARRAY
ARA=1 NUX=1 NUY=13 NUZ=1
FILL 1 2 5Q2 1 END FILL
ARA=2 NUX=60 NUY=20 NUZ=1
FILL P4 END FILL
ARA=3 NUX=4 NUY=2 NUZ=1
FILL 6 7 7 6 6 7 7 6 END FILL
ARA=4 NUX=4 NUY=2 NUZ=1
FILL 8 9 9 8 8 9 9 8 END FILL
GBL=5
ARA=5 NUX=1 NUY=1 NUZ=4
FILL 3 5 10 11 END FILL
END ARRAY
READ START
NST=1
XSM=-36.576 XSP=36.576
YSM=-18.288 YSP=18.288
ZSM=21.59 ZSP=94.09
END START
READ PLOT

TTL="PLAN VIEW 1/6 SCALE OF CORE, Z=MIDLEVEL OF ANNULI/INSERTS"
XUL=-91.44 YUL=91.44 ZUL=59.69
XLR=91.44 YLR=-91.44 ZLR=59.69
UAX=1. VDN=-1. DLX=1.524 NCH=* U.WGS* END

TTL="PLAN VIEW 1/6 SCALE OF CORE, Z=MIDLEVEL OF GRATING"
XUL=-91.44 YUL=91.44 ZUL=20.0025
XLR=91.44 YLR=-91.44 ZLR=20.0025
UAX=1. VDN=-1. DLX=1.524 NCH=* U.WGS* END

TTL="PLAN VIEW 1/6 SCALE OF CORE, Z=MIDLEVEL OF FIR TIMBERS"
XUL=-91.44 YUL=91.44 ZUL=9.2075
XLR=91.44 YLR=-91.44 ZLR=9.2075
UAX=1. VDN=-1. DLX=1.524 NCH=* U.WGS* END

TTL="PLAN VIEW 1/10 SCALE OF MOCKUP, Z=MIDLEVEL OF U UNITS"
XUL=-135. YUL=135. ZUL=59.69
XLR=135. YLR=-135. ZLR=59.69
UAX=1. VDN=-1. DLX=2.54 NCH=* U.WGS* END

TTL="PLAN VIEW 2X SCALE OF SINGLE U UNIT, Z=MIDLEVEL OF UNIT"
XUL=0.0 YUL=18.288 ZUL=59.69
XLR=18.288 YLR=0. ZLR=59.69
UAX=1. VDN=-1. DLX=0.127 NCH=* U.WGS* END

TTL="CROSS SECTION OF CORE 1/6 SCALE, Y=9.144"
XUL=-91.44 YUL=9.144 ZUL=110.
XLR=91.44 YLR=9.144 ZLR=-10.
UAX=1. WDN=-1. DLX=1.524 NCH=* U.WGS* END

TTL="CROSS SECTION OF MOCKUP 1/10 SCALE, Y=9.144"
XUL=-135. YUL=9.144 ZUL=125.
XLR=135. YLR=9.144 ZLR=-10.
UAX=1. WDN=-1. DLX=2.54 NCH=* U.WGS* END

TTL="CROSS SECTION OF GRATING/FIR TIMBERS, FULL SCALE"
XUL=0. YUL=0. ZUL=24.13
XLR=25.4 YLR=0. ZLR=-3.0
UAX=1. WDN=-1. DLX=.254 NCH=* U.WGS* END

TTL="PLAN VIEW OF GRATING THRU TIEBARS, FULL SCALE"
XUL=0. YUL=25.4 ZUL=21.193
XLR=25.4 YLR=0. ZLR=21.193
UAX=1. VDN=-1. DLX=.254 NCH=* U.WGS* END

TTL="PLAN VIEW OF GRATING @ GRATING MIDLEVEL, FULL SCALE"
XUL=0. YUL=25.4 ZUL=20.0025
XLR=25.4 YLR=0. ZLR=20.0025
UAX=1. VDN=-1. DLX=.254 NCH=* U.WGS* END

TTL="PLAN VIEW OF TIMBERS @ TIMBER MIDLEVEL, FULL SCALE"
XUL=0. YUL=25.4 ZUL=9.2075
XLR=25.4 YLR=-25.4 ZLR=9.2075
UAX=1. VDN=-1. DLX=.254 NCH=* U.WGS* END

TTL="CROSS SECTION OF CENTRAL UNIT, FULL SCALE, Y=9.144"
XUL=0.0 YUL=9.144 ZUL=110.
XLR=18.288 YLR=9.144 ZLR=-10.
UAX=1. WDN=-1. DLX=.254 NCH=* U.WGS* END

END PLOT
END DATA
END

CAB14
=CSAS25
CASE EBJ.12 U(3.85) 22 @ 2.5"/0.0"/0.35"/72.3CM, SQUARE
27GROUPNDF4 INPHOMMEDIUM

' U(3.85) METAL
U-235 1 0. 1.8643E-3 END
U-238 1 0. 4.5971E-2 END

' FULL DENSITY WATER MODERATOR/REFLECTOR
H2O 2 1.0 END

' FIR TIMBER MODEL
C 3 0. 1.06802E-2 END
H 3 0. 2.21713E-2 END
O 3 0. 1.10850E-2 END

' STEEL FOR GRATING, TANK WALLS AND FLOOR
CARBONSTEEL 4 1.0 END

' STAINLESS STEEL LINING FOR TANK
SS304 5 1.0 END

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Table A.2 (continued)

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END COMP
CASE EBJ.12 U(3.85) 22 @ 2.5"/0.0"/0.35"/72.3CM, SQUARE
READ PARM
NPG=600 NUB=YES PLT=NO PDN=YES TME=90 TBA=2
END PARM
READ GEOM

UNIT 1
COM=* FIR TIMBER 7.25" X 72" X 7.25" *
CUBOID 3 1 182.88 0. 18.415 0. 18.415 0.

UNIT 2
COM=* WATER GAP 3.5" X 72" X 7.25" BETWEEN TIMBERS *
CUBOID 2 1 182.88 0. 8.89 0. 18.415 0.

UNIT 3
COM=* ARRAY OF TIMBERS 72" X 72" X 7.25" *
ARRAY 1 3*0.0
REPLICATE 2 1 2R0. 2R0.3175 2R0. 1
REPLICATE 2 1 4R30.48 2R0. 1

UNIT 4
COM=* SECTION OF STEEL GRATING *
CUBOID 4 1 2.778125 .238125 .396875 -.396875 3.175 2.38125
CUBOID 2 1 2.778125 .238125 4.524375 -4.524375 3.175 0.
CUBOID 4 1 3.01625 0. 4.524375 -4.524375 3.175 0.

UNIT 5
COM=* ARRAY OF STEEL GRATING *
ARRAY 2 3*0.0
REPLICATE 2 1 4R0.9525 2R0.0 1
REPLICATE 2 1 4R30.48 2R0. 1

UNIT 6
COM=* U(3.85) ROD, H=72.3, SUBMERGED *
CYLINDER 1 1 1.419903 72.3 0.
CYLINDER 1 1 2.008046 72.3 0.
CYLINDER 1 1 2.459344 72.3 0.
CYLINDER 1 1 2.839806 72.3 0.
CYLINDER 1 1 3.175000 72.3 0.
CUBOID 2 1 4P3.6195 72.3 0.

UNIT 7
COM=* WATER CUBOID TO COMPLETE ARRAY 3 *
CUBOID 2 1 4P3.6195 72.3 0.

UNIT 8
COM=* U(3.85) ROD, H=3.9, DRY *
CYLINDER 1 1 1.419903 3.9 0.
CYLINDER 1 1 2.008046 3.9 0.
CYLINDER 1 1 2.459344 3.9 0.
CYLINDER 1 1 2.839806 3.9 0.
CYLINDER 1 1 3.175000 3.9 0.
CUBOID 0 1 4P3.6195 3.9 0.

UNIT 9
COM=* VOID CUBOID TO COMPLETE ARRAY 4 *
CUBOID 0 1 4P3.6195 3.9 0.

UNIT 10
COM=* U(3.85) ROD ARRAY, H=72.3, SUBMERGED *
ARRAY 3 3*0.0
REPLICATE 2 1 4R73.3425 2R0. 1
REPLICATE 2 1 4R30.48 2R0. 1

UNIT 11
COM=* ARRAY OF 22 U(3.85) RODS, H=3.9, DRY *
ARRAY 4 3*0.0
REPLICATE 0 1 4R73.3425 2R0. 1
REPLICATE 0 1 4R30.48 2R0. 1

CORE 5 1 -121.92 -121.92 0.
REPLICATE 5 1 5R0.0 0.1905 1
REPLICATE 4 1 5R0.0 2.54 1
END GEOM
READ ARRAY
ARA=1 NUX=1 NUY=13 NUZ=1
FILL 1 2 5Q2 1 END FILL
ARA=2 NUX=60 NUY=20 NUZ=1
FILL F4 END FILL
ARA=3 NUX=5 NUY=5 NUZ=1
FILL 2R6 3R7 20R6 END FILL
ARA=4 NUX=5 NUY=5 NUZ=1
FILL 2R8 3R9 20R8 END FILL
GBL=5
ARA=5 NUX=1 NUY=1 NUZ=4
FILL 3 5 10 11 END FILL
END ARRAY
READ START
NST=1
XSM=-18.0975 XSP=18.0975
YSM=-18.0975 YSP=18.0975
ZSM=21.59 ZSP=93.89
END START
RRAD PLOT

TTL="PLAN VIEW 1/6 SCALE OF CORE, Z=MIDLEVEL OF ANNULI/INSERTS"
XUL=-91.44 YUL=91.44 ZUL=59.69
XLR=91.44 YLR=-91.44 ZLR=59.69
UAX=1. VDN=-1. DLX=1.524 NCH=* U.WGS* END

TTL="PLAN VIEW OF ARRAY, FULL SCALE"
XUL=-18.0975 YUL=18.0975 ZUL=59.69
XLR=18.0975 YLR=-18.0975 ZLR=59.69
UAX=1. VDN=-1. DLX=.254 NCH=* U.WGS* END

TTL="PLAN VIEW 1/6 SCALE OF CORE, Z=MIDLEVEL OF GRATING"
XUL=-91.44 YUL=91.44 ZUL=20.0025
XLR=91.44 YLR=-91.44 ZLR=20.0025
UAX=1. VDN=-1. DLX=1.524 NCH=* U.WGS* END

TTL="PLAN VIEW 1/6 SCALE OF CORE, Z=MIDLEVEL OF FIR TIMBERS"
XUL=-91.44 YUL=91.44 ZUL=9.2075
XLR=91.44 YLR=-91.44 ZLR=9.2075
UAX=1. VDN=-1. DLX=1.524 NCH=* U.WGS* END

TTL="PLAN VIEW 1/10 SCALE OF MOCKUP, Z=MIDLEVEL OF U UNITS"
XUL=-135. YUL=135. ZUL=59.69
XLR=135. YLR=-135. ZLR=59.69
UAX=1. VDN=-1. DLX=2.54 NCH=* U.WGS* END

TTL="PLAN VIEW 2X SCALE OF SINGLE U UNIT, Z=MIDLEVEL OF UNIT"
XUL=-3.6195 YUL=3.6195 ZUL=59.69
XLR=3.6195 YLR=-3.6195 ZLR=59.69
UAX=1. VDN=-1. DLX=0.127 NCH=* U.WGS* END

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Table A.2 (continued)

TTL="CROSS SECTION OF CORE 1/6 SCALE,Y=0.0"
 XUL=-91.44 YUL=0.0 ZUL=110.
 XLR=91.44 YLR=0.0 ZLR=-10.
 UAX=1. WDN=-1. DLX=1.524 NCH=* U.WGS* END

TTL="CROSS SECTION OF MOCKUP 1/10 SCALE,Y=0.0"
 XUL=-135. YUL=0.0 ZUL=125.
 XLR=135. YLR=0.0 ZLR=-10.
 UAX=1. WDN=-1. DLX=2.54 NCH=* U.WGS* END

TTL="CROSS SECTION OF GRATING/FIR TIMBERS, FULL SCALE"
 XUL=0. YUL=0. ZUL=24.13
 XLR=25.4 YLR=0. ZLR=-3.0
 UAX=1. WDN=-1. DLX=.254 NCH=* U.WGS* END

TTL="PLAN VIEW OF GRATING THRU TIEBARS, FULL SCALE"
 XUL=0. YUL=25.4 ZUL=21.193
 XLR=25.4 YLR=0. ZLR=21.193
 UAX=1. VDN=-1. DLX=.254 NCH=* U.WGS* END

TTL="PLAN VIEW OF GRATING @ GRATING MIDLEVEL, FULL SCALE"
 XUL=0. YUL=25.4 ZUL=20.0025
 XLR=25.4 YLR=0. ZLR=20.0025
 UAX=1. VDN=-1. DLX=.254 NCH=* U.WGS* END

TTL="PLAN VIEW OF TIMBERS @ TIMBER MIDLEVEL, FULL SCALE"
 XUL=0. YUL=25.4 ZUL=9.2075
 XLR=25.4 YLR=-25.4 ZLR=9.2075
 UAX=1. VDN=-1. DLX=.254 NCH=* U.WGS* END

TTL="CROSS SECTION OF CENTRAL UNIT, 2XL SCALE,Y=0.0"
 XUL=-3.6195 YUL=0.0 ZUL=110.
 XLR=3.6195 YLR=0.0 ZLR=-10.
 UAX=1. WDN=-1. DLX=.127 NCH=* U.WGS* END

END PLOT
 END DATA
 END

CAB15
 =CSAS25
 CASE EBJ.13 U(3.85) 15 @ 2.5"/0.0"/0.75"/64.8CM, SQUARE
 27GROUPNDF4 INFHOMMEDIUM

' U(3.85) METAL
 U-235 1 0. 1.8643E-3 END
 U-238 1 0. 4.5971E-2 END

' FULL DENSITY WATER MODERATOR/REFLECTOR
 H2O 2 1.0 END

' FIR TIMBER MODEL
 C 3 0. 1.06802E-2 END
 H 3 0. 2.21713E-2 END
 O 3 0. 1.10850E-2 END

' STEEL FOR GRATING, TANK WALLS AND FLOOR
 CARBONSTEEL 4 1.0 END

' STAINLESS STEEL LINING FOR TANK
 SS304 5 1.0 END

END COMP
 CASE EBJ.13 U(3.85) 15 @ 2.5"/0.0"/0.75"/64.8CM, SQUARE
 READ PARM
 NPG=600 NUB=YES PLT=NO FDN=YES TME=90 TBA=2
 END PARM
 READ GEOM

UNIT 1
 COM=* FIR TIMBER 7.25" X 72" X 7.25" *
 CUBOID 3 1 182.88 0. 18.415 0. 18.415 0.

UNIT 2
 COM=* WATER GAP 3.5" X 72" X 7.25" BETWEEN TIMBERS *
 CUBOID 2 1 182.88 0. 8.89 0. 18.415 0.

UNIT 3
 COM=* ARRAY OF TIMBERS 72" X 72" X 7.25" *
 ARRAY 1 3*0.0
 REPLICATE 2 1 2R0. 2R0.3175 2R0. 1
 REPLICATE 2 1 4R30.48 2R0. 1

UNIT 4
 COM=* SECTION OF STEEL GRATING *
 CUBOID 4 1 2.778125 .238125 .396875 -.396875 3.175 2.38125
 CUBOID 2 1 2.778125 .238125 4.524375 -4.524375 3.175 0.
 CUBOID 4 1 3.01625 0. 4.524375 -4.524375 3.175 0.

UNIT 5
 COM=* ARRAY OF STEEL GRATING *
 ARRAY 2 3*0.0
 REPLICATE 2 1 4R0.9525 2R0.0 1
 REPLICATE 2 1 4R30.48 2R0. 1

UNIT 6
 COM=* U(3.85) ROD, H=64.8, SUBMERGED *
 CYLINDER 1 1 1.419903 64.8 0.
 CYLINDER 1 1 2.008046 64.8 0.
 CYLINDER 1 1 2.459344 64.8 0.
 CYLINDER 1 1 2.839806 64.8 0.
 CYLINDER 1 1 3.175000 64.8 0.
 CUBOID 2 1 4P4.1275 64.8 0.

Table A.2 (continued)

```

UNIT 7
COM=* WATER CUBOID TO COMPLETE ARRAY 3 *
CUBOID 2 1 4P4.1275 64.8 0.

UNIT 8
COM=* U(3.85) ROD, H=11.4, DRY *
CYLINDER 1 1 1.419903 11.4 0.
CYLINDER 1 1 2.008046 11.4 0.
CYLINDER 1 1 2.459344 11.4 0.
CYLINDER 1 1 2.839806 11.4 0.
CYLINDER 1 1 3.175000 11.4 0.
CUBOID 0 1 4P4.1275 11.4 0.

UNIT 9
COM=* VOID CUBOID TO COMPLETE ARRAY 4 *
CUBOID 0 1 4P4.1275 11.4 0.

UNIT 10
COM=* U(3.85) ROD ARRAY, H=64.8, SUBMERGED *
ARRAY 3 3*0.0
REPLICATE 2 1 4R74.93 2R0. 1
REPLICATE 2 1 4R30.48 2R0. 1

UNIT 11
COM=* ARRAY OF 15 RODS, H=11.4, DRY *
ARRAY 4 3*0.0
REPLICATE 0 1 4R74.93 2R0. 1
REPLICATE 0 1 4R30.48 2R0. 1

CORE 5 1 -121.92 -121.92 0.
REPLICATE 5 1 5R0.0 0.1905 1
REPLICATE 4 1 5R0.0 2.54 1
END GEOM
READ ARRAY
ARA=1 NUX=1 NUY=13 NUZ=1
FILL 1 2 5Q2 1 END FILL
ARA=2 NUX=60 NUY=20 NUZ=1
FILL F4 END FILL
ARA=3 NUX=4 NUY=4 NUZ=1
FILL 3R6 7 12R6 END FILL
ARA=4 NUX=4 NUY=4 NUZ=1
FILL 3R8 9 12R8 END FILL
GBL=5
ARA=5 NUX=1 NUY=1 NUZ=4
FILL 3 5 10 11 END FILL
END ARRAY
READ START
NST=1
XSM=-16.51 XSP=16.51
YSM=-16.51 YSP=16.51
ZSM=21.59 ZSP=86.39
END START
READ PLOT

TTL="PLAN VIEW 1/6 SCALE OF CORE, Z=MIDLEVEL OF ANNULI/INSERTS"
XUL=-91.44 YUL=91.44 ZUL=59.69
XLR=91.44 YLR=-91.44 ZLR=59.69
UAX=1. VDN=-1. DLX=1.524 NCH=* U.WGS* END

TTL="PLAN VIEW FULL SCALE OF ARRAY, Z=MIDLEVEL OF UNITS"
XUL=-16.51 YUL=16.51 ZUL=59.69
XLR=16.51 YLR=-16.51 ZLR=59.69
UAX=1. VDN=-1. DLX=.254 NCH=* U.WGS* END

TTL="PLAN VIEW 1/6 SCALE OF CORE, Z=MIDLEVEL OF GRATING"
XUL=-91.44 YUL=91.44 ZUL=20.0025
XLR=91.44 YLR=-91.44 ZLR=20.0025
UAX=1. VDN=-1. DLX=1.524 NCH=* U.WGS* END

TTL="PLAN VIEW 1/6 SCALE OF CORE, Z=MIDLEVEL OF FIR TIMBERS"
XUL=-91.44 YUL=91.44 ZUL=9.2075
XLR=91.44 YLR=-91.44 ZLR=9.2075
UAX=1. VDN=-1. DLX=1.524 NCH=* U.WGS* END

TTL="PLAN VIEW 1/10 SCALE OF MOCKUP, Z=MIDLEVEL OF U UNITS"
XUL=-135. YUL=135. ZUL=59.69
XLR=135. YLR=-135. ZLR=59.69
UAX=1. VDN=-1. DLX=2.54 NCH=* U.WGS* END

TTL="PLAN VIEW 2X SCALE OF SINGLE U UNIT, Z=MIDLEVEL OF UNIT"
XUL=0.0 YUL=8.255 ZUL=59.69
XLR=8.255 YLR=0.0 ZLR=59.69
UAX=1. VDN=-1. DLX=0.127 NCH=* U.WGS* END

TTL="CROSS SECTION OF CORE 1/6 SCALE, Y=4.1275"
XUL=-91.44 YUL=4.1275 ZUL=110.
XLR=91.44 YLR=4.1275 ZLR=-10.
UAX=1. WDN=-1. DLX=1.524 NCH=* U.WGS* END

TTL="CROSS SECTION OF MOCKUP 1/10 SCALE, Y=4.1275"
XUL=-135. YUL=4.1275 ZUL=125.
XLR=135. YLR=4.1275 ZLR=-10.
UAX=1. WDN=-1. DLX=2.54 NCH=* U.WGS* END

TTL="CROSS SECTION OF GRATING/FIR TIMBERS, FULL SCALE"
XUL=0. YUL=0. ZUL=24.13
XLR=25.4 YLR=0. ZLR=-3.0
UAX=1. WDN=-1. DLX=.254 NCH=* U.WGS* END

TTL="PLAN VIEW OF GRATING THRU TIEBARS, FULL SCALE"
XUL=0. YUL=25.4 ZUL=21.193
XLR=25.4 YLR=0. ZLR=21.193
UAX=1. VDN=-1. DLX=.254 NCH=* U.WGS* END

TTL="PLAN VIEW OF GRATING @ GRATING MIDLEVEL, FULL SCALE"
XUL=0. YUL=25.4 ZUL=20.0025
XLR=25.4 YLR=0. ZLR=20.0025
UAX=1. VDN=-1. DLX=.254 NCH=* U.WGS* END

TTL="PLAN VIEW OF TIMBERS @ TIMBER MIDLEVEL, FULL SCALE"
XUL=0. YUL=25.4 ZUL=9.2075
XLR=25.4 YLR=-25.4 ZLR=9.2075
UAX=1. VDN=-1. DLX=.254 NCH=* U.WGS* END

TTL="CROSS SECTION OF CENTRAL UNIT, 2X SCALE, Y=4.1275"
XUL=0.0 YUL=4.1275 ZUL=110.
XLR=8.255 YLR=4.1275 ZLR=-10.
UAX=1. WDN=-1. DLX=.127 NCH=* U.WGS* END

END PLOT
END DATA
END

```

Table A.2 (continued)

```

CAB16
=CSAS25
CASE EBJ.14 U(3.85) 23 @ 2.5"/0.0"/1.50"/68.9CM, SQUARE
27GROUPNDF4 INPHOMMEDIUM

' U(3.85) METAL
U-235      1 0.  1.8643E-3 END
U-238      1 0.  4.5971E-2 END

' FULL DENSITY WATER MODERATOR/REFLECTOR
H2O        2 1.0      END

' FIR TIMBER MODEL
C          3 0.  1.06802E-2 END
H          3 0.  2.21713E-2 END
O          3 0.  1.10850E-2 END

' STEEL FOR GRATING, TANK WALLS AND FLOOR
CARBONSTEEL 4 1.0      END

' STAINLESS STEEL LINING FOR TANK
SS304      5 1.0      END

END COMP
CASE EBJ.14 U(3.85) 23 @ 2.5"/0.0"/1.50"/68.9CM, SQUARE
READ PARM
NPG=600 NUB=YES PLT=NO PDN=YES TME=90 TBA=2
END PARM
READ GEOM

UNIT 1
COM=* FIR TIMBER 7.25" X 72" X 7.25" *
CUBOID 3 1 182.88 0. 18.415 0. 18.415 0.

UNIT 2
COM=* WATER GAP 3.5" X 72" X 7.25" BETWEEN TIMBERS *
CUBOID 2 1 182.88 0. 8.89 0. 18.415 0.

UNIT 3
COM=* ARRAY OF TIMBERS 72" X 72" X 7.25" *
ARRAY 1 3*0.0
REPLICATE 2 1 2R0. 2R0.3175 2R0. 1
REPLICATE 2 1 4R30.48 2R0. 1

UNIT 4
COM=* SECTION OF STEEL GRATING *
CUBOID 4 1 2.778125 .238125 .396875 -.396875 3.175 2.38125
CUBOID 2 1 2.778125 .238125 4.524375 -4.524375 3.175 0.
CUBOID 4 1 3.01625 0. 4.524375 -4.524375 3.175 0.

UNIT 5
COM=* ARRAY OF STEEL GRATING *
ARRAY 2 3*0.0
REPLICATE 2 1 4R0.9525 2R0.0 1
REPLICATE 2 1 4R30.48 2R0. 1

UNIT 6
COM=* U(3.85) ROD, H=68.9, SUBMERGED *
CYLINDER 1 1 1.419903 68.9 0.
CYLINDER 1 1 2.008046 68.9 0.
CYLINDER 1 1 2.459344 68.9 0.
CYLINDER 1 1 2.839806 68.9 0.
CYLINDER 1 1 3.175000 68.9 0.
CUBOID 2 1 4P5.08 68.9 0.

```

```

UNIT 7
COM=* WATER CUBOID TO COMPLETE ARRAY 3 *
CUBOID 2 1 4P5.08 68.9 0.

UNIT 8
COM=* U(3.85) ROD, H=7.3, DRY *
CYLINDER 1 1 1.419903 7.3 0.
CYLINDER 1 1 2.008046 7.3 0.
CYLINDER 1 1 2.459344 7.3 0.
CYLINDER 1 1 2.839806 7.3 0.
CYLINDER 1 1 3.175000 7.3 0.
CUBOID 0 1 4P5.08 7.3 0.

UNIT 9
COM=* VOID CUBOID TO COMPLETE ARRAY 4 *
CUBOID 0 1 4P5.08 7.3 0.

UNIT 10
COM=* U(3.85) ROD ARRAY, H=68.9, SUBMERGED *
ARRAY 3 3*0.0
REPLICATE 2 1 4R66.04 2R0. 1
REPLICATE 2 1 4R30.48 2R0. 1

UNIT 11
COM=* ARRAY OF 22 U(3.85) RODS, H=7.3, DRY *
ARRAY 4 3*0.0
REPLICATE 0 1 4R66.04 2R0. 1
REPLICATE 0 1 4R30.48 2R0. 1

CORE 5 1 -121.92 -121.92 0.
REPLICATE 5 1 5R0.0 0.1905 1
REPLICATE 4 1 5R0.0 2.54 1
END GEOM
READ ARRAY
ARA=1 NUX=1 NUY=13 NUZ=1
FILL 1 2 5Q2 1 END FILL
ARA=2 NUX=60 NUY=20 NUZ=1
FILL P4 END FILL
ARA=3 NUX=5 NUY=5 NUZ=1
FILL 3R6 2R7 20R6 END FILL
ARA=4 NUX=5 NUY=5 NUZ=1
FILL 3R8 2R9 20R8 END FILL
GBL=5
ARA=5 NUX=1 NUY=1 NUZ=4
FILL 3 5 10 11 END FILL
END ARRAY
READ START
NST=1
XSM=-25.4 XSP=25.4
YSM=-25.4 YSP=25.4
ZSM=21.59 ZSP=90.49
END START
READ PLOT

TTL="PLAN VIEW 1/6 SCALE OF CORE, Z=MIDLEVEL OF ANNULI/INSERTS"
XUL=-91.44 YUL=91.44 ZUL=59.69
XLR=91.44 YLR=-91.44 ZLR=59.69
UAX=1. VDN=-1. DLX=1.524 NCH=* U.WGS* END

TTL="PLAN VIEW OF ARRAY, FULL SCALE"
XUL=-25.4 YUL=25.4 ZUL=59.69
XLR=25.4 YLR=-25.4 ZLR=59.69
UAX=1. VDN=-1. DLX=.254 NCH=* U.WGS* END

```

Table A.2 (continued)

```

TTL="PLAN VIEW 1/6 SCALE OF CORE, Z=MIDLEVEL OF GRATING"
XUL=-91.44 YUL=91.44 ZUL=20.0025
XLR=91.44 YLR=-91.44 ZLR=20.0025
UAX=1. VDN=-1. DLX=1.524 NCH=* U.WGS* END

TTL="PLAN VIEW 1/6 SCALE OF CORE, Z=MIDLEVEL OF FIR TIMBERS"
XUL=-91.44 YUL=91.44 ZUL=9.2075
XLR=91.44 YLR=-91.44 ZLR=9.2075
UAX=1. VDN=-1. DLX=1.524 NCH=* U.WGS* END

TTL="PLAN VIEW 1/10 SCALE OF MOCKUP, Z=MIDLEVEL OF U UNITS"
XUL=-135. YUL=135. ZUL=59.69
XLR=135. YLR=-135. ZLR=59.69
UAX=1. VDN=-1. DLX=2.54 NCH=* U.WGS* END

TTL="PLAN VIEW 2X SCALE OF SINGLE U UNIT, Z=MIDLEVEL OF UNIT"
XUL=-5.08 YUL=5.08 ZUL=59.69
XLR=5.08 YLR=-5.08 ZLR=59.69
UAX=1. VDN=-1. DLX=0.127 NCH=* U.WGS* END

TTL="CROSS SECTION OF CORE 1/6 SCALE,Y=0.0"
XUL=-91.44 YUL=0.0 ZUL=110.
XLR=91.44 YLR=0.0 ZLR=-10.
UAX=1. WDN=-1. DLX=1.524 NCH=* U.WGS* END

TTL="CROSS SECTION OF MOCKUP 1/10 SCALE,Y=0.0"
XUL=-135. YUL=0.0 ZUL=125.
XLR=135. YLR=0.0 ZLR=-10.
UAX=1. WDN=-1. DLX=2.54 NCH=* U.WGS* END

TTL="CROSS SECTION OF GRATING/FIR TIMBERS, FULL SCALE"
XUL=0. YUL=0. ZUL=24.13
XLR=25.4 YLR=0. ZLR=-3.0
UAX=1. WDN=-1. DLX=.254 NCH=* U.WGS* END

TTL="PLAN VIEW OF GRATING THRU TIEBARS, FULL SCALE"
XUL=0. YUL=25.4 ZUL=21.193
XLR=25.4 YLR=0. ZLR=21.193
UAX=1. VDN=-1. DLX=.254 NCH=* U.WGS* END

TTL="PLAN VIEW OF GRATING @ GRATING MIDLEVEL, FULL SCALE"
XUL=0. YUL=25.4 ZUL=20.0025
XLR=25.4 YLR=0. ZLR=20.0025
UAX=1. VDN=-1. DLX=.254 NCH=* U.WGS* END

TTL="PLAN VIEW OF TIMBERS @ TIMBER MIDLEVEL, FULL SCALE"
XUL=0. YUL=25.4 ZUL=9.2075
XLR=25.4 YLR=-25.4 ZLR=9.2075
UAX=1. VDN=-1. DLX=.254 NCH=* U.WGS* END

TTL="CROSS SECTION OF CENTRAL UNIT, 2X SCALE,Y=0.0"
XUL=-5.08 YUL=0.0 ZUL=110.
XLR=5.08 YLR=0.0 ZLR=-10.
UAX=1. WDN=-1. DLX=.127 NCH=* U.WGS* END

END PLOT
END DATA
END

```

Table A.3. Table 3 input data

```
CAS04
=CSAS25
BRITISH HANDBOOK OF CRITICALITY SAFETY U(1.42)F4 & PARAFFIN (CASE 04)
27GROUPNDF4 INFHOMMEDIUM
UF4      1 0.4903 293 92235 1.4023 92238 98.5977 END
' NOTE: THE ENRICHMENT GIVEN IN THE REFERENCE IS NOT WEIGHT PERCENT
PARAFFIN 1 0.4572 END
END COMP
BRITISH HANDBOOK OF CRITICALITY SAFETY U(1.42)F4 & PARAFFIN (CASE 04)
READ PARM NPG=600 NUB=YES FDN=YES END PARM
READ GEOM
CUBOID 1 1 2P46.55 2P46.50 2P61.9
END GEOM
END DATA
END
```

```
CAS05
=CSAS25
BRITISH HANDBOOK OF CRITICALITY SAFETY U(1.42)F4 & PARAFFIN (CASE 05)
27GROUPNDF4 INFHOMMEDIUM
UF4      1 0.4903 293 92235 1.4023 92238 98.5977 END
' NOTE: THE ENRICHMENT GIVEN IN THE REFERENCE IS NOT WEIGHT PERCENT
PARAFFIN 1 0.4572 END
END COMP
BRITISH HANDBOOK OF CRITICALITY SAFETY U(1.42)F4 & PARAFFIN (CASE 05)
READ PARM NPG=600 NUB=YES FDN=YES END PARM
READ GEOM
CUBOID 1 1 2P50.00 2P49.95 2P51.55
END GEOM
END DATA
END
```

```
CAS06
=CSAS25
BRITISH HANDBOOK OF CRITICALITY SAFETY U(1.42)F4 & PARAFFIN (CASE 06)
27GROUPNDF4 INFHOMMEDIUM
UF4      1 0.4903 293 92235 1.4023 92238 98.5977 END
' NOTE: THE ENRICHMENT GIVEN IN THE REFERENCE IS NOT WEIGHT PERCENT
PARAFFIN 1 0.4572 END
END COMP
BRITISH HANDBOOK OF CRITICALITY SAFETY U(1.42)F4 & PARAFFIN (CASE 06)
READ PARM NPG=600 NUB=YES FDN=YES END PARM
READ GEOM
CUBOID 1 1 2P65.35 2P65.3 2P37.1
END GEOM
END DATA
END
=CSAS25
BRITISH HANDBOOK OF CRITICALITY SAFETY U(1.42)F4 & PARAFFIN (CASE 06)
HANSEN-ROACH INFHOMMEDIUM
UF4      1 0.4903 293 92235 1.4023 92238 98.5977 END
' NOTE: THE ENRICHMENT GIVEN IN THE REFERENCE IS NOT WEIGHT PERCENT
PARAFFIN 1 0.4572 END
END COMP
BRITISH HANDBOOK OF CRITICALITY SAFETY U(1.42)F4 & PARAFFIN (CASE 06)
READ PARM NPG=600 NUB=YES FDN=YES END PARM
READ GEOM
CUBOID 1 1 2P65.35 2P65.3 2P37.1
END GEOM
END DATA
END
```

```
CAS11
=CSAS25
RAFFETY AND MILHALCZO U(2)F4-1 REFLECTED (CASE 11)
27GROUPNDF4 INFHOMMEDIUM
U-235 1 0 1.5811E-4 END
U-238 1 0 7.6467E-3 END
H      1 0 3.0864E-2 END
C      1 0 1.4839E-2 END
F      1 0 3.1219E-2 END
PARAFFIN 2 1.0 END
PLEXIGLASS 3 0.918 END
AL      3 0.062 END
END COMP
RAFFETY AND MALHALCZO U(2)F4-1 REFLECTED (CASE 11)
READ PARM RUN=YES NPG=600 NUB=YES FDN=YES END PARM
READ GEOM
UNIT 1
CUBOID 1 1 4P28.110 2P56.44
REPLICATE 2 2 5*3.048 0.0 5
UNIT 2
CUBOID 3 1 4P28.110 2*0.0
REPLICATE 3 2 4*3.048 0.0 3.048 5
END GEOM
READ ARRAY
NUX=1 NUY=1 NUZ=2
FILL 2 1 END FILL
END ARRAY
READ BIAS ID=400 2 6 END BIAS
END DATA
END
=CSAS25
RAFFETY AND MILHALCZO U(2)F4-1 REFLECTED (CASE 11)
HANSEN-ROACH INFHOMMEDIUM
U-235 1 0 1.5811E-4 END
U-238 1 0 7.6467E-3 END
H      1 0 3.0864E-2 END
C      1 0 1.4839E-2 END
F      1 0 3.1219E-2 END
PARAFFIN 2 1.0 END
PLEXIGLASS 3 0.918 END
AL      3 0.062 END
END COMP
RAFFETY AND MALHALCZO U(2)F4-1 REFLECTED (CASE 11)
READ PARM RUN=YES PLT=NO NPG=600 NUB=YES FDN=YES END PARM
READ GEOM
UNIT 1
CUBOID 1 1 4P28.110 2P56.44
REPLICATE 2 2 5*3.048 0.0 5
UNIT 2
CUBOID 3 1 4P28.110 2*0.0
REPLICATE 3 2 4*3.048 0.0 3.048 5
END GEOM
READ ARRAY
NUX=1 NUY=1 NUZ=2
FILL 2 1 END FILL
END ARRAY
READ BIAS ID=400 2 6 END BIAS
READ PLOT TTL='XZ SLICE OF CASE 11 SHOWING BIASING REGIONS'
XUL=-1 YUL=20 ZUL=146
XLR=88 YLR=20 ZLR=-3
UAX=1 WDN=-1 NAX=130 NCH='0123456'
PIC=WTS
END PLOT
END DATA
END
```

Table A.3 (continued)

```

CAS12
=CSAS25
RAFFETY AND MILHALCZO U(2)F4-1 UNREFLECTED (CASE 12)
27GROUPNDF4  INPHOMMEDIUM
U-235  1 0 1.5811E-4  END
U-238  1 0 7.6467E-3  END
H      1 0 3.0864E-2  END
C      1 0 1.4839E-2  END
F      1 0 3.1219E-2  END
END COMP
RAFFETY AND MALHALCZO U(2)F4-1 UNREFLECTED (CASE12)
READ PARM  NPG=600 NUB=YES FDN=YES END PARM
READ GEOM
CUBOID  1 1 35.735 -35.735 35.735 -35.735 47.07 -47.07
END GEOM
END DATA
END
=CSAS25
RAFFETY AND MILHALCZO U(2)F4-1 UNREFLECTED (CASE 12)
HANSEN-ROACH  INPHOMMEDIUM
U-235  1 0 1.5811E-4  END
U-238  1 0 7.6467E-3  END
H      1 0 3.0864E-2  END
C      1 0 1.4839E-2  END
F      1 0 3.1219E-2  END
END COMP
RAFFETY AND MALHALCZO U(2)F4-1 UNREFLECTED (CASE12)
READ PARM  NPG=600 NUB=YES FDN=YES END PARM
READ GEOM
CUBOID  1 1 35.735 -35.735 35.735 -35.735 47.07 -47.07
END GEOM
END DATA
END
CAS13
=CSAS25
RAFFETY AND MILHALCZO U(2)F4-2 REFLECTED (CASE 13) NO BIASING
27GROUPNDF4  INPHOMMEDIUM
U-235  1 0 1.3303E-4  END
U-238  1 0 6.4370E-3  END
H      1 0 3.9097E-2  END
C      1 0 1.8797E-2  END
F      1 0 2.6280E-2  END
PARAFFIN  2 1.0  END
PLEXIGLASS  3 0.918  END
AL         3 0.062  END
END COMP
RAFFETY AND MALHALCZO U(2)F4-2 REFLECTED (CASE 13) NO BIASING
READ PARM  RUN=YES NPG=600 NUB=YES FDN=YES END PARM
READ GEOM
UNIT 1
CUBOID  1 1 4P25.555 2P36.935
REPLICATE  2 2 5*3.048 0.0 5
UNIT 2
CUBOID  3 1 4P25.555 2*0.0
REPLICATE  3 2 4*3.048 0.0 3.048 5
END GEOM
READ ARRAY
NUX=1  NUY=1  NUZ=2
FILL  2 1  END FILL
END ARRAY
' READ BIAS ID=400  2 6  END BIAS
END DATA
END

```

```

=CSAS25
RAFFETY AND MILHALCZO U(2)F4-2 REFLECTED (CASE 13) NO BIASING
HANSEN-ROACH  INPHOMMEDIUM
U-235  1 0 1.3303E-4  END
U-238  1 0 6.4370E-3  END
H      1 0 3.9097E-2  END
C      1 0 1.8797E-2  END
F      1 0 2.6280E-2  END
PARAFFIN  2 1.0  END
PLEXIGLASS  3 0.918  END
AL         3 0.062  END
END COMP
RAFFETY AND MALHALCZO U(2)F4-2 REFLECTED (CASE 13) NO BIASING
READ PARM  RUN=YES PLT=NO NPG=600 NUB=YES FDN=YES END PARM
READ GEOM
UNIT 1
CUBOID  1 1 4P25.555 2P36.935
REPLICATE  2 2 5*3.048 0.0 5
UNIT 2
CUBOID  3 1 4P25.555 2*0.0
REPLICATE  3 2 4*3.048 0.0 3.048 5
END GEOM
READ ARRAY
NUX=1  NUY=1  NUZ=2
FILL  2 1  END FILL
END ARRAY
' READ BIAS ID=400  2 6  END BIAS
READ PLOT TTL='XZ SLICE OF CASE 13 SHOWING BIASING REGIONS'
XUL=-1  YUL=20  ZUL=106
XLR=83  YLR=20  ZLR=-3
UAX=1  WDN=-1  NAX=130  NCH='0123456'
PIC=WTS
END PLOT
END DATA
END

```

Table A.3 (continued)

```

CAS14
=CSAS25
RAFFETY AND MILHALCZO U(2)F4-2 UNREFLECTED (CASE 14)
27GROUPNDF4  INFHOMMEDIUM
U-235  1 0 1.3303E-4 END
U-238  1 0 6.4370E-3 END
H      1 0 3.9097E-2 END
C      1 0 1.8797E-2 END
F      1 0 2.6280E-2 END
END COMP
RAFFETY AND MALHALCZO U(2)F4-2 UNREFLECTED (CASE 14)
READ PARM  NPG=600 NUB=YES FDN=YES END PARM
READ GEOM
CUBOID  1 1 28.11 -28.11 28.11 -28.11 61.235 -61.235
END GEOM
END DATA
END
=CSAS25
RAFFETY AND MILHALCZO U(2)F4-2 UNREFLECTED (CASE 14)
HANSEN-ROACH  INFHOMMEDIUM
U-235  1 0 1.3303E-4 END
U-238  1 0 6.4370E-3 END
H      1 0 3.9097E-2 END
C      1 0 1.8797E-2 END
F      1 0 2.6280E-2 END
END COMP
RAFFETY AND MALHALCZO U(2)F4-2 UNREFLECTED (CASE 14)
READ PARM  NPG=600 NUB=YES FDN=YES END PARM
READ GEOM
CUBOID  1 1 28.11 -28.11 28.11 -28.11 61.235 -61.235
END GEOM
END DATA
END
CAS15
=CSAS25
RAFFETY AND MALHALCZO U(2)F4-3 REFLECTED (CASE 15)
27GROUPNDF4  INFHOMMEDIUM
U-235  1 0 1.1191E-4 END
U-238  1 0 5.4152E-3 END
H      1 0 4.5472E-2 END
C      1 0 2.1861E-2 END
F      1 0 2.2109E-2 END
PARAFFIN  2 1.0 END
PLEXIGLASS  3 0.918 END
AL        3 0.062 END
END COMP
RAFFETY AND MALHALCZO U(2)F4-3 REFLECTED (CASE 15)
READ PARM  RUN=YES  NPG=600 NUB=YES FDN=YES END PARM
READ GEOM
UNIT  1
CUBOID  1 1 4P26.835 2P27.145
REPLICATE  2 2 5*3.048 0.0 5
UNIT  2
CUBOID  3 1 4P26.835 2*0.0
REPLICATE  3 2 4*3.048 0.0 3.048 5
END GEOM
READ ARRAY
NUX=1  NUY=1  NUZ=2
FILL  2 1 END FILL
END ARRAY
READ BIAS ID=400  2 6 END BIAS
READ PLOT TTL='XZ SLICE OF CASE 15 SHOWING BIASING REGIONS'
XUL=-1  YUL=20  ZUL=86
XLR=86  YLR=20  ZLR=-3
UAX=1  WDN=-1  NAX=130  NCH='0123456'
PIC=WTS
END PLOT
END DATA
END

```

```

READ BIAS ID=400  2 6 END BIAS
END DATA
END
=CSAS25
RAFFETY AND MILHALCZO U(2)F4-3 REFLECTED (CASE 15)
HANSEN-ROACH  INFHOMMEDIUM
U-235  1 0 1.1191E-4 END
U-238  1 0 5.4152E-3 END
H      1 0 4.5472E-2 END
C      1 0 2.1861E-2 END
F      1 0 2.2109E-2 END
PARAFFIN  2 1.0 END
PLEXIGLASS  3 0.918 END
AL        3 0.062 END
END COMP
RAFFETY AND MALHALCZO U(2)F4-3 REFLECTED (CASE 15)
READ PARM  RUN=YES  NPG=600 NUB=YES FDN=YES END PARM
READ GEOM
UNIT  1
CUBOID  1 1 4P26.835 2P27.145
REPLICATE  2 2 5*3.048 0.0 5
UNIT  2
CUBOID  3 1 4P26.835 2*0.0
REPLICATE  3 2 4*3.048 0.0 3.048 5
END GEOM
READ ARRAY
NUX=1  NUY=1  NUZ=2
FILL  2 1 END FILL
END ARRAY
READ BIAS ID=400  2 6 END BIAS
READ PLOT TTL='XZ SLICE OF CASE 15 SHOWING BIASING REGIONS'
XUL=-1  YUL=20  ZUL=86
XLR=86  YLR=20  ZLR=-3
UAX=1  WDN=-1  NAX=130  NCH='0123456'
PIC=WTS
END PLOT
END DATA
END

```


Table A.3 (continued)

```

CAS16
=CSAS25
RAFFETY AND MILHALCZO U(2)F4-4 REFLECTED (CASE 16)
27GROUPNDF4  INFHOMMEDIUM
U-235  1 0 0.9924E-4  END
U-238  1 0 4.7998E-3  END
H      1 0 4.9212E-2  END
C      1 0 2.3660E-2  END
F      1 0 1.9596E-2  END
PARAFFIN  2 1.0  END
PLEXIGLASS  3 0.918  END
AL        3 0.062  END
END COMP
RAFFETY AND MALHALCZO U(2)F4-4 REFLECTED (CASE 16)
READ PARM  RUN=YES  NPG=600  NUB=YES  FDN=YES  END PARM
READ GEOM
UNIT 1
CUBOID  1 1 4P23.000 2P48.285
REPLICATE  2 2 5*3.048 0.0 5
UNIT 2
CUBOID  3 1 4P23.000 2*0.0
REPLICATE  3 2 4*3.048 0.0 3.048 5
END GEOM
READ ARRAY
NUX=1  NUY=1  NUZ=2
FILL  2 1  END FILL
END ARRAY
READ BIAS  ID=400  2 6  END BIAS
END DATA
END
=CSAS25
RAFFETY AND MILHALCZO U(2)F4-4 REFLECTED (CASE 16)
HANSEN-ROACH  INFHOMMEDIUM
U-235  1 0 0.9924E-4  END
U-238  1 0 4.7998E-3  END
H      1 0 4.9212E-2  END
C      1 0 2.3660E-2  END
F      1 0 1.9596E-2  END
PARAFFIN  2 1.0  END
PLEXIGLASS  3 0.918  END
AL        3 0.062  END
END COMP
RAFFETY AND MALHALCZO U(2)F4-4 REFLECTED (CASE 16)
READ PARM  RUN=YES  PLT=NO  NPG=600  NUB=YES  FDN=YES  END PARM
READ GEOM
UNIT 1
CUBOID  1 1 4P23.000 2P48.285
REPLICATE  2 2 5*3.048 0.0 5
UNIT 2
CUBOID  3 1 4P23.000 2*0.0
REPLICATE  3 2 4*3.048 0.0 3.048 5
END GEOM
READ ARRAY
NUX=1  NUY=1  NUZ=2
FILL  2 1  END FILL
END ARRAY
READ BIAS  ID=400  2 6  END BIAS
READ PLOT  TTL='XZ SLICE OF CASE 16 SHOWING BIASING REGIONS'
XUL=-1  YUL=20  ZUL=129
XLR=79  YLR=20  ZLR=-3
UAX=1  WDN=-1  NAX=130  NCH='0123456'
PIC=WTS
END PLOT
END DATA
END

```

```

CAS17
=CSAS25
RAFFETY AND MILHALCZO U(2)F4-5 REFLECTED (CASE 17)
27GROUPNDF4  INFHOMMEDIUM
U-235  1 0 0.8667E-4  END
U-238  1 0 4.1941E-3  END
H      1 0 5.3187E-2  END
C      1 0 2.5570E-2  END
F      1 0 1.7123E-2  END
POLYETHYLENE  2 1.0  END
PLEXIGLASS  3 0.918  END
AL        3 0.062  END
END COMP
RAFFETY AND MALHALCZO U(2)F4-5 REFLECTED (CASE 17)
READ PARM  RUN=YES  NPG=600  NUB=YES  FDN=YES  END PARM
READ GEOM
UNIT 1
CUBOID  1 1 2P28.160 2P30.645 2P27.040
REPLICATE  2 2 5*3.048 0.0 5
UNIT 2
CUBOID  3 1 2P28.160 2P30.645 2*0.0
REPLICATE  3 2 4*3.048 0.0 3.048 5
END GEOM
READ ARRAY
NUX=1  NUY=1  NUZ=2
FILL  2 1  END FILL
END ARRAY
READ BIAS  ID=400  2 6  END BIAS
END DATA
END
=CSAS25
RAFFETY AND MILHALCZO U(2)F4-5 REFLECTED (CASE 17)
HANSEN-ROACH  INFHOMMEDIUM
U-235  1 0 0.8667E-4  END
U-238  1 0 4.1941E-3  END
H      1 0 5.3187E-2  END
C      1 0 2.5570E-2  END
F      1 0 1.7123E-2  END
POLYETHYLENE  2 1.0  END
PLEXIGLASS  3 0.918  END
AL        3 0.062  END
END COMP
RAFFETY AND MALHALCZO U(2)F4-5 REFLECTED (CASE 17)
READ PARM  RUN=YES  PLT=NO  NPG=600  NUB=YES  FDN=YES  END PARM
READ GEOM
UNIT 1
CUBOID  1 1 2P28.160 2P30.645 2P27.040
REPLICATE  2 2 5*3.048 0.0 5
UNIT 2
CUBOID  3 1 2P28.160 2P30.645 2*0.0
REPLICATE  3 2 4*3.048 0.0 3.048 5
END GEOM
READ ARRAY
NUX=1  NUY=1  NUZ=2
FILL  2 1  END FILL
END ARRAY
READ BIAS  ID=400  2 6  END BIAS
READ PLOT  TTL='XZ SLICE OF CASE 17 SHOWING BIASING REGIONS'
XUL=-1  YUL=20  ZUL=86
XLR=89  YLR=20  ZLR=-3
UAX=1  WDN=-1  NAX=130  NCH='0123456'
PIC=WTS
END PLOT
END DATA
END

```

Table A.3 (continued)

```

CAS18
=CSAS25
RAFFETY AND MILHALCZO U(2)F4-5 UNREFLECTED (CASE 18)
27GROUPNDF4 INFHOMMEDIUM
U-235 1 0 0.8667E-4 END
U-238 1 0 4.1941E-3 END
H 1 0 5.3187E-2 END
C 1 0 2.5570E-2 END
F 1 0 1.7123E-2 END
END COMP
RAFFETY AND MALHALCZO U(2)F4-5 UNREFLECTED (CASE18)
READ PARM NPG=600 NUB=YES FDN=YES END PARM
READ GEOM
CUBOID 1 1 30.65 -30.65 33.27 -33.27 33.26 -33.26
END GEOM
END DATA
END
=CSAS25
RAFFETY AND MILHALCZO U(2)F4-5 UNREFLECTED (CASE 18)
HANSEN-ROACH INFHOMMEDIUM
U-235 1 0 0.8667E-4 END
U-238 1 0 4.1941E-3 END
H 1 0 5.3187E-2 END
C 1 0 2.5570E-2 END
F 1 0 1.7123E-2 END
END COMP
RAFFETY AND MALHALCZO U(2)F4-5 UNREFLECTED (CASE18)
READ PARM NPG=600 NUB=YES FDN=YES END PARM
READ GEOM
CUBOID 1 1 30.65 -30.65 33.27 -33.27 33.26 -33.26
END GEOM
END DATA
END

```

```

CAS19
=CSAS25
RAFFETY AND MILHALCZO U(2)F4-6 REFLECTED (CASE 19)
27GROUPNDF4 INFHOMMEDIUM
U-235 1 0 0.6232E-4 END
U-238 1 0 3.0100E-3 END
H 1 0 6.0557E-2 END
C 1 0 2.9114E-2 END
F 1 0 1.2309E-2 END
POLYETHYLENE 2 1.0 END
PLEXIGLASS 3 0.918 END
AL 3 0.062 END
END COMP
RAFFETY AND MALHALCZO U(2)F4-6 REFLECTED (CASE 19)
READ PARM RUN=YES NPG=600 NUB=YES FDN=YES END PARM
READ GEOM
UNIT 1
CUBOID 1 1 2P38.255 2P38.220 2P41.210
REPLICATE 2 2 5*3.048 0.0 5
UNIT 2
CUBOID 3 1 2P38.255 2P38.220 2*0.0
REPLICATE 3 2 4*3.048 0.0 3.048 5
END GEOM
READ ARRAY
NUX=1 NUY=1 NUZ=2
FILL 2 1 END FILL
END ARRAY

```

```

READ BIAS ID=400 2 6 END BIAS
END DATA
END
=CSAS25
RAFFETY AND MILHALCZO U(2)F4-6 REFLECTED (CASE 19)
HANSEN-ROACH INFHOMMEDIUM
U-235 1 0 0.6232E-4 END
U-238 1 0 3.0100E-3 END
H 1 0 6.0557E-2 END
C 1 0 2.9114E-2 END
F 1 0 1.2309E-2 END
POLYETHYLENE 2 1.0 END
PLEXIGLASS 3 0.918 END
AL 3 0.062 END
END COMP
RAFFETY AND MALHALCZO U(2)F4-6 REFLECTED (CASE 19)
READ PARM RUN=YES PLT=NO NPG=600 NUB=YES FDN=YES END PARM
READ GEOM
UNIT 1
CUBOID 1 1 2P38.255 2P38.220 2P41.210
REPLICATE 2 2 5*3.048 0.0 5
UNIT 2
CUBOID 3 1 2P38.255 2P38.220 2*0.0
REPLICATE 3 2 4*3.048 0.0 3.048 5
END GEOM
READ ARRAY
NUX=1 NUY=1 NUZ=2
FILL 2 1 END FILL
END ARRAY
READ BIAS ID=400 2 6 END BIAS
READ PLOT TTL='XZ SLICE OF CASE 19 SHOWING BIASING REGIONS'
XUL=-1 YUL=20 ZUL=115
XLR=108 YLR=20 ZLR=-3
UAX=1 WDN=-1 NAX=130 NCH='0123456'
PIC=WTS
END PLOT
END DATA
END

```

Table A.3 (continued)

```

CAS20
=CSAS25
RAFFETY AND MILHALCZO U(2)F4-6 UNREFLECTED (CASE 20)
27GROUPNDF4  INPHOMMEDIUM
U-235  1 0 0.6232E-4  END
U-238  1 0 3.0100E-3  END
H      1 0 6.0557E-2  END
C      1 0 2.9114E-2  END
F      1 0 1.2309E-2  END
END COMP
RAFFETY AND MALHALCZO U(2)F4-6 UNREFLECTED (CASE20)
READ PARM  NPG=600 NUB=YES FDN=YES END PARM
READ GEOM
CUBOID  1 1 40.725 -40.725 43.35 -43.35 44.110 -44.110
END GEOM
END DATA
END
=CSAS25
RAFFETY AND MILHALCZO U(2)F4-6 UNREFLECTED (CASE 20)
HANSEN-ROACH  INPHOMMEDIUM
U-235  1 0 0.6232E-4  END
U-238  1 0 3.0100E-3  END
H      1 0 6.0557E-2  END
C      1 0 2.9114E-2  END
F      1 0 1.2309E-2  END
END COMP
RAFFETY AND MALHALCZO U(2)F4-6 UNREFLECTED (CASE20)
READ PARM  NPG=600 NUB=YES FDN=YES END PARM
READ GEOM
CUBOID  1 1 40.725 -40.725 43.35 -43.35 44.110 -44.110
END GEOM
END DATA
END

CAS21
=CSAS25
RAFFETY AND MILHALCZO U(3)F4-1 REFLECTED (CASE 21) NO BIAS
27GROUPNDF4  INPHOMMEDIUM
U-235  1 0 2.3494E-4  END
U-238  1 0 7.4999E-3  END
H      1 0 3.1341E-2  END
C      1 0 1.5067E-2  END
F      1 0 3.0939E-2  END
PARAFFIN  2 1.0  END
PLEXIGLASS  3 0.918  END
AL        3 0.062  END
END COMP
RAFFETY AND MILHALCZO U(3)F4-1 REFLECTED (CASE 21) NO BIAS
READ PARM  RUN=YES  NPG=600 NUB=YES FDN=YES END PARM
READ GEOM
UNIT  1
CUBOID  1 1 2P25.57 2P25.57 2P25.635
REPLICATE  2 2 5*3.048 0.0 5
UNIT  2
CUBOID  3 1 2P25.57 2P25.57 2*0.0
REPLICATE  3 2 4*3.048 0.0 3.048 5
END GEOM
READ ARRAY
NUX=1  NUY=1  NUZ=2
FILL  2 1  END FILL
END ARRAY
' READ BIAS ID=400  2 6  END BIAS
END DATA
END

```

```

=CSAS25
RAFFETY AND MILHALCZO U(3)F4-1 REFLECTED (CASE 21) NO BIAS
HANSEN-ROACH  INPHOMMEDIUM
U-235  1 0 2.3494E-4  END
U-238  1 0 7.4999E-3  END
H      1 0 3.1341E-2  END
C      1 0 1.5067E-2  END
F      1 0 3.0939E-2  END
PARAFFIN  2 1.0  END
PLEXIGLASS  3 0.918  END
AL        3 0.062  END
END COMP
RAFFETY AND MILHALCZO U(3)F4-1 REFLECTED (CASE 21) NO BIAS
READ PARM  RUN=YES PLT=NO NPG=600 NUB=YES FDN=YES END PARM
READ GEOM
UNIT  1
CUBOID  1 1 2P25.57 2P25.57 2P25.635
REPLICATE  2 2 5*3.048 0.0 5
UNIT  2
CUBOID  3 1 2P25.57 2P25.57 2*0.0
REPLICATE  3 2 4*3.048 0.0 3.048 5
END GEOM
READ ARRAY
NUX=1  NUY=1  NUZ=2
FILL  2 1  END FILL
END ARRAY
' READ BIAS ID=400  2 6  END BIAS
READ PLOT TTL='XZ SLICE OF CASE 21 SHOWING BIASING REGIONS'
XUL=-1  YUL=20  ZUL=83
XLR=83  YLR=20  ZLR=-3
UAX=1  WDN=-1  NAX=130  NCH='0123456'
PIC=WTS
END PLOT
END DATA
END

```

Table A.3 (continued)

```

CAS23
=CSAS25
RAFFETY AND MILHALCZO U(3)F4-1 REFLECTED (CASE 23)
27GROUPNDF#  INFHOMMEDIUM
U-235  1 0 2.3494E-4  END
U-238  1 0 7.4999E-3  END
H      1 0 3.1341E-2  END
C      1 0 1.5067E-2  END
F      1 0 3.0939E-2  END
PARAFFIN 2 1.0  END
PLEXIGLASS 3 0.918  END
AL      3 0.062  END
END COMP
RAFFETY AND MALHALCZO U(3)F4-1 REFLECTED (CASE 23)
READ PARM  RUN=YES  NPG=600  NUB=YES  FDN=YES  END PARM
READ GEOM
UNIT 1
CUBOID  1 1 2P23.010 2P23.010 2P33.785
REPLICATE 2 2 5*3.048 0.0 5
UNIT 2
CUBOID  3 1 2P23.010 2P23.010 2*0.0
REPLICATE 3 2 4*3.048 0.0 3.048 5
END GEOM
READ ARRAY
NUX=1  NUY=1  NUZ=2
FILL  2 1  END FILL
END ARRAY
READ BIAS ID=400  2 6  END BIAS
END DATA
END
=CSAS25
RAFFETY AND MILHALCZO U(3)F4-1 REFLECTED (CASE 23)
HANSEN-ROACH  INFHOMMEDIUM
U-235  1 0 2.3494E-4  END
U-238  1 0 7.4999E-3  END
H      1 0 3.1341E-2  END
C      1 0 1.5067E-2  END
F      1 0 3.0939E-2  END
PARAFFIN 2 1.0  END
PLEXIGLASS 3 0.918  END
AL      3 0.062  END
END COMP
RAFFETY AND MALHALCZO U(3)F4-1 REFLECTED (CASE 23)
READ PARM  RUN=YES  PLT=NO  NPG=600  NUB=YES  FDN=YES  END PARM
READ GEOM
UNIT 1
CUBOID  1 1 2P23.010 2P23.010 2P33.785
REPLICATE 2 2 5*3.048 0.0 5
UNIT 2
CUBOID  3 1 2P23.010 2P23.010 2*0.0
REPLICATE 3 2 4*3.048 0.0 3.048 5
END GEOM
READ ARRAY
NUX=1  NUY=1  NUZ=2
FILL  2 1  END FILL
END ARRAY
READ BIAS ID=400  2 6  END BIAS
READ PLOT TTL='XZ SLICE OF CASE 23 SHOWING BIASING REGIONS'
XUL=-1  YUL=20  ZUL=99
XLR=79  YLR=20  ZLR=-3
UAX=1  WDN=-1  NAX=130  NCH='0123456'
PIC=WTS
END PLOT
END DATA
END

```

```

CAS22
=CSAS25
RAFFETY AND MILHALCZO U(3)F4-1 REFLECTED (CASE 22)
27GROUPNDF#  INFHOMMEDIUM
U-235  1 0 2.3494E-4  END
U-238  1 0 7.4999E-3  END
H      1 0 3.1341E-2  END
C      1 0 1.5067E-2  END
F      1 0 3.0939E-2  END
PARAFFIN 2 1.0  END
PLEXIGLASS 3 0.918  END
AL      3 0.062  END
END COMP
RAFFETY AND MALHALCZO U(3)F4-1 REFLECTED (CASE 22)
READ PARM  RUN=YES  NPG=600  NUB=YES  FDN=YES  END PARM
READ GEOM
UNIT 1
CUBOID  1 1 2P21.735 2P21.735 2P43.1950
REPLICATE 2 2 5*3.048 0.0 5
UNIT 2
CUBOID  3 1 2P21.735 2P21.735 2*0.0
REPLICATE 3 2 4*3.048 0.0 3.048 5
END GEOM
READ ARRAY
NUX=1  NUY=1  NUZ=2
FILL  2 1  END FILL
END ARRAY
READ BIAS ID=400  2 6  END BIAS
END DATA
END
=CSAS25
RAFFETY AND MILHALCZO U(3)F4-1 REFLECTED (CASE 22)
HANSEN-ROACH  INFHOMMEDIUM
U-235  1 0 2.3494E-4  END
U-238  1 0 7.4999E-3  END
H      1 0 3.1341E-2  END
C      1 0 1.5067E-2  END
F      1 0 3.0939E-2  END
PARAFFIN 2 1.0  END
PLEXIGLASS 3 0.918  END
AL      3 0.062  END
END COMP
RAFFETY AND MALHALCZO U(3)F4-1 REFLECTED (CASE 22)
READ PARM  RUN=YES  PLT=NO  NPG=600  NUB=YES  FDN=YES  END PARM
READ GEOM
UNIT 1
CUBOID  1 1 2P21.735 2P21.735 2P43.1950
REPLICATE 2 2 5*3.048 0.0 5
UNIT 2
CUBOID  3 1 2P21.735 2P21.735 2*0.0
REPLICATE 3 2 4*3.048 0.0 3.048 5
END GEOM
READ ARRAY
NUX=1  NUY=1  NUZ=2
FILL  2 1  END FILL
END ARRAY
READ BIAS ID=400  2 6  END BIAS
READ PLOT TTL='XZ SLICE OF CASE 22 SHOWING BIASING REGIONS'
XUL=-1  YUL=20  ZUL=129
XLR=79  YLR=20  ZLR=-3
UAX=1  WDN=-1  NAX=130  NCH='0123456'
PIC=WTS
END PLOT
END DATA
END

```

Table A.3 (continued)

```

CAS24
=CSAS25
RAFFETY AND MALHALCZO U(3)F4-1 REFLECTED (CASE 24) NO BIASING
27GROUPNDF4  INFHOMMEDIUM
U-235  1 0 2.3494E-4  END
U-238  1 0 7.4999E-3  END
H      1 0 3.1341E-2  END
C      1 0 1.5067E-2  END
F      1 0 3.0939E-2  END
PARAFFIN 2 1.0  END
PLEXIGLASS 3 0.918  END
AL      3 0.062  END
END COMP
RAFFETY AND MALHALCZO U(3)F4-1 REFLECTED (CASE 24) NO BIASING
READ PARM  RUN=YES  NPG=600  NUB=YES  FDN=YES  END PARM
READ GEOM
UNIT 1
CUBOID  1 1 2P28.125 2P28.125 2P21.705
REPLICATE 2 2 5*3.048 0.0 5
UNIT 2
CUBOID  3 1 2P28.125 2P28.125 2*0.0
REPLICATE 3 2 4*3.048 0.0 3.048 5
END GEOM
READ ARRAY
NUX=1  NUY=1  NUZ=2
FILL  2 1  END FILL
END ARRAY
' READ BIAS ID=400  2 6  END BIAS
END DATA
END
=CSAS25
RAFFETY AND MALHALCZO U(3)F4-1 REFLECTED (CASE 24) NO BIASING
HANSEN-ROACH  INFHOMMEDIUM
U-235  1 0 2.3494E-4  END
U-238  1 0 7.4999E-3  END
H      1 0 3.1341E-2  END
C      1 0 1.5067E-2  END
F      1 0 3.0939E-2  END
PARAFFIN 2 1.0  END
PLEXIGLASS 3 0.918  END
AL      3 0.062  END
END COMP
RAFFETY AND MALHALCZO U(3)F4-1 REFLECTED (CASE 24) NO BIASING
READ PARM  RUN=YES  PLT=NO  NPG=600  NUB=YES  FDN=YES  END PARM
READ GEOM
UNIT 1
CUBOID  1 1 2P28.125 2P28.125 2P21.705
REPLICATE 2 2 5*3.048 0.0 5
UNIT 2
CUBOID  3 1 2P28.125 2P28.125 2*0.0
REPLICATE 3 2 4*3.048 0.0 3.048 5
END GEOM
READ ARRAY
NUX=1  NUY=1  NUZ=2
FILL  2 1  END FILL
END ARRAY
' READ BIAS ID=400  2 6  END BIAS
READ PLOT TTL='XE SLICE OF CASE 24 SHOWING BIASING REGIONS'
XUL=-1  YUL=20  ZUL=75
XLR=88  YLR=20  ZLR=-3
UAX=1  WDN=-1  NAX=130  NCH='0123456'
PIC=WTS
END PLOT
END DATA
END

```

```

CAS25
=CSAS25
RAFFETY AND MALHALCZO U(3)F4-1 REFLECTED (CASE 25)
27GROUPNDF4  INFHOMMEDIUM
U-235  1 0 2.3494E-4  END
U-238  1 0 7.4999E-3  END
H      1 0 3.1341E-2  END
C      1 0 1.5067E-2  END
F      1 0 3.0939E-2  END
PARAFFIN 2 1.0  END
PLEXIGLASS 3 0.918  END
AL      3 0.062  END
END COMP
RAFFETY AND MALHALCZO U(3)F4-1 REFLECTED (CASE 25)
READ PARM  RUN=YES  NPG=600  NUB=YES  FDN=YES  END PARM
READ GEOM
UNIT 1
CUBOID  1 1 2P30.680 2P30.680 2P19.335
REPLICATE 2 2 5*3.048 0.0 5
UNIT 2
CUBOID  3 1 2P30.680 2P30.680 2*0.0
REPLICATE 3 2 4*3.048 0.0 3.048 5
END GEOM
READ ARRAY
NUX=1  NUY=1  NUZ=2
FILL  2 1  END FILL
END ARRAY
READ BIAS ID=400  2 6  END BIAS
END DATA
END
=CSAS25
RAFFETY AND MALHALCZO U(3)F4-1 REFLECTED (CASE 25)
HANSEN-ROACH  INFHOMMEDIUM
U-235  1 0 2.3494E-4  END
U-238  1 0 7.4999E-3  END
H      1 0 3.1341E-2  END
C      1 0 1.5067E-2  END
F      1 0 3.0939E-2  END
PARAFFIN 2 1.0  END
PLEXIGLASS 3 0.918  END
AL      3 0.062  END
END COMP
RAFFETY AND MALHALCZO U(3)F4-1 REFLECTED (CASE 25)
READ PARM  RUN=YES  PLT=NO  NPG=600  NUB=YES  FDN=YES  END PARM
READ GEOM
UNIT 1
CUBOID  1 1 2P30.680 2P30.680 2P19.335
REPLICATE 2 2 5*3.048 0.0 5
UNIT 2
CUBOID  3 1 2P30.680 2P30.680 2*0.0
REPLICATE 3 2 4*3.048 0.0 3.048 5
END GEOM
READ ARRAY
NUX=1  NUY=1  NUZ=2
FILL  2 1  END FILL
END ARRAY
READ BIAS ID=400  2 6  END BIAS
READ PLOT TTL='XE SLICE OF CASE 25 SHOWING BIASING REGIONS'
XUL=-1  YUL=20  ZUL=71
XLR=93  YLR=20  ZLR=-3
UAX=1  WDN=-1  NAX=130  NCH='0123456'
PIC=WTS
END PLOT
END DATA
END

```

Table A.3 (continued)

```

CAS26
=CSAS25
RAFFETY AND MALHALCZO U(3)F4-1 UNREFLECTED (CASE 26)
27GROUPNDF4 INFHOMMEDIUM
U-235 1 0 2.3494E-4 END
U-238 1 0 7.4999E-3 END
H 1 0 3.1341E-2 END
C 1 0 1.5067E-2 END
F 1 0 3.0939E-2 END
END COMP
RAFFETY AND MALHALCZO U(3)F4-1 UNREFLECTED (CASE 26)
READ PARM NPG=600 NUB=YES FDN=YES END PARM
READ GEOM
CUBOID 1 1 28.235 -28.235 28.235 -28.235 43.32 -43.32
END GEOM
END DATA
END
=CSAS25
RAFFETY AND MALHALCZO U(3)F4-1 UNREFLECTED (CASE 26)
HANSEN-ROACH INFHOMMEDIUM
U-235 1 0 2.3494E-4 END
U-238 1 0 7.4999E-3 END
H 1 0 3.1341E-2 END
C 1 0 1.5067E-2 END
F 1 0 3.0939E-2 END
END COMP
RAFFETY AND MALHALCZO U(3)F4-1 UNREFLECTED (CASE 26)
READ PARM NPG=600 NUB=YES FDN=YES END PARM
READ GEOM
CUBOID 1 1 28.235 -28.235 28.235 -28.235 43.32 -43.32
END GEOM
END DATA
END

```

```

CAS27
=CSAS25
RAFFETY AND MALHALCZO U(3)F4-1 UNREFLECTED (CASE 27)
27GROUPNDF4 INFHOMMEDIUM
U-235 1 0 2.3494E-4 END
U-238 1 0 7.4999E-3 END
H 1 0 3.1341E-2 END
C 1 0 1.5067E-2 END
F 1 0 3.0939E-2 END
END COMP
RAFFETY AND MALHALCZO U(3)F4-1 UNREFLECTED (CASE 27)
READ PARM NPG=600 NUB=YES FDN=YES END PARM
READ GEOM
CUBOID 1 1 28.125 -28.125 30.68 -30.68 37.19 -37.19
END GEOM
END DATA
END
=CSAS25
RAFFETY AND MALHALCZO U(3)F4-1 UNREFLECTED (CASE 27)
HANSEN-ROACH INFHOMMEDIUM
U-235 1 0 2.3494E-4 END
U-238 1 0 7.4999E-3 END
H 1 0 3.1341E-2 END
C 1 0 1.5067E-2 END
F 1 0 3.0939E-2 END
END COMP

```

```

RAFFETY AND MALHALCZO U(3)F4-1 UNREFLECTED (CASE 27)
READ PARM NPG=600 NUB=YES FDN=YES END PARM
READ GEOM
CUBOID 1 1 28.125 -28.125 30.68 -30.68 37.19 -37.19
END GEOM
END DATA
END

```

```

CAS28
=CSAS25
RAFFETY AND MALHALCZO U(3)F4-1 UNREFLECTED (CASE 28)
27GROUPNDF4 INFHOMMEDIUM
U-235 1 0 2.3494E-4 END
U-238 1 0 7.4999E-3 END
H 1 0 3.1341E-2 END
C 1 0 1.5067E-2 END
F 1 0 3.0939E-2 END
END COMP
RAFFETY AND MALHALCZO U(3)F4-1 UNREFLECTED (CASE 28)
READ PARM NPG=600 NUB=YES FDN=YES END PARM
READ GEOM
CUBOID 1 1 30.7 -30.7 30.7 -30.7 33.00 -33.00
END GEOM
END DATA
END
=CSAS25
RAFFETY AND MALHALCZO U(3)F4-1 UNREFLECTED (CASE 28)
HANSEN-ROACH INFHOMMEDIUM
U-235 1 0 2.3494E-4 END
U-238 1 0 7.4999E-3 END
H 1 0 3.1341E-2 END
C 1 0 1.5067E-2 END
F 1 0 3.0939E-2 END
END COMP
RAFFETY AND MALHALCZO U(3)F4-1 UNREFLECTED (CASE 28)
READ PARM NPG=600 NUB=YES FDN=YES END PARM
READ GEOM
CUBOID 1 1 30.7 -30.7 30.7 -30.7 33.00 -33.00
END GEOM
END DATA
END

```

Table A.3 (continued)

```

CAS29
=CSAS25
RAFFETY AND MILHALCZO U(3)F4-2 REFLECTED (CAS29)
27GROUPNDF4 INFHOMMEDIUM
U-235 1 0 1.6709E-4 END
U-238 1 0 5.3355E-3 END
H 1 0 4.6262E-2 END
C 1 0 2.2241E-2 END
F 1 0 2.2011E-2 END
POLYETHYLENE 2 1.0 END
PLEXIGLASS 3 0.918 END
AL 3 0.062 END
END COMP
RAFFETY AND MALHALCZO U(3)F4-2 REFLECTED (CAS29)
READ PARM RUN=YES NPG=600 NUB=YES FDN=YES END PARM
READ GEOM
UNIT 1
CUBOID 1 1 2P20.405 2P20.400 2P19.745
REPLICATE 2 2 5*3.048 0.0 5
UNIT 2
CUBOID 3 1 2P20.405 2P20.400 2*0.0
REPLICATE 3 2 4*3.048 0.0 3.048 5
END GEOM
READ ARRAY
NUX=1 NUY=1 NUZ=2
FILL 2 1 END FILL
END ARRAY
READ BIAS ID=400 2 6 END BIAS
END DATA
=CSAS25
RAFFETY AND MILHALCZO U(3)F4-2 REFLECTED (CAS29)
HANSEN-ROACH INFHOMMEDIUM
U-235 1 0 1.6709E-4 END
U-238 1 0 5.3355E-3 END
H 1 0 4.6262E-2 END
C 1 0 2.2241E-2 END
F 1 0 2.2011E-2 END
POLYETHYLENE 2 1.0 END
PLEXIGLASS 3 0.918 END
AL 3 0.062 END
END COMP
RAFFETY AND MALHALCZO U(3)F4-2 REFLECTED (CAS29)
READ PARM RUN=YES PLT=NO NPG=600 NUB=YES FDN=YES END PARM
READ GEOM
UNIT 1
CUBOID 1 1 2P20.405 2P20.400 2P19.745
REPLICATE 2 2 5*3.048 0.0 5
UNIT 2
CUBOID 3 1 2P20.405 2P20.400 2*0.0
REPLICATE 3 2 4*3.048 0.0 3.048 5
END GEOM
READ ARRAY
NUX=1 NUY=1 NUZ=2
FILL 2 1 END FILL
END ARRAY
READ BIAS ID=400 2 6 END BIAS
READ PLOT TTL='XZ SLICE OF CAS29 SHOWING BIASING REGIONS'
XUL=-1 YUL=20 ZUL=71
XLR=73 YLR=20 ZLR=-3
UAX=1 WDN=-1 NAX=130 NCH='0123456'
PIC=WTS
END PLOT
END DATA
END

```

```

CAS30
=CSAS25
RAFFETY AND MILHALCZO U(3)F4-2 UNREFLECTED (CASE 30)
27GROUPNDF4 INFHOMMEDIUM
U-235 1 0 1.6709E-4 END
U-238 1 0 5.3355E-3 END
H 1 0 4.6262E-2 END
C 1 0 2.2241E-2 END
F 1 0 2.2011E-2 END
END COMP
RAFFETY AND MALHALCZO U(3)F4-2 UNREFLECTED (CASE 30)
READ PARM RUN=YES NPG=600 NUB=YES FDN=YES END PARM
READ GEOM
CUBOID 1 1 2P20.450 2P20.465 2P58.400
END GEOM
END DATA
=CSAS25
RAFFETY AND MILHALCZO U(3)F4-2 UNREFLECTED (CASE 30)
HANSEN-ROACH INFHOMMEDIUM
U-235 1 0 1.6709E-4 END
U-238 1 0 5.3355E-3 END
H 1 0 4.6262E-2 END
C 1 0 2.2241E-2 END
F 1 0 2.2011E-2 END
END COMP
RAFFETY AND MALHALCZO U(3)F4-2 UNREFLECTED (CASE 30)
READ PARM RUN=YES NPG=600 NUB=YES FDN=YES END PARM
READ GEOM
CUBOID 1 1 2P20.450 2P20.465 2P58.400
END GEOM
END DATA
END

```

```

CAS31
=CSAS25
RAFFETY AND MILHALCZO U(3)F4-2 UNREFLECTED (CASE 31)
27GROUPNDF4 INFHOMMEDIUM
U-235 1 0 1.6709E-4 END
U-238 1 0 5.3355E-3 END
H 1 0 4.6262E-2 END
C 1 0 2.2241E-2 END
F 1 0 2.2011E-2 END
END COMP
RAFFETY AND MALHALCZO U(3)F4-2 UNREFLECTED (CASE 31)
READ PARM RUN=YES NPG=600 NUB=YES FDN=YES END PARM
READ GEOM
CUBOID 1 1 2P24.295 2P25.570 2P24.265
END GEOM
END DATA
=CSAS25
RAFFETY AND MILHALCZO U(3)F4-2 UNREFLECTED (CASE 31)
HANSEN-ROACH INFHOMMEDIUM
U-235 1 0 1.6709E-4 END
U-238 1 0 5.3355E-3 END
H 1 0 4.6262E-2 END
C 1 0 2.2241E-2 END
F 1 0 2.2011E-2 END
END COMP

```

Table A.3 (continued)

RAFFETY AND MALHALCZO U(3)F4-2 UNREFLECTED (CASE 31)
 READ PARM RUN=YES NPG=600 NUB=YES FDN=YES END PARM
 READ GEOM
 CUBOID 1 1 2P24.295 2P25.570 2P24.265
 END GEOM
 END DATA
 END

CAS32
 =CSAS25
 RAFFETY AND MILHALCZO U(3)F4-2 UNREFLECTED (CASE 32)
 27GROUPNDF4 INFHOMMEDIUM
 U-235 1 0 1.6709E-4 END
 U-238 1 0 5.3355E-3 END
 H 1 0 4.6262E-2 END
 C 1 0 2.2241E-2 END
 F 1 0 2.2011E-2 END
 END COMP
 RAFFETY AND MALHALCZO U(3)F4-2 UNREFLECTED (CASE 32)
 READ PARM RUN=YES NPG=600 NUB=YES FDN=YES END PARM
 READ GEOM
 CUBOID 1 1 2P40.855 2P40.830 2P15.670
 END GEOM
 END DATA
 END

=CSAS25
 RAFFETY AND MILHALCZO U(3)F4-2 UNREFLECTED (CASE 32)
 HANSEN-ROACH INFHOMMEDIUM
 U-235 1 0 1.6709E-4 END
 U-238 1 0 5.3355E-3 END
 H 1 0 4.6262E-2 END
 C 1 0 2.2241E-2 END
 F 1 0 2.2011E-2 END
 END COMP
 RAFFETY AND MALHALCZO U(3)F4-2 UNREFLECTED (CASE 32)
 READ PARM RUN=YES NPG=600 NUB=YES FDN=YES END PARM
 READ GEOM
 CUBOID 1 1 2P40.855 2P40.830 2P15.670
 END GEOM
 END DATA
 END

CAS33
 =CSAS25
 CRITICAL REFLECTED CYLINDER OF AQUEOUS U(4.98)O2F2 (CASE 33)
 27GROUPNDF4 INFHOMMEDIUM
 SOLNUO2F2 1 910.36 0.0 1 298 92235 4.98 92238 95.02 END
 SS304 2 1.0 END
 H2O 3 1.0 END
 CD 4 1.0 END
 END COMP
 CRITICAL REFLECTED CYLINDER OF AQUEOUS U(4.98)O2F2 (CASE 33)
 READ PARM RUN=YES NPG=600 NUB=YES FDN=YES END PARM
 READ GEOM
 UNIT 1
 CYLINDER 1 1 19.545 2P27.225
 CYLINDER 0 1 19.545 78.975 -27.225
 CYLINDER 2 1 19.624 79.054 -27.304
 CYLINDER 4 1 19.705 79.054 -27.304
 CYLINDER 2 1 22.245 79.054 -27.304
 CYLINDER 3 1 45.000 79.054 -27.304
 CUBOID 0 1 4P45.000 79.054 -27.304
 END GEOM
 END DATA
 END
 =CSAS25
 CRITICAL REFLECTED CYLINDER OF AQUEOUS U(4.98)O2F2 (CASE 33)
 HANSEN-ROACH INFHOMMEDIUM
 SOLNUO2F2 1 910.36 0.0 1 298 92235 4.98 92238 95.02 END
 SS304 2 1.0 END
 H2O 3 1.0 END
 CD 4 1.0 END
 END COMP
 CRITICAL REFLECTED CYLINDER OF AQUEOUS U(4.98)O2F2 (CASE 33)
 READ PARM RUN=YES NPG=600 NUB=YES FDN=YES END PARM
 READ GEOM
 UNIT 1
 CYLINDER 1 1 19.545 2P27.225
 CYLINDER 0 1 19.545 78.975 -27.225
 CYLINDER 2 1 19.624 79.054 -27.304
 CYLINDER 4 1 19.705 79.054 -27.304
 CYLINDER 2 1 22.245 79.054 -27.304
 CYLINDER 3 1 45.000 79.054 -27.304
 CUBOID 0 1 4P45.000 79.054 -27.304
 END GEOM
 READ PLOT TTL='XZ SLICE OF CYLINDER CASE 33'
 XUL=-45 YUL=0.0 ZUL=81
 XLR=45 YLR=0.0 ZLR=-29
 UAX=1 WDN=-1 NAX=130 NCH='01234' END
 TTL='ENLARGEMENT OF LOWER RIGHT HAND CORNER OF CYLINDER'
 XUL=18 YUL=0.0 ZUL=-25
 XLR=23 YLR=0.0 ZLR=-28
 UAX=1 WDN=-1 NAX=130 NCH='01234'
 END PLOT
 END DATA
 END

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Table A.3 (continued)

```

CAS34
=CSAS25
CRITICAL REFLECTED CYLINDER OF AQUEOUS U(4.98)O2F2 (CASE 34)
27GROUPNDF4 INFHOMMEDIUM
' SOLNUO2F2 1 910.36 0.0 1 298 92235 4.98 92238 95.02 END
U-235 1 0 1.1599E-4 END
U-238 1 0 2.1852E-3 END
F 1 0 4.6024E-3 END
H 1 0 5.6605E-2 END
O 1 0 3.2904E-2 END
SS304 2 1.0 END
H2O 3 1.0 END
END COMP
CRITICAL REFLECTED CYLINDER OF AQUEOUS U(4.98)O2F2 (CASE 34)
READ PARM RUN=YES NPG=600 NUB=YES PDN=YES END PARM
READ GEOM
UNIT 1
CYLINDER 1 1 16.510 2P71.500
CYLINDER 0 1 16.510 172.400 -71.500
CYLINDER 2 1 16.589 172.479 -71.579
CYLINDER 2 1 19.129 172.479 -71.579
CYLINDER 3 1 45.000 172.479 -71.579
CUBOID 0 1 4P45.000 172.479 -71.579
END GEOM
END DATA
END
=CSAS25
CRITICAL REFLECTED CYLINDER OF AQUEOUS U(4.98)O2F2 (CASE 34)
HANSEN-ROACH INFHOMMEDIUM
' SOLNUO2F2 1 910.36 0.0 1 298 92235 4.98 92238 95.02 END
U-235 1 0 1.1599E-4 END
U-238 1 0 2.1852E-3 END
F 1 0 4.6024E-3 END
H 1 0 5.6605E-2 END
O 1 0 3.2904E-2 END
SS304 2 1.0 END
H2O 3 1.0 END
END COMP
CRITICAL REFLECTED CYLINDER OF AQUEOUS U(4.98)O2F2 (CASE 34)
READ PARM RUN=YES NPG=600 NUB=YES PDN=YES END PARM
READ GEOM
UNIT 1
CYLINDER 1 1 16.510 2P71.500
CYLINDER 0 1 16.510 172.400 -71.500
CYLINDER 2 1 16.589 172.479 -71.579
CYLINDER 2 1 19.129 172.479 -71.579
CYLINDER 3 1 45.000 172.479 -71.579
CUBOID 0 1 4P45.000 172.479 -71.579
END GEOM
READ PLOT TTL='XZ SLICE OF CYLINDER CASE 34'
XUL=-45 YUL=0.0 ZUL=174
XLR=45 YLR=0.0 ZLR=-73
UAX=1 WDN=-1 NAX=130 NCH='0123'END
TTL='ENLARGEMENT OF LOWER RIGHT CORNER OF CYLINDER'
XUL=15 YUL=0.0 ZUL=-69
XLR=20 YLR=0.0 ZLR=-73
UAX=1 WDN=-1 NAX=130 NCH='0123'
END PLOT
END DATA
END

```

```

CAS35
=CSAS25
CRITICAL SPHERE OF AQUEOUS U(4.98)O2F2 (CASE 35)
27GROUPNDF4 INFHOMMEDIUM
' SOLNUO2F2 1 910.18 0.0 1 292 92235 4.98 92238 95.02 END
U-235 1 0 1.1613E-4 END
U-238 1 0 2.1878E-3 END
H 1 0 5.6947E-2 END
O 1 0 3.3081E-2 END
F 1 0 4.6080E-3 END
SS304 2 1.0 END
END COMP
CRITICAL SPHERE OF AQUEOUS U(4.98)O2F2 (CASE 35)
READ PARM RUN=YES NPG=600 NUB=YES PDN=YES END PARM
READ GEOM
UNIT 1
SPHERE 1 1 25.3873
SPHERE 2 1 25.4127
CUBOID 0 1 6P25.4127
END GEOM
END DATA
END
=CSAS25
CRITICAL SPHERE OF AQUEOUS U(4.98)O2F2 (CASE 35)
HANSEN-ROACH INFHOMMEDIUM
' SOLNUO2F2 1 910.18 0.0 1 292 92235 4.98 92238 95.02 END
U-235 1 0 1.1613E-4 END
U-238 1 0 2.1878E-3 END
H 1 0 5.6947E-2 END
O 1 0 3.3081E-2 END
F 1 0 4.6080E-3 END
SS304 2 1.0 END
END COMP
CRITICAL SPHERE OF AQUEOUS U(4.98)O2F2 (CASE 35)
READ PARM RUN=YES NPG=600 NUB=YES PDN=YES END PARM
READ GEOM
UNIT 1
SPHERE 1 1 25.3873
SPHERE 2 1 25.4127
CUBOID 0 1 6P25.4127
END GEOM
READ PLOT TTL='XZ SLICE OF SPHERE CASE 35'
XUL=-26 YUL=0.0 ZUL=26
XLR=26 YLR=0.0 ZLR=-26
UAX=1 WDN=-1 NAX=130 NCH='012'
TTL='ENLARGEMENT OF SPHERE WALL'
XUL=24 YUL=0.0 ZUL=2
XLR=26 YLR=0.0 ZLR=-2
UAX=1 WDN=-1 NAX=130 NCH='012'
END PLOT
END DATA
END

```

Table A.3 (continued)

```

CAS36
=CSAS25
CRITICAL CYLINDER OF AQUEOUS U(4.98)O2F2 (CASE 36)
27GROUPNDF4 INPHOMMEDIUM
SOLNUO2F2 1 910.36 0.0 1 298 92235 4.98 92238 95.02 END
SS304 2 1.0 END
END COMP
CRITICAL CYLINDER OF AQUEOUS U(4.98)O2F2 (CASE 36)
READ PARM RUN=YES NPG=600 NUB=YES FDN=YES END PARM
READ GEOM
UNIT 1
CYLINDER 1 1 19.5500 2P50.85
CYLINDER 0 1 19.5500 74.16 -50.85
CYLINDER 2 1 19.6287 74.16 -50.9287
CUBOID 0 1 4P19.6287 74.16 -50.9287
END GEOM
END DATA
END
=CSAS25
CRITICAL CYLINDER OF AQUEOUS U(4.98)O2F2 (CASE 36)
HANSEN-ROACH INPHOMMEDIUM
SOLNUO2F2 1 910.36 0.0 1 298 92235 4.98 92238 95.02 END
SS304 2 1.0 END
END COMP
CRITICAL CYLINDER OF AQUEOUS U(4.98)O2F2 (CASE 36)
READ PARM RUN=YES NPG=600 NUB=YES FDN=YES END PARM
READ GEOM
UNIT 1
CYLINDER 1 1 19.5500 2P50.85
CYLINDER 0 1 19.5500 74.16 -50.85
CYLINDER 2 1 19.6287 74.16 -50.9287
CUBOID 0 1 4P19.6287 74.16 -50.9287
END GEOM
READ PLOT TTL='XZ SLICE OF CYLINDER CASE 36'
XUL=-21 YUL=0.0 ZUL=76
XLR=21 YLR=0.0 ZLR=-52
UAX=1 WDN=-1 NAX=130 NCH='012'END
TTL='ENLARGEMENT OF LOWER RIGHT CORNER OF CYLINDER'
XUL=18 YUL=0.0 ZUL=-49
XLR=21 YLR=0.0 ZLR=-52
UAX=1 WDN=-1 NAX=130 NCH='012'
END PLOT
END DATA
END

```

```

CAR01
=CSAS25
ROCKY FLATS CRITICALS NUREG/CR-1071 EXPERIMENT NUMBER 1 (27 GROUP)
' 48 FUEL CANS 2.44 CM MODERATOR GEE.HU77.DATA(OPT1)
27GROUPNDF4 LATTICECELL
U308 1 5.4078E-1 293.0 92234 0.03 92235 4.46 92236 0.08 92238 95.43 END
H2O 1 8.9514E-2 END
ARBM-BAGGIE 1.0 3 0 0 0 1001 14.01 6012 84.9 8016 1.20 1 1.9134E-2
END
ARBM-AL1100 1.0 3 0 0 1 13027 99.18 26000 0.5 29000 0.2 2 9.5390E-1
END
ARBM-TAPE(VINYL) 1.0 7 0 0 0 1001 5.92 6012 45.91 8016 10.82 17000
25.73 20040 6.9 22000 1.6 82000 1.1 2 1.1115E-2 END
ARBM-TAPE(MYLAR) 1.0 3 0 0 0 1001 6.83 6012 65.50 8016 27.02 2
1.7491E-2 END
ARBM-MODERATOR 1.185 3 0 0 0 1001 7.83 6012 59.49 8016 32.48 3 END
ARBM-PLEX(REG) 1.0 3 0 0 0 1001 7.84 6012 59.59 8016 32.23 4
1.1773 END
ARBM-PLEX(PAPER) 1.0 3 0 0 0 1001 6.48 6012 42.17 8016 49.5 4
3.7534E-3 END
ARBM-PLEX(GLUE) 1.0 3 0 0 0 1001 11.67 6012 86.29 8016 1.20 4
1.1648E-3 END
ARBM-PLEX(TRIS) 1.0 8 0 0 1 1001 7.16 6012 52.03 7014 0.16 8016 29.82
15031 1.02 17000 1.81 35079 4.260 35081 2.840 5 1.2757 END
ARBM-PLEX(PAPER) 1.0 3 0 0 0 1001 6.48 6012 42.17 8016 49.5 5
3.7534E-3 END
ARBM-PLEX(GLUE) 1.0 3 0 0 0 1001 11.67 6012 86.29 8016 1.20 5
1.1648E-3 END
ARBM-FILLER 1.185 3 0 0 0 1001 7.83 6012 59.49 8016 32.48 6 .88 END
' THIS MATERIAL IS ACTUALLY MODERATOR ADJUSTED FOR THE VOLUME
' FRACTION OF THE VOID FILLED BETWEEN CORE AND REFLECTOR.
END COMP
SPHTRIANGP 19.9462 18.5857 1 3 18.9579 2 END
ROCKY FLATS CRITICALS NUREG/CR-1071 EXPERIMENT NUMBER 1 (27 GROUP)
' 48 FUEL CANS 2.44 CM MODERATOR GEE.HU77.DATA(OPT1)
READ PARM RUN=YES NPG=600
NUB=YES FDN=YES PLT=NO
END PARM
READ GEOM
UNIT 1
COM='FUEL BOX 15.28 CM ON A SIDE WITH .15 CM WALLS .05CM STACKING VOID'
CUBOID 1 1 6P7.49
CUBOID 2 1 6P7.64
CUBOID 0 1 6P7.6650
UNIT 2
COM='X-FACE INTERSTITIAL MODERATOR'
CUBOID 3 1 2P1.2200 4P7.665
UNIT 3
COM='Y-FACE INTERSTITIAL MODERATOR'
CUBOID 3 1 2P7.665 2P1.2200 2P7.665
UNIT 4
COM='Z-FACE INTERSTITIAL MODERATOR'
CUBOID 3 1 4P7.665 2P1.2200
UNIT 5
COM='MORE X-FACE MODERATOR'
CUBOID 3 1 4P1.2200 2P7.665
UNIT 6
COM='MORE Y-FACE MODERATOR'
CUBOID 3 1 2P7.665 4P1.2200
UNIT 7
COM='MORE Z-FACE MODERATOR'
CUBOID 3 1 2P1.2200 2P7.665 2P1.2200

```

Table A.3 (continued)

```

UNIT 8
COM='LAST OF INTERSTITIAL MODERATOR'
CUBOID 3 1 6P1.2200
UNIT 9
COM='NORTH SPLIT TABLE CORE'
ARRAY 1 3*0.0
UNIT 10
COM='SOUTH SPLIT TABLE CORE'
ARRAY 2 3*0.0
UNIT 11
COM='PLEXIGLASS REFLECTOR SHEET WITHOUT TRIS, NORTH BOTTOM REFLECTOR'
CUBOID 4 1 2P16.5500 2P38.7500 2P0.6150
UNIT 12
COM='PLEXIGLASS REFLECTOR SHEET WITH TRIS, NORTH BOTTOM REFLECTOR'
CUBOID 5 1 2P16.5500 2P38.7500 2P0.6150
UNIT 13
COM='UPPER PORTION NORTH BOTTOM REFLECTOR WITH TRIS'
CUBOID 5 1 2P16.550 2P38.75 2P8.24
UNIT 14
COM='LOWER PORTION NORTH BOTTOM REFLECTOR WITH TRIS'
CUBOID 5 1 2P16.550 2P38.75 2P3.69
UNIT 15
COM='NORTH BOTTOM REFLECTOR INCLUDES REGULAR AND TRIS'
ARRAY 3 3*0.0
UNIT 16
COM='PLEXIGLAS SHEET BOTTOM SOUTH REFLECTOR WITHOUT TRIS'
CUBOID 0 1 2P5.1 2P2.55 2P0.615
CUBOID 4 1 44.3 -5.1 2P38.75 2P0.615
UNIT 17
COM='PLEXIGLAS SHEET BOTTOM SOUTH REFLECTOR WITH TRIS'
CUBOID 0 1 2P5.1 2P2.55 2P0.615
CUBOID 5 1 44.3 -5.1 2P38.75 2P0.6150
UNIT 18
COM='LOWER PORTION SOUTH BOTTOM REFLECTOR WITH TRIS'
CUBOID 0 1 2P5.1 2P2.55 2P8.855
CUBOID 5 1 44.3 -5.1 2P38.75 2P8.855
UNIT 19
COM='SOUTH BOTTOM REFLECTOR WITH REGULAR AND TRIS'
ARRAY 4 3*0.0
UNIT 20
COM='EAST AND WEST REFLECTORS FOR NORTH REFLECTOR WITH TRIS'
CUBOID 5 1 2P16.550 2P12.65 2P54.2825
UNIT 21
COM='ARRAY FOR EAST AND WEST REFLECTORS FOR NORTH REFLECTOR'
ARRAY 5 3*0.0
UNIT 22
COM='EAST AND WEST REFLECTORS FOR SOUTH REFLECTOR WITH TRIS'
CUBOID 5 1 2P24.700 2P12.65 2P54.2825
UNIT 23
COM='ARRAY FOR EAST AND WEST REFLECTORS FOR SOUTH REFLECTOR'
ARRAY 6 3*0.0
UNIT 24
COM='NORTH TOP REFLECTOR WITH TRIS'
CUBOID 5 1 2P29.100 2P64.05 2P12.15
UNIT 25
COM='ARRAY FOR NORTH TOP REFLECTOR'
ARRAY 7 3*0.0
UNIT 26
COM='SOUTH TOP REFLECTOR WITH TRIS'
CUBOID 0 1 2P5.1 2P2.55 2P12.15
CUBOID 5 1 69.4 -5.1 2P64.05 2P12.15

UNIT 27
COM='ARRAY FOR SOUTH TOP REFLECTOR'
ARRAY 8 3*0.0
UNIT 28
COM='NORTH END REFLECTOR 9.8CM PORTION WITHOUT TRIS'
CUBOID 4 1 2P4.9000 2P64.0500 2P54.2825
UNIT 29
COM='NORTH END REFLECTOR 5.2 CM PORTION WITH TRIS'
CUBOID 5 1 2P2.6 2P64.0500 2P54.2825
UNIT 30
COM='NORTH END REFLECTOR 10.1 CM PORTION WITHOUT TRIS'
CUBOID 4 1 2P5.05 2P64.05 2P54.2825
UNIT 31
COM='ARRAY FOR NORTH END REFLECTOR'
ARRAY 9 3*0.0
UNIT 32
COM='SOUTH END REFLECTOR'
CUBOID 5 1 2P12.55 2P64.05 2P54.2825
UNIT 33
COM='ARRAY FOR SOUTH END REFLECTOR'
ARRAY 10 3*0.0
UNIT 34
COM='BOTTOM MODERATING PLASTIC NORTH CORE'
CUBOID 6 1 2P16.550 2P38.7500 2P13.0500
UNIT 35
COM='TOP MODERATING PLASTIC NORTH CORE'
CUBOID 6 1 2P16.550 2P38.7500 2P3.2525
UNIT 36
ARRAY 11 3*0.0
UNIT 37
ARRAY 12 3*0.0
UNIT 38
COM='NORTH CORE WITH BOTTOM REFLECTOR'
ARRAY 13 3* 0.0
UNIT 39
COM='NORTH CORE WITH EAST AND WEST REFLECTOR'
ARRAY 14 3*0.0
UNIT 40
COM='NORTH CORE WITH END REFLECTOR'
ARRAY 15 3*0.0
UNIT 41
COM='NORTH SPLIT TABLE FACEPLATE'
CUBOID 3 1 2P0.6150 2P64.0500 2P66.4325
UNIT 42
COM='NORTH CORE WITH TOP REFLECTOR'
ARRAY 16 3*0.0
UNIT 43
COM='NORTH CORE WITH FACEPLATE'
ARRAY 17 3*0.0
UNIT 44
COM='12.95 CM THICK MODERATOR SOUTH CORE'
CUBOID 6 1 2P23.924 2P6.475 2P40.183
UNIT 45
COM='2.95 THICK MODERATOR SOUTH CORE'
CUBOID 6 1 2P23.924 2P38.5285 2P1.475
UNIT 46
COM='COMBINATION OF CORE WITH 12.95 THICK MODERATOR'
ARRAY 18 3*0.0
UNIT 47
COM='COMBINATION OF CORE WITH 2.95 THICK MODERATOR'
ARRAY 19 3*0.0
UNIT 48
COM='SOUTH CORE WITH EAST WEST REFLECTORS'
ARRAY 20 3*0.0

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Table A.3 (continued)

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UNIT 49
COM='SOUTH CORE WITH EAST WEST REFLECTORS'
ARRAY 21 3*0.0
UNIT 50
COM='SOUTH CORE END REFLECTOR'
ARRAY 22 3*0.0
UNIT 51
COM='FACEPLATE FOR SOUTH SPLIT TABLE'
CUBOID 3 1 2P0.4620 2P64.0500 2P66.4325
UNIT 52
COM='SOUTH CORE WITH TOP REFLECTOR'
ARRAY 23 3*0.0
UNIT 53
COM='SOUTH CORE WITH FACEPLATE'
ARRAY 24 3*0.0
UNIT 54
COM='AIR GAP'
CUBOID 0 1 2P0.1550 2P64.0500 2P66.4325
GLOBAL
UNIT 55
COM='TOTAL'
ARRAY 25 3*0.0
UNIT 56
COM='EMPTY FUEL LOCATION'
CUBOID 0 1 6P7.6650
UNIT 57
COM='SIDE MODERATOR'
CUBOID 6 1 2P16.550 2P4.4300 2P25.4350
UNIT 58
COM='END MODERATOR'
CUBOID 6 1 2P8.1500 2P38.7500 2P25.4350
UNIT 59
COM='SOUTH CORE BOTTOM MODERATING PLASTIC'
CUBOID 6 1 2P24.7000 2P38.7500 2P13.0500
UNIT 60
COM='SOUTH CORE TOP MODERATING PLASTIC'
CUBOID 6 1 2P24.7000 2P38.7500 2P3.2525
UNIT 61
COM='Y-FACE MODERATOR VOID'
CUBOID 0 1 2P7.665 2P1.2200 2P7.665
END GEOMETRY
READ ARRAY
ARA=1 NUX=3 NUY=7 NUZ=5
COM='NORTH SPLIT TABLE CORE'
FILL 1 2 1 3 5 3 2Q6 1 2 1
      4 7 4 6 8 6 2Q6 4 7 4
      1Q42
      56 2 1 3 5 3 1 2 1 3 5 3 1Q6 56 2 1 END FILL
ARA=2 NUX=3 NUY=7 NUZ=5
COM='SOUTH SPLIT TABLE CORE'
FILL 1 2 1 3 5 3 2Q6 1 2 1
      4 7 4 6 8 6 2Q6 4 7 4
      1Q42
      1 2 56 3 5 61 2Q6 1 2 56 END FILL
ARA=3 NUX=1 NUY=1 NUZ=3
COM='NORTH BOTTOM REFLECTOR'
FILL 14 11 13 END FILL
ARA=4 NUX=1 NUY=1 NUZ=7
COM='SOUTH BOTTOM REFLECTOR'
FILL 18 16 17 16 16 17 17 END FILL
ARA=5 NUX=1 NUY=1 NUZ=1
COM='EAST AND WEST WALLS OF NORTH REFLECTOR'
FILL 20 END FILL
ARA=6 NUX=1 NUY=1 NUZ=1

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COM='EAST AND WEST WALLS OF SOUTH REFLECTOR'
FILL 22 END FILL
ARA=7 NUX=1 NUY=1 NUZ=1
COM='ARRAY FOR NORTH TOP REFLECTOR'
FILL 24 END FILL
ARA=8 NUX=1 NUY=1 NUZ=1
COM='ARRAY FOR SOUTH TOP REFLECTOR'
FILL 26 END FILL
ARA=9 NUX=3 NUY=1 NUZ=1
COM='ARRAY FOR NORTH END REFLECTOR'
FILL 28 29 30 END FILL
ARA=10 NUX=1 NUY=1 NUZ=1
COM='ARRAY FOR SOUTH END REFLECTOR'
FILL 32 END FILL
ARA=11 NUX=1 NUY=2 NUZ=1
COM='COMBINARION OF CORE WITH SIDE MODERATOR'
FILL 9 57 END FILL
ARA=12 NUX=1 NUY=1 NUZ=3
COM='COMBINATION OF PREVIOUS ARRAY WITH TOP AND BOTTOM MODERATOR'
FILL 34 36 35 END FILL
ARA=13 NUX=1 NUY=1 NUZ=2
COM='COMBINATION OF NORTH CORE WITH BOTTOM REFLECTOR'
FILL 15 37 END FILL
ARA=14 NUX=1 NUY=3 NUZ=1
COM='NORTH CORE WITH SIDE REFLECTORS'
FILL 21 38 21 END FILL
ARA=15 NUX=2 NUY=1 NUZ=1
COM='NORTH CORE WITH END REFLECTOR'
FILL 31 39 END FILL
ARA=16 NUX=1 NUY=1 NUZ=2
COM='NORTH CORE WITH TOP REFLECTOR'
FILL 40 25 END FILL
ARA=17 NUX=2 NUY=1 NUZ=1
COM='NORTH CORE WITH FACEPLATE'
FILL 42 41 END FILL
ARA=18 NUX=1 NUY=2 NUZ=1
COM='COMBINATION OF S. CORE WITH SIDE MODERATOR'
FILL 10 57 END FILL
ARA=19 NUX=2 NUY=1 NUZ=1
COM='COMBINATION OF CORE WITH END MODERATOR'
FILL 46 58 END FILL
ARA=20 NUX=1 NUY=1 NUZ=4
COM='SOUTH CORE WITH BOTTOM MODERATOR AND REFLECTOR'
FILL 19 59 47 60 END FILL
ARA=21 NUX=1 NUY=3 NUZ=1
COM='SOUTH CORE WITH EAST WEST REFLECTORS'
FILL 23 48 23 END FILL
ARA=22 NUX=2 NUY=1 NUZ=1
COM='SOUTH CORE WITH END REFLECTOR'
FILL 49 33 END FILL
ARA=23 NUX=1 NUY=1 NUZ=2
COM='COMBINATION OF CORE WITH TOP REFLECTOR'
FILL 50 27 END FILL
ARA=24 NUX=2 NUY=1 NUZ=1
COM='SOUTH CORE WITH FACEPLATE'
FILL 51 52 END FILL
ARA=25 NUX=3 NUY=1 NUZ=1
COM='TOTAL'
FILL 43 54 53 END FILL
END ARRAY
READ PLOT TTL='XZ SLICE OF RFP1 SHOWING MATERIAL REGIONS'
XUL=-2 YUL=64.05 ZUL=136
XLR=137 YLR=64.05 ZLR=-2
UAX=1 WDN=-1 NAX=130 NCH='0123456'END

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Table A.3 (continued)

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TTL='YZ SLICE OF NORTH CORE SECOND ROW'
XUL=28 YUL=-2 ZUL=136
XLR=28 YLR=136 ZLR=-2
VAX=1 WDN=-1 NAX=130 NCH='0123456'END
TTL='YZ SLICE OF SOUTH CORE SECOND ROW'
XUL=80 YUL=-2 ZUL=136
XLR=80 YLR=136 ZLR=-2
VAX=1 WDN=-1 NAX=130 NCH='0123456'
END PLOT
END DATA
END

CAR02
=CSAS25
ROCKY FLATS CRITICALS NUREG/CR-1071 EXPERIMENT NUMBER 2 (27 GROUP)
' 43 FUEL CANS 2.44 CM MODERATOR GER.HU77.DATA(OPT2)
27GROUPNDF4 LATTICECELL
U308 1 5.4078E-1 293.0 92234 0.03 92235 4.46 92236 0.08 92238 95.43 END
H2O 1 8.9514E-2 END
ARBM-BAGGIE 1.0 3 0 0 0 1001 14.01 6012 84.9 8016 1.20 1 1.9134E-2
END
ARBM-AL1100 1.0 3 0 0 1 13027 99.18 26000 0.5 29000 0.2 2 9.5390E-1
END
ARBM-TAPE(VINYL) 1.0 7 0 0 0 1001 5.92 6012 45.91 8016 10.82 17000
25.73 20040 6.9 22000 1.6 82000 1.1 2 1.1115E-2 END
ARBM-TAPE(MYLAR) 1.0 3 0 0 0 1001 6.83 6012 65.50 8016 27.02 2
1.7491E-2 END
ARBM-MODERATOR 1.185 3 0 0 0 1001 7.83 6012 59.49 8016 32.48 3 END
ARBM-FLEX(REG) 1.0 3 0 0 0 1001 7.84 6012 59.59 8016 32.23 4
1.1773 END
ARBM-FLEX(PAPER) 1.0 3 0 0 0 1001 6.48 6012 42.17 8016 49.5 4
3.7534E-3 END
ARBM-FLEX(GLUE) 1.0 3 0 0 0 1001 11.67 6012 86.29 8016 1.20 4
1.1648E-3 END
ARBM-FLEX(TRIS) 1.0 8 0 0 1 1001 7.16 6012 52.03 7014 0.16 8016 29.82
15031 1.02 17000 1.81 35079 4.260 35081 2.840 5 1.2757 END
ARBM-FLEX(PAPER) 1.0 3 0 0 0 1001 6.48 6012 42.17 8016 49.5 5
3.7534E-3 END
ARBM-FLEX(GLUE) 1.0 3 0 0 0 1001 11.67 6012 86.29 8016 1.20 5
1.1648E-3 END
ARBM-MODERATOR 1.185 3 0 0 0 1001 7.83 6012 59.49 8016 32.48 6 .89 END
' THIS MATERIAL IS ACTUALLY MODERATOR ADJUSTED FOR THE VOLUME
' FRACTION OF THE VOID FILLED BETWEEN CORE AND REFLECTOR.
END COMP
SPHTRIANGP 19.9462 18.5857 1 3 18.9579 2 END
ROCKY FLATS CRITICALS NUREG/CR-1071 EXPERIMENT NUMBER 2 (27 GROUP)
' 43 FUEL CANS 2.44 CM MODERATOR GER.HU77.DATA(OPT2)
READ PARM RUN=YES NPG=600
NUB=YES FDN=YES PLT=NO
END PARM
READ GEOM
UNIT 1
COM='FUEL BOX 15.28 CM ON A SIDE WITH .15 CM WALLS .05CM STACKING VOID'
CUBOID 1 1 6P7.49
CUBOID 2 1 6P7.64
CUBOID 0 1 6P7.6650
UNIT 2
COM='X-FACE INTERSTITIAL MODERATOR'
CUBOID 3 1 2P1.2200 4P7.665
UNIT 3
COM='Y-FACE INTERSTITIAL MODERATOR'
CUBOID 3 1 2P7.665 2P1.2200 2P7.665
UNIT 4
COM='Z-FACE INTERSTITIAL MODERATOR'
CUBOID 3 1 4P7.665 2P1.2200
UNIT 5
COM='MORE X-FACE MODERATOR'
CUBOID 3 1 4P1.2200 2P7.665
UNIT 6
COM='MORE Y-FACE MODERATOR'
CUBOID 3 1 2P7.665 4P1.2200
UNIT 7
COM='MORE Z-FACE MODERATOR'
CUBOID 3 1 2P1.2200 2P7.665 2P1.2200
UNIT 8
COM='LAST OF INTERSTITIAL MODERATOR'
CUBOID 3 1 6P1.2200
UNIT 9
COM='NORTH SPLIT TABLE CORE'
ARRAY 1 3*0.0
UNIT 10
COM='SOUTH SPLIT TABLE CORE'
ARRAY 2 3*0.0
UNIT 11
COM='PLEXIGLASS REFLECTOR SHEET WITHOUT TRIS, NORTH BOTTOM REFLECTOR'
CUBOID 4 1 2P16.5500 2P38.7500 2P0.6150
UNIT 12
COM='PLEXIGLASS REFLECTOR SHEET WITH TRIS, NORTH BOTTOM REFLECTOR'
CUBOID 5 1 2P16.5500 2P38.7500 2P0.6150
UNIT 13
COM='UPPER PORTION NORTH BOTTOM REFLECTOR WITH TRIS'
CUBOID 5 1 2P16.550 2P38.75 2P8.24
UNIT 14
COM='LOWER PORTION NORTH BOTTOM REFLECTOR WITH TRIS'
CUBOID 5 1 2P16.550 2P38.75 2P3.69
UNIT 15
COM='NORTH BOTTOM REFLECTOR INCLUDES REGULAR AND TRIS'
ARRAY 3 3*0.0
UNIT 16
COM='PLEXIGLAS SHEET BOTTOM SOUTH REFLECTOR WITHOUT TRIS'
CUBOID 0 1 2P5.1 2P2.55 2P0.6150
CUBOID 4 1 44.3 -5.1 2P38.75 2P0.615
UNIT 17
COM='PLEXIGLAS SHEET BOTTOM SOUTH REFLECTOR WITH TRIS'
CUBOID 0 1 2P5.1 2P2.55 2P0.6150
CUBOID 5 1 44.3 -5.1 2P38.75 2P0.6150
UNIT 18
COM='LOWER PORTION SOUTH BOTTOM REFLECTOR WITH TRIS'
CUBOID 0 1 2P5.1 2P2.55 2P8.855
CUBOID 5 1 44.3 -5.1 2P38.75 2P8.855
UNIT 19
COM='SOUTH BOTTOM REFLECTOR WITH REGULAR AND TRIS'
ARRAY 4 3*0.0
UNIT 20
COM='EAST AND WEST REFLECTORS FOR NORTH REFLECTOR WITH TRIS'
CUBOID 5 1 2P16.550 2P12.65 2P54.2825
UNIT 21
COM='ARRAY FOR EAST AND WEST REFLECTORS FOR NORTH REFLECTOR'
ARRAY 5 3*0.0
UNIT 22
COM='EAST AND WEST REFLECTORS FOR SOUTH REFLECTOR WITH TRIS'
CUBOID 5 1 2P24.700 2P12.65 2P54.2825
UNIT 23
COM='ARRAY FOR EAST AND WEST REFLECTORS FOR SOUTH REFLECTOR'
ARRAY 6 3*0.0

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Table A.3 (continued)

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UNIT 24
COM='NORTH TOP REFLECTOR WITH TRIS'
CUBOID 5 1 2P29.100 2P64.05 2P12.15
UNIT 25
COM='ARRAY FOR NORTH TOP REFLECTOR'
ARRAY 7 3*0.0
UNIT 26
COM='SOUTH TOP REFLECTOR WITH TRIS'
CUBOID 0 1 2P5.1 2P2.55 2P12.15
CUBOID 5 1 69.4 -5.1 2P64.05 2P12.15
UNIT 27
COM='ARRAY FOR SOUTH TOP REFLECTOR'
ARRAY 8 3*0.0
UNIT 28
COM='NORTH END REFLECTOR 9.8CM PORTION WITHOUT TRIS'
CUBOID 4 1 2P4.9000 2P64.0500 2P54.2825
UNIT 29
COM='NORTH END REFLECTOR 5.2 CM PORTION WITH TRIS'
CUBOID 5 1 2P2.6 2P64.0500 2P54.2825
UNIT 30
COM='NORTH END REFLECTOR 10.1 CM PORTION WITHOUT TRIS'
CUBOID 4 1 2P5.05 2P64.05 2P54.2825
UNIT 31
COM='ARRAY FOR NORTH END REFLECTOR'
ARRAY 9 3*0.0
UNIT 32
COM='SOUTH END REFLECTOR'
CUBOID 5 1 2P12.55 2P64.05 2P54.2825
UNIT 33
COM='ARRAY FOR SOUTH END REFLECTOR'
ARRAY 10 3*0.0
UNIT 34
COM='BOTTOM MODERATING PLASTIC NORTH CORE'
CUBOID 6 1 2P16.550 2P38.7500 2P13.0500
UNIT 35
COM='TOP MODERATING PLASTIC NORTH CORE'
CUBOID 6 1 2P16.550 2P38.7500 2P3.2525
UNIT 36
ARRAY 11 3*0.0
UNIT 37
ARRAY 12 3*0.0
UNIT 38
COM='NORTH CORE WITH BOTTOM REFLECTOR'
ARRAY 13 3* 0.0
UNIT 39
COM='NORTH CORE WITH EAST AND WEST REFLECTOR'
ARRAY 14 3*0.0
UNIT 40
COM='NORTH CORE WITH END REFLECTOR'
ARRAY 15 3*0.0
UNIT 41
COM='NORTH SPLIT TABLE FACEPLATE'
CUBOID 3 1 2P0.6150 2P64.0500 2P66.4325
UNIT 42
COM='NORTH CORE WITH TOP REFLECTOR'
ARRAY 16 3*0.0
UNIT 43
COM='NORTH CORE WITH FACEPLATE'
ARRAY 17 3*0.0
UNIT 44
COM='12.95 CM THICK MODERATOR SOUTH CORE'
CUBOID 6 1 2P23.924 2P6.475 2P40.183

UNIT 45
COM='2.95 THICK MODERATOR SOUTH CORE'
CUBOID 6 1 2P23.924 2P38.5285 2P1.475
UNIT 46
COM='COMBINATION OF CORE WITH 12.95 THICK MODERATOR'
ARRAY 18 3*0.0
UNIT 47
COM='COMBINATION OF CORE WITH 2.95 THICK MODERATOR'
ARRAY 19 3*0.0
UNIT 48
COM='SOUTH CORE WITH EAST WEST REFLECTORS'
ARRAY 20 3*0.0
UNIT 49
COM='SOUTH CORE WITH EAST WEST REFLECTORS'
ARRAY 21 3*0.0
UNIT 50
COM='SOUTH CORE END REFLECTOR'
ARRAY 22 3*0.0
UNIT 51
COM='FACEPLATE FOR SOUTH SPLIT TABLE'
CUBOID 3 1 2P0.4620 2P64.0500 2P66.4325
UNIT 52
COM='SOUTH CORE WITH TOP REFLECTOR'
ARRAY 23 3*0.0
UNIT 53
COM='SOUTH CORE WITH FACEPLATE'
ARRAY 24 3*0.0
UNIT 54
COM='AIR GAP'
CUBOID 0 1 2P0.7600 2P64.0500 2P66.4325
GLOBAL
UNIT 55
COM='TOTAL'
ARRAY 25 3*0.0
UNIT 56
COM='EMPTY FUEL LOCATION'
CUBOID 0 1 6P7.6650
UNIT 57
COM='SIDE MODERATOR'
CUBOID 6 1 2P16.550 2P4.4300 2P25.4350
UNIT 58
COM='END MODERATOR'
CUBOID 6 1 2P8.1500 2P38.7500 2P25.4350
UNIT 59
COM='SOUTH CORE BOTTOM MODERATING PLASTIC'
CUBOID 6 1 2P24.7000 2P38.7500 2P13.0500
UNIT 60
COM='SOUTH CORE TOP MODERATING PLASTIC'
CUBOID 6 1 2P24.7000 2P38.7500 2P3.2525
UNIT 61
COM='Y-FACE MODERATOR VOID'
CUBOID 0 1 2P7.665 2P1.2200 2P7.665
END GEOMETRY
READ ARRAY
ARA=1 NUX=3 NUY=7 NUZ=5
COM='NORTH SPLIT TABLE CORE'
FILL 1 2 1 3 5 3 2Q6 1 2 1
      4 7 4 6 8 6 2Q6 4 7 4
      1Q42
      56 2 1 3 5 3 1 2 1 3 5 3 1Q6 56 2 1 END FILL
ARA=2 NUX=3 NUY=7 NUZ=5
COM='SOUTH SPLIT TABLE CORE'

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Table A.3 (continued)

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FILL 1 2 1 3 5 3 2Q6 1 2 1
      4 7 4 6 8 6 2Q6 4 7 4
      1Q42
      1 2 56 3 5 3 1 2 1 3 5 3 1 2 56 3 5 61 1 2 56  END FILL
ARA=3  NUX=1 NUY=1 NUZ=3
COM='NORTH BOTTOM REFLECTOR'
FILL 14 11 13  END FILL
ARA=4  NUX=1 NUY=1 NUZ=7
COM='SOUTH BOTTOM REFLECTOR'
FILL 18 16 17 16 16 17 17  END FILL
ARA=5  NUX=1 NUY=1 NUZ=1
COM='EAST AND WEST WALLS OF NORTH REFLECTOR'
FILL 20  END FILL
ARA=6  NUX=1 NUY=1 NUZ=1
COM='EAST AND WEST WALLS OF SOUTH REFLECTOR'
FILL 22  END FILL
ARA=7  NUX=1 NUY=1 NUZ=1
COM='ARRAY FOR NORTH TOP REFLECTOR'
FILL 24  END FILL
ARA=8  NUX=1 NUY=1 NUZ=1
COM='ARRAY FOR SOUTH TOP REFLECTOR'
FILL 26  END FILL
ARA=9  NUX=3 NUY=1 NUZ=1
COM='ARRAY FOR NORTH END REFLECTOR'
FILL 28 29 30  END FILL
ARA=10 NUX=1 NUY=1 NUZ=1
COM='ARRAY FOR SOUTH END REFLECTOR'
FILL 32  END FILL
ARA=11 NUX=1 NUY=2 NUZ=1
COM='COMBINARION OF CORE WITH SIDE MODERATOR'
FILL 9 57  END FILL
ARA=12 NUX=1 NUY=1 NUZ=3
COM='COMBINATION OF PREVIOUS ARRAY WITH TOP AND BOTTOM MODERATOR'
FILL 34 36 35  END FILL
ARA=13 NUX=1 NUY=1 NUZ=2
COM='COMBINATION OF NORTH CORE WITH BOTTOM REFLECTOR'
FILL 15 37  END FILL
ARA=14 NUX=1 NUY=3 NUZ=1
COM='NORTH CORE WITH SIDE REFLECTORS'
FILL 21 38 21  END FILL
ARA=15 NUX=2 NUY=1 NUZ=1
COM='NORTH CORE WITH END REFLECTOR'
FILL 31 39  END FILL
ARA=16 NUX=1 NUY=1 NUZ=2
COM='NORTH CORE WITH TOP REFLECTOR'
FILL 40 25  END FILL
ARA=17 NUX=2 NUY=1 NUZ=1
COM='NORTH CORE WITH FACEPLATE'
FILL 42 41  END FILL
ARA=18 NUX=1 NUY=2 NUZ=1
COM='COMBINATION OF S. CORE WITH SIDE MODERATOR'
FILL 10 57  END FILL
ARA=19 NUX=2 NUY=1 NUZ=1
COM='COMBINATION OF CORE WITH END MODERATOR'
FILL 46 58  END FILL
ARA=20 NUX=1 NUY=1 NUZ=4
COM='SOUTH CORE WITH BOTTOM MODERATOR AND REFLECTOR'
FILL 19 59 47 60  END FILL
ARA=21 NUX=1 NUY=3 NUZ=1
COM='SOUTH CORE WITH EAST WEST REFLECTORS'
FILL 23 48 23  END FILL
ARA=22 NUX=2 NUY=1 NUZ=1
COM='SOUTH CORE WITH END REFLECTOR'
FILL 49 33  END FILL

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ARA=23 NUX=1 NUY=1 NUZ=2
COM='COMBINATION OF CORE WITH TOP REFLECTOR'
FILL 50 27  END FILL
ARA=24 NUX=2 NUY=1 NUZ=1
COM='SOUTH CORE WITH FACEPLATE'
FILL 51 52  END FILL
ARA=25 NUX=3 NUY=1 NUZ=1
COM='TOTAL'
FILL 43 54 53  END FILL
END ARRAY
READ PLOT TTL='XZ SLICE OF RFP2 SHOWING MATERIAL REGIONS'
XUL=-2 YUL=64.05 ZUL=136
XLR=137 YLR=64.05 ZLR=-2
UAX=1 WDN=-1 NAX=130 NCH='0123456' END
TTL='YZ SLICE OF NORTH CORE SECOND ROW'
XUL=28 YUL=-2 ZUL=136
XLR=28 YLR=136 ZLR=-2
VAX=1 WDN=-1 NAX=130 NCH='0123456' END
TTL='YZ SLICE OF SOUTH CORE SECOND ROW'
XUL=80 YUL=-2 ZUL=136
XLR=80 YLR=136 ZLR=-2
VAX=1 WDN=-1 NAX=130 NCH='0123456'
END PLOT
END DATA
END

CAR03
=CSAS25
ROCKY FLATS CRITICALS NUREG/CR-1071 EXPERIMENT NUMBER 3 (27 GROUP)
' 100 FUEL CANS 0.929 CM MODERATOR GEE.HU77.DATA(UND)
27GROUPNDF4 LATTICECELL
U308 1 5.4078E-1 293.0 92234 0.03 92235 4.46 92236 0.08 92238 95.43 END
H2O 1 8.9514E-2 END
ARB-M-BAGGIE 1.0 3 0 0 0 1001 14.01 6012 84.9 8016 1.20 1 1.9134E-2
END
ARB-M-AL1100 1.0 3 0 0 1 13027 99.18 26000 0.5 29000 0.2 2 9.5390E-1
END
ARB-M-TAPE(VINYL) 1.0 7 0 0 0 1001 5.92 6012 45.91 8016 10.82 17000
25.73 20040 6.9 22000 1.6 82000 1.1 2 1.1115E-2 END
ARB-M-TAPE(MYLAR) 1.0 3 0 0 0 1001 6.83 6012 65.50 8016 27.02 2
1.7491E-2 END
ARB-M-MODERATOR 1.185 3 0 0 0 1001 7.83 6012 59.49 8016 32.48 3 END
ARB-M-PLEX(REG) 1.0 3 0 0 0 1001 7.84 6012 59.59 8016 32.23 4
1.1773 END
ARB-M-PLEX(PAPER) 1.0 3 0 0 0 1001 6.48 6012 42.17 8016 49.5 4
3.7534E-3 END
ARB-M-PLEX(GLUE) 1.0 3 0 0 0 1001 11.67 6012 86.29 8016 1.20 4
1.1648E-3 END
ARB-M-PLEX(TRIS) 1.0 8 0 0 1 1001 7.16 6012 52.03 7014 0.16 8016 29.82
15031 1.02 17000 1.81 35079 4.260 35081 2.840 5 1.2757 END
ARB-M-PLEX(PAPER) 1.0 3 0 0 0 1001 6.48 6012 42.17 8016 49.5 5
3.7534E-3 END
ARB-M-PLEX(GLUE) 1.0 3 0 0 0 1001 11.67 6012 86.29 8016 1.20 5
1.1648E-3 END
ARB-M-FILLER 1.185 3 0 0 0 1001 7.83 6012 59.49 8016 32.48 6 0.7 END
' THIS MATERIAL IS ACTUALLY MODERATOR ADJUSTED FOR THE VOLUME
' FRACTION OF THE VOID FILLED BETWEEN CORE AND REFLECTOR.
END COMP
SPHTRIANGP 19.00 18.5857 1 3 18.9579 2 END
ROCKY FLATS CRITICALS NUREG/CR-1071 EXPERIMENT NUMBER 3 (27 GROUP)
' 100 FUEL CANS 0.929 CM MODERATOR GEE.HU77.DATA(UND)
READ PARM RUN=YES NPG=600
NUB=YES FDN=YES PLT=NO
END PARM

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Table A.3 (continued)

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READ GEOM
UNIT 1
COM='FUEL BOX 15.28 CM ON A SIDE WITH .15 CM WALLS .05CM STACKING VOID'
CUBOID 1 1 6P7.49
CUBOID 2 1 6P7.64
CUBOID 0 1 6P7.6650
UNIT 2
COM='X-FACE INTERSTITIAL MODERATOR'
CUBOID 3 1 2P0.4645 4P7.665
UNIT 3
COM='Y-FACE INTERSTITIAL MODERATOR'
CUBOID 3 1 2P7.665 2P0.4645 2P7.665
UNIT 4
COM='Z-FACE INTERSTITIAL MODERATOR'
CUBOID 3 1 4P7.665 2P0.4645
UNIT 5
COM='MORE X-FACE MODERATOR'
CUBOID 3 1 4P0.4645 2P7.665
UNIT 6
COM='MORE Y-FACE MODERATOR'
CUBOID 3 1 2P7.665 4P0.4645
UNIT 7
COM='MORE Z-FACE MODERATOR'
CUBOID 3 1 2P0.4645 2P7.665 2P0.4645
UNIT 8
COM='LAST OF INTERSTITIAL MODERATOR'
CUBOID 3 1 6P0.4645
UNIT 9
COM='NORTH SPLIT TABLE CORE'
ARRAY 1 3*0.0
UNIT 10
COM='SOUTH SPLIT TABLE CORE'
ARRAY 2 3*0.0
UNIT 11
COM='PLEXIGLASS REFLECTOR SHEET WITHOUT TRIS, NORTH BOTTOM REFLECTOR'
CUBOID 4 1 2P15.8000 2P38.7500 2P0.6150
UNIT 12
COM='PLEXIGLASS REFLECTOR SHEET WITH TRIS, NORTH BOTTOM REFLECTOR'
CUBOID 5 1 2P15.8000 2P38.7500 2P0.6150
UNIT 13
COM='UPPER PORTION NORTH BOTTOM REFLECTOR WITH TRIS'
CUBOID 5 1 2P15.8 2P38.75 2P8.24
UNIT 14
COM='LOWER PORTION NORTH BOTTOM REFLECTOR WITH TRIS'
CUBOID 5 1 2P15.8 2P38.75 2P3.69
UNIT 15
COM='NORTH BOTTOM REFLECTOR INCLUDES REGULAR AND TRIS'
ARRAY 3 3*0.0
UNIT 16
COM='PLEXIGLAS SHEET BOTTOM SOUTH REFLECTOR WITHOUT TRIS'
CUBOID 0 1 2P5.1 2P2.5 2P0.6150
CUBOID 4 1 44.3 -5.1 2P38.75 2P0.615
UNIT 17
COM='PLEXIGLAS SHEET BOTTOM SOUTH REFLECTOR WITH TRIS'
CUBOID 0 1 2P5.1 2P2.5 2P0.6150
CUBOID 5 1 44.3 -5.1 2P38.75 2P0.6150
UNIT 18
COM='LOWER PORTION SOUTH BOTTOM REFLECTOR WITH TRIS'
CUBOID 0 1 2P5.1 2P2.5 2P8.855
CUBOID 5 1 44.3 -5.1 2P38.75 2P8.855
UNIT 19
COM='SOUTH BOTTOM REFLECTOR WITH REGULAR AND TRIS'
ARRAY 4 3*0.0
UNIT 20
COM='EAST AND WEST REFLECTORS FOR NORTH REFLECTOR WITH TRIS'
CUBOID 5 1 2P15.8 2P12.65 2P54.2825

UNIT 21
COM='ARRAY FOR EAST AND WEST REFLECTORS FOR NORTH REFLECTOR'
ARRAY 5 3*0.0
UNIT 22
COM='EAST AND WEST REFLECTORS FOR SOUTH REFLECTOR WITH TRIS'
CUBOID 5 1 2P24.700 2P12.65 2P54.2825
UNIT 23
COM='ARRAY FOR EAST AND WEST REFLECTORS FOR SOUTH REFLECTOR'
ARRAY 6 3*0.0
UNIT 24
COM='NORTH TOP REFLECTOR WITH TRIS'
CUBOID 5 1 2P28.35 2P64.05 2P12.15
UNIT 25
COM='ARRAY FOR NORTH TOP REFLECTOR'
ARRAY 7 3*0.0
UNIT 26
COM='SOUTH TOP REFLECTOR WITH TRIS'
CUBOID 0 1 2P5.1 2P2.5 2P12.15
CUBOID 5 1 69.4 -5.1 2P64.05 2P12.15
UNIT 27
COM='ARRAY FOR SOUTH TOP REFLECTOR'
ARRAY 8 3*0.0
UNIT 28
COM='NORTH END REFLECTOR 9.8CM PORTION WITHOUT TRIS'
CUBOID 4 1 2P4.9000 2P64.0500 2P54.2825
UNIT 29
COM='NORTH END REFLECTOR 5.2 CM PORTION WITH TRIS'
CUBOID 5 1 2P2.6 2P64.0500 2P54.2825
UNIT 30
COM='NORTH END REFLECTOR 10.1 CM PORTION WITHOUT TRIS'
CUBOID 4 1 2P5.05 2P64.05 2P54.2825
UNIT 31
COM='ARRAY FOR NORTH END REFLECTOR'
ARRAY 9 3*0.0
UNIT 32
COM='SOUTH END REFLECTOR'
CUBOID 5 1 2P12.55 2P64.05 2P54.2825
UNIT 33
COM='ARRAY FOR SOUTH END REFLECTOR'
ARRAY 10 3*0.0
UNIT 34
COM='12.95 THICK MODERATING PLASTIC NORTH CORE'
CUBOID 6 1 2P15.7945 2P6.4750 2P40.1830
UNIT 35
COM='2.95 THICK MODERATING PLASTIC NORTH CORE'
CUBOID 6 1 2P15.7945 2P38.5285 2P1.475
UNIT 36
ARRAY 11 3*0.0
UNIT 37
ARRAY 12 3*0.0
REPLICATE 0 1 0.0 0.011 0.443 0.0 0.1590 0.0 1
UNIT 38
COM='NORTH CORE WITH BOTTOM REFLECTOR'
ARRAY 13 3* 0.0
UNIT 39
COM='NORTH CORE WITH EAST AND WEST REFLECTOR'
ARRAY 14 3*0.0
UNIT 40
COM='NORTH CORE WITH END REFLECTOR'
ARRAY 15 3*0.0
UNIT 41
COM='NORTH SPLIT TABLE FACEPLATE'
CUBOID 3 1 2P0.6150 2P64.0500 2P66.4325

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Table A.3 (continued)

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UNIT 42
COM='NORTH CORE WITH TOP REFLECTOR'
ARRAY 16 3*0.0
UNIT 43
COM='NORTH CORE WITH FACEPLATE'
ARRAY 17 3*0.0
UNIT 44
COM='12.95 CM THICK MODERATOR SOUTH CORE'
CUBOID 6 1 2P23.924 2P6.475 2P40.183
UNIT 45
COM='2.95 THICK MODERATOR SOUTH CORE'
CUBOID 6 1 2P23.924 2P38.5285 2P1.475
UNIT 46
COM='COMBINATION OF CORE WITH 12.95 THICK MODERATOR'
ARRAY 18 3*0.0
UNIT 47
COM='COMBINATION OF CORE WITH 2.95 THICK MODERATOR'
ARRAY 19 3*0.0
REPLICATE 0 1 1.552 0.0 0.4430 0.0 0.159 0.0 1
UNIT 48
COM='SOUTH CORE WITH EAST WEST REFLECTORS'
ARRAY 20 3*0.0
UNIT 49
COM='SOUTH CORE WITH EAST WEST REFLECTORS'
ARRAY 21 3*0.0
UNIT 50
COM='SOUTH CORE END REFLECTOR'
ARRAY 22 3*0.0
UNIT 51
COM='FACEPLATE FOR SOUTH SPLIT TABLE'
CUBOID 3 1 2P0.4620 2P64.0500 2P66.4325
UNIT 52
COM='SOUTH CORE WITH TOP REFLECTOR'
ARRAY 23 3*0.0
UNIT 53
COM='SOUTH CORE WITH FACEPLATE'
ARRAY 24 3*0.0
UNIT 54
COM='AIR GAP'
CUBOID 0 1 2P0.5250 2P64.0500 2P66.4325
GLOBAL
UNIT 55
COM='TOTAL'
ARRAY 25 3*0.0
END GEOMETRY
READ ARRAY
ARA=1 NUX=3 NUY=7 NUZ=9
COM='NORTH SPLIT TABLE CORE'
FILL 1 2 1 3 5 3 2Q6 1 2 1
      4 7 4 6 8 6 2Q6 4 7 4
      3Q42
      1 2 1 3 5 3 2Q6 1 2 1 END FILL
ARA=2 NUX=5 NUY=7 NUZ=9
COM='SOUTH SPLIT TABLE CORE'
FILL 1 2 1 2 1 3 5 3 5 3 2Q10 1 2 1 2 1
      4 7 4 7 4 6 8 6 8 6 2Q10 4 7 4 7 4
      3Q70
      1 2 1 2 1 3 5 3 5 3 2Q10 1 2 1 2 1 END FILL
ARA=3 NUX=1 NUY=1 NUZ=3
COM='NORTH BOTTOM REFLECTOR'
FILL 14 11 13 END FILL
ARA=4 NUX=1 NUY=1 NUZ=7
COM='SOUTH BOTTOM REFLECTOR'
FILL 18 16 17 16 16 17 17 END FILL

ARA=5 NUX=1 NUY=1 NUZ=1
COM='EAST AND WEST WALLS OF NORTH REFLECTOR'
FILL 20 END FILL
ARA=6 NUX=1 NUY=1 NUZ=1
COM='EAST AND WEST WALLS OF SOUTH REFLECTOR'
FILL 22 END FILL
ARA=7 NUX=1 NUY=1 NUZ=1
COM='ARRAY FOR NORTH TOP REFLECTOR'
FILL 24 END FILL
ARA=8 NUX=1 NUY=1 NUZ=1
COM='ARRAY FOR SOUTH TOP REFLECTOR'
FILL 26 END FILL
ARA=9 NUX=3 NUY=1 NUZ=1
COM='ARRAY FOR NORTH END REFLECTOR'
FILL 28 29 30 END FILL
ARA=10 NUX=1 NUY=1 NUZ=1
COM='ARRAY FOR SOUTH END REFLECTOR'
FILL 32 END FILL
ARA=11 NUX=1 NUY=2 NUZ=1
COM='COMBINARION OF CORE WITH 12.95CM THICK MODERATOR'
FILL 9 34 END FILL
ARA=12 NUX=1 NUY=1 NUZ=2
COM='COMBINATION OF PREVIOUS ARRAY WITH 2.95CM THICK MODERATOR'
FILL 36 35 END FILL
ARA=13 NUX=1 NUY=1 NUZ=2
COM='COMBINATION OF NORTH CORE WITH BOTTOM REFLECTOR'
FILL 15 37 END FILL
ARA=14 NUX=1 NUY=3 NUZ=1
COM='NORTH CORE WITH SIDE REFLECTORS'
FILL 21 38 21 END FILL
ARA=15 NUX=2 NUY=1 NUZ=1
COM='NORTH CORE WITH END REFLECTOR'
FILL 31 39 END FILL
ARA=16 NUX=1 NUY=1 NUZ=2
COM='NORTH CORE WITH TOP REFLECTOR'
FILL 40 25 END FILL
ARA=17 NUX=2 NUY=1 NUZ=1
COM='NORTH CORE WITH FACEPLATE'
FILL 42 41 END FILL
ARA=18 NUX=1 NUY=2 NUZ=1
COM='COMBINATION OF S. CORE WITH 12.95 CM THICK MODERATOR'
FILL 10 44 END FILL
ARA=19 NUX=1 NUY=1 NUZ=2
COM='COMBINATION OF CORE WITH 2.95 CM THICK MODERATOR'
FILL 46 45 END FILL
ARA=20 NUX=1 NUY=1 NUZ=2
COM='SOUTH CORE WITH BOTTOM REFLECTOR'
FILL 19 47 END FILL
ARA=21 NUX=1 NUY=3 NUZ=1
COM='SOUTH CORE WITH EAST WEST REFLECTORS'
FILL 23 48 23 END FILL
ARA=22 NUX=2 NUY=1 NUZ=1
COM='SOUTH CORE WITH END REFLECTOR'
FILL 49 33 END FILL
ARA=23 NUX=1 NUY=1 NUZ=2
COM='COMBINATION OF CORE WITH TOP REFLECTOR'
FILL 50 27 END FILL
ARA=24 NUX=2 NUY=1 NUZ=1
COM='SOUTH CORE WITH FACEPLATE'
FILL 51 52 END FILL
ARA=25 NUX=3 NUY=1 NUZ=1
COM='TOTAL'
FILL 43 54 53 END FILL

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Table A.3 (continued)

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END ARRAY
READ PLOT TTL='XZ SLICE OF RFP3 SHOWING MATERIAL REGIONS'
XUL=-1 YUL=64.05 ZUL=135
XLR=136 YLR=64.05 ZLR=-2
UAX=1 WDN=-1 NAX=130 NCH='0123456'END
TTL='YZ SLICE OF NORTH CORE SECOND ROW'
XUL=28 YUL=-2 ZUL=136
XLR=28 YLR=136 ZLR=-2
VAX=1 WDN=-1 NAX=130 NCH='0123456'END
TTL='YZ SLICE OF SOUTH CORE SECOND ROW'
XUL=90 YUL=-2 ZUL=136
XLR=90 YLR=136 ZLR=-2
VAX=1 WDN=-1 NAX=130 NCH='0123456'
END PLOT
END DATA
END

CAR04
=CSAS25
ROCKY FLATS CRITICALS NUREG/CR-1071 EXPERIMENT NUMBER 13 (27 GROUP)
27GROUNDF4 LATTICECELL
U308 1 5.4078E-1 293.0 92234 0.03 92235 4.46 92236 0.08 92238 95.43 END
H2O 1 8.9514E-2 END
ARBM-BAGGIE 1.0 3 0 0 0 1001 14.01 6012 84.9 8016 1.20 1 1.9134E-2
END
ARBM-AL1100 1.0 3 0 0 1 13027 99.18 26000 0.5 29000 0.2 2 9.5390E-1
END
ARBM-TAPE(VINYL) 1.0 7 0 0 0 1001 5.92 6012 45.91 8016 10.82 17000
25.73 20040 6.9 22000 1.6 82000 1.1 2 1.1115E-2 END
ARBM-TAPE(MYLAR) 1.0 3 0 0 0 1001 6.83 6012 65.50 8016 27.02 2
1.7491E-2 END
ARBM-MODERATOR 1.185 3 0 0 0 1001 7.83 6012 59.49 8016 32.48 3 END
RFCONCRETE 5 1.0 END
END COMP
SPHTRIANGP 19.9462 18.5857 1 3 18.9579 2 END
ROCKY FLATS CRITICALS NUREG/CR-1071 EXPERIMENT NUMBER 13 (27 GROUP)
READ PARM RUN=YES NPG=600
PLT=NO FDN=YES NUB=YES
END PARM
READ GEOM
UNIT 1
COM='FUEL BOX 15.28 CM ON A SIDE WITH .15 CM WALLS .05CM STACKING VOID'
CUBOID 1 1 6P7.49
CUBOID 2 1 6P7.64
CUBOID 0 1 6P7.6650
UNIT 2
COM='X-FACE INTERSTITIAL MODERATOR'
CUBOID 3 1 2P1.2200 4P7.665
UNIT 3
COM='Y-FACE INTERSTITIAL MODERATOR'
CUBOID 3 1 2P7.665 2P1.2200 2P7.665
UNIT 4
COM='Z-FACE INTERSTITIAL MODERATOR'
CUBOID 3 1 4P7.665 2P1.2200
UNIT 5
COM='MORE X-FACE MODERATOR'
CUBOID 3 1 4P1.2200 2P7.665
UNIT 6
COM='MORE Y-FACE MODERATOR'
CUBOID 3 1 2P7.665 4P1.2200

UNIT 7
COM='MORE Z-FACE MODERATOR'
CUBOID 3 1 2P1.2200 2P7.665 2P1.2200
UNIT 8
COM='LAST OF INTERSTITIAL MODERATOR'
CUBOID 3 1 6P1.2200
UNIT 9
COM='NORTH SPLIT TABLE CORE'
ARRAY 1 -33.1 2*0.0
CUBOID 5 1 0.0 -33.6 76.2 0.0 50.87 -30.5
CUBOID 0 1 0.0 -33.6 77.5 0.0 52.70 -30.5
CUBOID 5 1 0.0 -33.6 103.0 -25.5 78.2 -56.0
CUBOID 0 1 0.0 -34.3 103.0 -25.5 78.2 -56.0
CUBOID 5 1 0.0 -59.9 103.0 -25.5 78.2 -56.0
UNIT 10
COM='SOUTH SPLIT TABLE CORE'
ARRAY 2 3*0.0
CUBOID 5 1 44.4 0.0 76.2 0.0 50.87 -30.5
CUBOID 0 1 47.5 0.0 77.5 0.0 52.70 -30.5
CUBOID 5 1 73.0 0.0 103.0 -25.5 78.2 -56.0
HOLE 11 0.0 38.75 -56.0
HOLE 11 0.0 38.75 52.7
UNIT 11
CUBOID 0 1 10.2 0.0 2P2.55 25.5 0.0
UNIT 12
COM='NORTH SPLIT TABLE FACEPLATE'
CUBOID 3 1 2P0.6150 2P64.2500 2P67.1
UNIT 13
COM='FACEPLATE FOR SOUTH SPLIT TABLE'
CUBOID 3 1 2P0.6150 2P64.2500 2P67.1
UNIT 14
COM='AIR GAP'
CUBOID 0 1 2P0.2850 2P64.2500 2P67.1
GLOBAL
UNIT 15
COM='TOTAL'
ARRAY 3 3*0.0
UNIT 56
COM='EMPTY FUEL LOCATION'
CUBOID 0 1 6P7.6650
UNIT 61
COM='Y-FACE MODERATOR VOID'
CUBOID 0 1 2P7.665 2P1.2200 2P7.665
END GEOMETRY
READ ARRAY
ARA=1 NUX=3 NUY=7 NUZ=5
COM='NORTH SPLIT TABLE CORE'
FILL 1 2 1 3 5 3 2Q6 1 2 1
4 7 4 6 8 6 2Q6 4 7 4
1Q42
56 2 1 61 5 3 2Q6 56 2 1 END FILL
ARA=2 NUX=3 NUY=7 NUZ=5
COM='SOUTH SPLIT TABLE CORE'
FILL 1 2 1 3 5 3 2Q6 1 2 1
4 7 4 6 8 6 2Q6 4 7 4
1Q42
1 2 56 3 5 61 2Q6 1 2 56 END FILL
ARA=3 NUX=5 NUY=1 NUZ=1
COM='TOTAL'
FILL 9 12 14 13 10 END FILL
END ARRAY

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Table A.3 (continued)

READ PLOT TTL='XZ SLICE OF RFP1 SHOWING MATERIAL REGIONS'
 XUL=-2 YUL=64.05 ZUL=136
 XLR=137 YLR=64.05 ZLR=-2
 UAX=1 WDN=-1 NAX=130 NCH='0123456'END
 TTL='YZ SLICE OF NORTH CORE SECOND ROW'
 XUL=28 YUL=-2 ZUL=136
 XLR=28 YLR=136 ZLR=-2
 VAX=1 WDN=-1 NAX=130 NCH='0123456'END
 TTL='YZ SLICE OF SOUTH CORE SECOND ROW'
 XUL=80 YUL=-2 ZUL=136
 XLR=80 YLR=136 ZLR=-2
 VAX=1 WDN=-1 NAX=130 NCH='0123456'
 END PLOT
 READ START NST=1
 XSM=15 XSP=122 YSM=15 YSP=122 ZSM=30 ZSP=122 END START
 END DATA
 END

CAR05
 =CSAS25
 ROCKY FLATS CRITICALS NUREG/CR-1071 EXPERIMENT NUMBER 15 (27 GROUP)
 27GROUPNDF4 LATTICECELL
 U308 1 5.4078E-1 293.0 92234 0.03 92235 4.46 92236 0.08 92238 95.43 END
 H2O 1 8.9514E-2 END
 ARBM-BAGGIE 1.0 3 0 0 0 1001 14.01 6012 84.9 8016 1.20 1 1.9134E-2
 END
 ARBM-AL1100 1.0 3 0 0 1 13027 99.18 26000 0.5 29000 0.2 2 9.5390E-1
 END
 ARBM-TAPE(VINYL) 1.0 7 0 0 0 1001 5.92 6012 45.91 8016 10.82 17000
 25.73 20040 6.9 22000 1.6 82000 1.1 2 1.1115E-2 END
 ARBM-TAPE(MYLAR) 1.0 3 0 0 0 1001 6.83 6012 65.50 8016 27.02 2
 1.7491E-2 END
 ARBM-MODERATOR 1.185 3 0 0 0 1001 7.83 6012 59.49 8016 32.48 3 END
 RPCONCRETE 5 1.0 END
 END COMP
 SPHTRIANGP 19.0000 18.5857 1 3 18.9579 2 END
 ROCKY FLATS CRITICALS NUREG/CR-1071 EXPERIMENT NUMBER 15 (27 GROUP)
 READ PARM RUN=YES NPG=600 PLT=NO
 FDN=YES NUB=YES
 END PARM
 READ GEOM
 UNIT 1
 COM='FUEL BOX 15.28 CM ON A SIDE WITH .15 CM WALLS .05CM STACKING VOID'
 CUBOID 1 1 6P7.49
 CUBOID 2 1 6P7.64
 CUBOID 0 1 6P7.6650
 UNIT 2
 COM='X-FACE INTERSTITIAL MODERATOR'
 CUBOID 3 1 2P0.4645 4P7.665
 UNIT 3
 COM='Y-FACE INTERSTITIAL MODERATOR'
 CUBOID 3 1 2P7.665 2P0.4645 2P7.665
 UNIT 4
 COM='Z-FACE INTERSTITIAL MODERATOR'
 CUBOID 3 1 4P7.665 2P0.4645
 UNIT 5
 COM='MORE X-FACE MODERATOR'
 CUBOID 3 1 4P0.4645 2P7.665
 UNIT 6
 COM='MORE Y-FACE MODERATOR'
 CUBOID 3 1 2P7.665 4P0.4645

UNIT 7
 COM='MORE Z-FACE MODERATOR'
 CUBOID 3 1 2P0.4645 2P7.665 2P0.4645
 UNIT 8
 COM='LAST OF INTERSTITIAL MODERATOR'
 CUBOID 3 1 6P0.4645
 UNIT 9
 COM='NORTH SPLIT TABLE CORE'
 ARRAY 1 -31.589 2*0.0
 CUBOID 5 1 0.0 -31.589 76.207 0.0 80.366 -25.5
 CUBOID 0 1 0.0 -32.3 77.5 0.0 83.2 -25.5
 CUBOID 5 1 0.0 -57.8 103.0 -25.5 108.7 -25.5
 UNIT 10
 COM='SOUTH SPLIT TABLE CORE'
 ARRAY 2 3*0.0
 CUBOID 5 1 47.848 0.0 76.207 0.0 80.366 -25.5
 HOLE 11 0.0 38.75 -25.5
 CUBOID 0 1 47.848 0.0 77.5 0.0 83.2 -25.5
 CUBOID 5 1 47.848 0.0 103.0 -25.5 108.7 -25.5
 HOLE 11 0.0 38.75 83.2
 CUBOID 0 1 48.848 0.0 103.0 -25.5 108.7 -25.5
 CUBOID 5 1 74.348 0.0 103.0 -25.5 108.7 -25.5
 UNIT 11
 CUBOID 0 1 10.2 0.0 2P2.55 25.5 0.0
 UNIT 12
 COM='NORTH SPLIT TABLE FACEPLATE'
 CUBOID 3 1 2P0.0 2P64.2500 2P67.1
 UNIT 13
 COM='FACEPLATE FOR SOUTH SPLIT TABLE'
 CUBOID 3 1 2P0.4620 2P64.2500 2P67.1
 UNIT 14
 COM='AIR GAP'
 CUBOID 0 1 2P0.2850 2P64.2500 2P67.1
 GLOBAL
 UNIT 15
 COM='TOTAL'
 ARRAY 3 3*0.0
 UNIT 56
 COM='EMPTY FUEL LOCATION'
 CUBOID 0 1 6P7.6650
 UNIT 61
 COM='Y-FACE MODERATOR VOID'
 CUBOID 0 1 2P7.665 2P0.4645 2P7.665
 END GEOMETRY
 READ ARRAY
 ARA=1 NUX=3 NUZ=7 NUZ=9
 COM='NORTH SPLIT TABLE CORE'
 FILL 1 2 1 3 5 3 2Q6 1 2 1
 4 7 4 6 8 6 2Q6 4 7 4
 3Q42
 1 2 1 3 5 3 2Q6 1 2 1 END FILL
 ARA=2 NUX=5 NUZ=7 NUZ=9
 COM='SOUTH SPLIT TABLE CORE'
 FILL 1 2 1 2 1 3 5 3 5 3 2Q10 1 2 1 2 1
 4 7 4 7 4 6 8 6 8 6 2Q10 4 7 4 7 4
 3Q70
 1 2 1 2 1 3 5 3 5 3
 56 2 1 2 1 61 5 3 5 3
 56 2 1 2 1 3 5 3 5 3
 1 2 1 2 1 END FILL
 ARA=3 NUX=5 NUZ=1 NUZ=1
 COM='TOTAL'
 FILL 9 12 14 13 10 END FILL

Table A.3 (continued)

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END ARRAY
READ PLOT TTL='XZ SLICE OF RFP1 SHOWING MATERIAL REGIONS'
XUL=-2 YUL=64.05 ZUL=136
XLR=137 YLR=64.05 ZLR=-2
UAX=1 WDN=-1 NAX=130 NCH='0123456'END
TTL='YZ SLICE OF NORTH CORE SECOND ROW'
XUL=28 YUL=-2 ZUL=136
XLR=28 YLR=136 ZLR=-2
VAX=1 WDN=-1 NAX=130 NCH='0123456'END
TTL='YZ SLICE OF SOUTH CORE SECOND ROW'
XUL=80 YUL=-2 ZUL=136
XLR=80 YLR=136 ZLR=-2
VAX=1 WDN=-1 NAX=130 NCH='0123456'
END PLOT
READ START NST=1
XSM=15 XSP=122 YSM=15 YSP=122 ZSM=30 ZSP=122 END START
END DATA
END

CAR06
=CSAS25
ROCKY FLATS CRITICALS NUREG/CR-0674 EXPERIMENT NUMBER ? (27 GROUP MODEL)
' FUEL CUBE 15.28 CM, U(4.46)308 @ H/U=0.77, HI ENRICHED SPHERE DRIVEN
27GROUPNDF4 INFHOMMEDIUM
U308 1 5.4078E-1 293.0 92234 0.03 92235 4.46 92236 0.08 92238 95.43 END
H2O 1 8.9514E-2 END
ARBM-BAGGIE 1.0 3 0 0 0 1001 14.01 6012 84.9 8016 1.20 1 1.9134E-2
END
ARBM-AL1100 1.0 3 0 0 1 13027 99.18 26000 0.5 29000 0.2 2 9.5390E-1
END
ARBM-TAPE(VINYL) 1.0 7 0 0 0 1001 5.92 6012 45.91 8016 10.82 17000
25.73 20040 6.9 22000 1.6 82000 1.1 2 1.1115E-2 END
ARBM-TAPE(MYLAR) 1.0 3 0 0 0 1001 6.83 6012 65.50 8016 27.02 2
1.7491E-2 END
ARBM-MODERATOR 1.185 3 0 0 0 1001 7.83 6012 59.49 8016 32.48 3 END
ARBM-FLEX(REG) 1.0 3 0 0 0 1001 7.84 6012 59.59 8016 32.23 4
1.1773 END
ARBM-FLEX(PAPER) 1.0 3 0 0 0 1001 6.48 6012 42.17 8016 49.5 4
3.7534E-3 END
ARBM-FLEX(GLUE) 1.0 3 0 0 0 1001 11.67 6012 86.29 8016 1.20 4
1.1648E-3 END
ARBM-FLEX(TRIS) 1.0 8 0 0 1 1001 7.16 6012 52.03 7014 0.16 8016 29.82
15031 1.02 17000 1.81 35079 4.260 35081 2.840 5 1.2757 END
ARBM-FLEX(PAPER) 1.0 3 0 0 0 1001 6.48 6012 42.17 8016 49.5 5
3.7534E-3 END
ARBM-FLEX(GLUE) 1.0 3 0 0 0 1001 11.67 6012 86.29 8016 1.20 5
1.1648E-3 END
ARBM-FILLER 1.185 3 0 0 0 1001 7.83 6012 59.49 8016 32.48 6 0.7 END
' THIS MATERIAL IS ACTUALLY MODERATOR ADJUSTED FOR THE VOLUME
' FRACTION OF THE VOID FILLED BETWEEN CORE AND REFLECTOR.
ARBM-AL1100 1.0 3 0 0 1 13027 99.18 26000 0.5 29000 0.2 7 2.715 END
URANIUM 8 0.9516 293.0 92234 1.0 92235 93.19 92236 0.4 92238 5.41 END
ARBM-PJ 0.816 2 0 0 0 1001 85.1 6012 14.9 8 0.0041 END
SS304 9 1.0 END
END COMP
ROCKY FLATS CRITICALS NUREG/CR-0674 EXPERIMENT NUMBER ? (27 GROUP MODEL)
' FUEL CUBE 15.28 CM, U(4.46)308 @ H/U=0.77, HI ENRICHED SPHERE DRIVEN
READ PARM NPG=600 NUB=YES PDN=YES PLT=NO END PARM
READ GEOM

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UNIT 1
COM='FUEL BOX WITH VOID AND PART OF AL BOX'
CUBOID 0 1 9.80 0.0 3.75 0.0 14.98 0.0
CUBOID 2 1 9.95 0.0 3.90 -0.15 14.98 0.0
CUBOID 1 1 14.98 0.0 9.365 -5.615 14.98 0.0
UNIT 2
COM='FRONT OF FUEL BOX'
CUBOID 2 1 0.15 0.0 5.615 0.0 14.98 0.0
CUBOID 0 1 0.15 0.0 9.365 0.0 14.98 0.0
CUBOID 2 1 0.15 0.0 14.98 0.0 14.98 0.0
UNIT 3
COM='REAR OF FUEL BOX'
CUBOID 2 1 0.15 0.0 14.98 0.0 14.98 0.0
UNIT 4
COM='ARRAY TO ASSEMBLE PART OF BOX'
ARRAY 26 3*0
UNIT 5
COM='TOP AND BOTTOM OF BOX'
CUBOID 0 1 9.80 0.0 3.750 0.0 0.15 0.0
CUBOID 2 1 15.28 0.0 9.365 -5.615 0.15 0.0
GLOBAL
UNIT 6
COM='ARRAY TO ASSEMBLE TOP AND BOTTOM'
ARRAY 27 3*0
CUBOID 2 1 15.28 0.0 15.13 -0.15 15.28 0.0
CUBOID 0 1 15.305 -0.025 15.155 -0.175 15.305 -0.025
UNIT 7
COM='FUEL BOX 15.28 CM ON A SIDE WITH .15 CM WALLS .05CM STACKING VOID'
CUBOID 1 1 6P7.49
CUBOID 2 1 6P7.64
CUBOID 0 1 6P7.6650
UNIT 8
COM='BOX FOR DRIVER'
CYLINDER 9 1 0.3175 2P7.32
HEMISPHE+X 8 1 7.334 CHORD 6.818
CUBOID 0 1 8.512 -6.818 2P7.665 2P7.665
HOLE 37 0.0 0.0 -7.665
UNIT 34
COM='ALUMINUM WEIGHT DISTRIBUTION PLATE FOR SPECIAL BOX'
CUBOID 0 1 9.80 0.0 3.750 0.0 0.16 0.0
CUBOID 7 1 15.33 0.0 9.54 -5.79 0.16 0.0
UNIT 35
COM='ALUMINUM WEIGHT DISTRIBUTION PLATE FOR BOXES'
CUBOID 7 1 4P7.665 0.16 0.0
UNIT 37
COM='DRIVER MOUNT'
CYLINDER 9 1 1.56 0.331 0.0
UNIT 9
COM='NORTH SPLIT TABLE CORE'
ARRAY 1 3*0.0
CUBOID 0 1 30.66 -0.94 77.5 0.0 83.475 0.0
UNIT 10
COM='SOUTH SPLIT TABLE CORE'
ARRAY 2 3*0.0
CUBOID 0 1 49.4 0.0 77.5 0.0 83.475 0.0
UNIT 11
COM='PLEXIGLASS REFLECTOR SHEET WITHOUT TRIS, NORTH BOTTOM REFLECTOR'
CUBOID 4 1 2P15.8000 2P38.7500 2P0.6150
UNIT 12
COM='PLEXIGLASS REFLECTOR SHEET WITH TRIS, NORTH BOTTOM REFLECTOR'
CUBOID 5 1 2P15.8000 2P38.7500 2P0.6150
UNIT 13
COM='UPPER PORTION NORTH BOTTOM REFLECTOR WITH TRIS'
CUBOID 5 1 2P15.8 2P38.75 2P8.24

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Table A.3 (continued)

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UNIT 14
COM='LOWER PORTION NORTH BOTTOM REFLECTOR WITH TRIS'
CUBOID 5 1 2P15.8 2P38.75 2P3.69
UNIT 15
COM='NORTH BOTTOM REFLECTOR INCLUDES REGULAR AND TRIS'
ARRAY 3 3*0.0
UNIT 16
COM='PLEXIGLAS SHEET BOTTOM SOUTH REFLECTOR WITHOUT TRIS'
CUBOID 0 1 2P5.1 2P2.5 2P0.6150
CUBOID 4 1 44.3 -5.1 2P38.75 2P0.615
UNIT 17
COM='PLEXIGLAS SHEET BOTTOM SOUTH REFLECTOR WITH TRIS'
CUBOID 0 1 2P5.1 2P2.5 2P0.6150
CUBOID 5 1 44.3 -5.1 2P38.75 2P0.6150
UNIT 18
COM='LOWER PORTION SOUTH BOTTOM REFLECTOR WITH TRIS'
CUBOID 0 1 2P5.1 2P2.5 2P8.855
CUBOID 5 1 44.3 -5.1 2P38.75 2P8.855
UNIT 19
COM='SOUTH BOTTOM REFLECTOR WITH REGULAR AND TRIS'
ARRAY 4 3*0.0
UNIT 20
COM='EAST AND WEST REFLECTORS FOR NORTH REFLECTOR WITH TRIS'
CUBOID 5 1 2P15.8 2P12.65 2P54.2825
UNIT 21
COM='ARRAY FOR EAST AND WEST REFLECTORS FOR NORTH REFLECTOR'
ARRAY 5 3*0.0
UNIT 22
COM='EAST AND WEST REFLECTORS FOR SOUTH REFLECTOR WITH TRIS'
CUBOID 5 1 2P24.700 2P12.65 2P54.2825
UNIT 23
COM='ARRAY FOR EAST AND WEST REFLECTORS FOR SOUTH REFLECTOR'
ARRAY 6 3*0.0
UNIT 24
COM='NORTH TOP REFLECTOR WITH TRIS'
CUBOID 5 1 2P28.35 2P64.05 2P12.15
UNIT 25
COM='ARRAY FOR NORTH TOP REFLECTOR'
ARRAY 7 3*0.0
UNIT 26
COM='SOUTH TOP REFLECTOR WITH TRIS'
CUBOID 0 1 2P5.1 2P2.5 2P12.15
CUBOID 5 1 69.4 -5.1 2P64.05 2P12.15
UNIT 27
COM='ARRAY FOR SOUTH TOP REFLECTOR'
ARRAY 8 3*0.0
UNIT 28
COM='NORTH END REFLECTOR 9.8CM PORTION WITHOUT TRIS'
CUBOID 4 1 2P4.9000 2P64.0500 2P54.2825
UNIT 29
COM='NORTH END REFLECTOR 5.2 CM PORTION WITH TRIS'
CUBOID 5 1 2P2.6 2P64.0500 2P54.2825
UNIT 30
COM='NORTH END REFLECTOR 10.1 CM PORTION WITHOUT TRIS'
CUBOID 4 1 2P5.05 2P64.05 2P54.2825
UNIT 31
COM='ARRAY FOR NORTH END REFLECTOR'
ARRAY 9 3*0.0
UNIT 32
COM='SOUTH END REFLECTOR'
CUBOID 5 1 2P12.55 2P64.05 2P54.2825
UNIT 33
COM='ARRAY FOR SOUTH END REFLECTOR'
ARRAY 10 3*0.0

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UNIT 38
COM='NORTH CORE WITH BOTTOM REFLECTOR'
ARRAY 13 3* 0.0
UNIT 39
COM='NORTH CORE WITH EAST AND WEST REFLECTOR'
ARRAY 14 3*0.0
UNIT 40
COM='NORTH CORE WITH END REFLECTOR'
ARRAY 15 3*0.0
UNIT 42
COM='NORTH CORE WITH TOP REFLECTOR'
ARRAY 16 3*0.0
UNIT 48
COM='SOUTH CORE WITH BOTTOM REFLECTORS'
ARRAY 20 3*0.0
UNIT 49
COM='SOUTH CORE WITH EAST WEST REFLECTORS'
ARRAY 21 3*0.0
UNIT 50
COM='SOUTH CORE END REFLECTOP'
ARRAY 22 3*0.0
UNIT 52
COM='SOUTH CORE WITH TOP REFLECTOR'
ARRAY 23 3*0.0
UNIT 54
COM='AIR GAP'
HEMISPHE-X 8 1 7.334 CHORD -6.818
CUBOID 0 1 -6.818 -7.619 64.475 -63.625 69.13 -63.735
GLOBAL
UNIT 55
COM='TOTAL'
ARRAY 25 3*0.0
END GEOMETRY
READ ARRAY
ARA=1 NUX=2 NUY=5 NUZ=9
COM='NORTH SPLIT TABLE CORE'
FILL 10R7
      10R35
      10R7
      10R35
      10R7
      10R35
      10R7
      10R35
      10R7 END FILL
ARA=2 NUX=3 NUY=5 NUZ=9
COM='SOUTH SPLIT TABLE CORE'
FILL 6R7 6 8R7
      6R35 34 8R35
      6R7 6 8R7
      6R35 34 8R35
      6R7 8 8R7
      6R35 34 8R35
      6R7 6 8R7
      6R35 34 8R35
      6R7 6 8R7 END FILL
ARA=3 NUX=1 NUY=1 NUZ=3
COM='NORTH BOTTOM REFLECTOR'
FILL 14 11 13 END FILL
ARA=4 NUX=1 NUY=1 NUZ=7
COM='SOUTH BOTTOM REFLECTOR'
FILL 18 16 17 16 16 17 17 END FILL
ARA=5 NUX=1 NUY=1 NUZ=1
COM='EAST AND WEST WALLS OF NORTH REFLECTOR'
FILL 20 END FILL

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Table A.3 (continued)

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ARA=6 NUX=1 NUY=1 NUZ=1
COM='EAST AND WEST WALLS OF SOUTH REFLECTOR'
FILL 22 END FILL
ARA=7 NUX=1 NUY=1 NUZ=1
COM='ARRAY FOR NORTH TOP REFLECTOR'
FILL 24 END FILL
ARA=8 NUX=1 NUY=1 NUZ=1
COM='ARRAY FOR SOUTH TOP REFLECTOR'
FILL 26 END FILL
ARA=9 NUX=3 NUY=1 NUZ=1
COM='ARRAY FOR NORTH END REFLECTOR'
FILL 28 29 30 END FILL
ARA=10 NUX=1 NUY=1 NUZ=1
COM='ARRAY FOR SOUTH END REFLECTOR'
FILL 32 END FILL
ARA=13 NUX=1 NUY=1 NUZ=2
COM='COMBINATION OF NORTH CORE WITH BOTTOM REFLECTOR'
FILL 15 9 END FILL
ARA=14 NUX=1 NUY=3 NUZ=1
COM='NORTH CORE WITH SIDE REFLECTORS'
FILL 21 38 21 END FILL
ARA=15 NUX=2 NUY=1 NUZ=1
COM='NORTH CORE WITH END REFLECTOR'
FILL 31 39 END FILL
ARA=16 NUX=1 NUY=1 NUZ=2
COM='NORTH CORE WITH TOP REFLECTOR'
FILL 40 25 END FILL
ARA=20 NUX=1 NUY=1 NUZ=2
COM='SOUTH CORE WITH BOTTOM REFLECTOR'
FILL 19 10 END FILL
ARA=21 NUX=1 NUY=3 NUZ=1
COM='SOUTH CORE WITH EAST WEST REFLECTORS'
FILL 23 48 23 END FILL
ARA=22 NUX=2 NUY=1 NUZ=1
COM='SOUTH CORE WITH END REFLECTOR'
FILL 49 33 END FILL
ARA=23 NUX=1 NUY=1 NUZ=2
COM='COMBINATION OF CORE WITH TOP REFLECTOR'
FILL 50 27 END FILL
ARA=25 NUX=3 NUY=1 NUZ=1
COM='TOTAL'
FILL 42 54 52 END FILL
ARA=26 NUX=3 NUY=1 NUZ=1
COM='ASSEMBLY OF FUEL BOX FRONT AND REAR'
FILL 2 1 3 END FILL
ARA=27 NUX=1 NUY=1 NUZ=3
COM='ASSEMBLY OF FUEL BOX TOP AND BOTTOM'
FILL 5 4 5 END FILL
END ARRAY
READ PLOT TTL='YZ SLICE OF SOUTH CORE FIRST ROW'
XUL=64.319 YUL=55.625 ZUL=71.735
XLR=64.319 YLR=71.625 ZLR=55.735
VAX=1 WDN=-1 NAX=130 NCH='012345678'END
TTL='XZ SLICE OF SPHERE CUBOID'
XUL=56.0 YUL=63.625 ZUL=71.735
XLR=72.0 YLR=63.625 ZLR=55.735
UAX=1 WDN=-1 NAX=130 NCH='012345678'
END PLOT
' READ START NST=6 TFX=65 TFY=63.625 TFPZ=63.735 LNU=300 END START
READ START NST=1 XSM=56.981 XSP=71.649 YSM=56.219 YSP=70.959
ZSM=56.401 ZSP=71.069 END START
END DATA
END

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CAR07
=CSAS25
ROCKY FLATS CRITICALS NUREG/CR-0674 EXPERIMENT NUMBER ? (27 GROUP MODEL)
' FUEL CUBE 15.28 CM, U(4.46)308 @ H/U=0.77, HI CONC. SOLUTION DRIVEN
27GROUPE4 INFHOMMEDIUM
U308 1 5.4078E-1 293.0 92234 0.03 92235 4.46 92236 0.08 92238 95.43 END
H2O 1 8.9514E-2 END
ARBM-BAGGIE 1.0 3 0 0 0 1001 14.01 6012 84.9 8016 1.20 1 1.9134E-2
END
ARBM-AL1100 1.0 3 0 0 1 13027 99.18 26000 0.5 29000 0.2 2 9.5390E-1
END
ARBM-TAPE(VINYL) 1.0 7 0 0 0 1001 5.92 6012 45.91 8016 10.82 17000
25.73 20040 6.9 22000 1.6 82000 1.1 2 1.1115E-2 END
ARBM-TAPE(MYLAR) 1.0 3 0 0 0 1001 6.83 6012 65.50 8016 27.02 2
1.7491E-2 END
ARBM-MODERATOR 1.185 3 0 0 0 1001 7.83 6012 59.49 8016 32.48 3 END
ARBM-PLEX(REG) 1.0 3 0 0 0 1001 7.84 6012 59.59 8016 32.23 4
1.1773 END
ARBM-PLEX(PAPER) 1.0 3 0 0 0 1001 6.48 6012 42.17 8016 49.5 4
3.7534E-3 END
ARBM-PLEX(GLUE) 1.0 3 0 0 0 1001 11.67 6012 86.29 8016 1.20 4
1.1648E-3 END
ARBM-PLEX(TRIS) 1.0 8 0 0 1 1001 7.16 6012 52.03 7014 0.16 8016 29.82
15031 1.02 17000 1.81 35079 4.260 35081 2.840 5 1.2757 END
ARBM-PLEX(PAPER) 1.0 3 0 0 0 1001 6.48 6012 42.17 8016 49.5 5
3.7534E-3 END
ARBM-PLEX(GLUE) 1.0 3 0 0 0 1001 11.67 6012 86.29 8016 1.20 5
1.1648E-3 END
ARBM-FILLER 1.185 3 0 0 0 1001 7.83 6012 59.49 8016 32.48 6 0.7 END
' THIS MATERIAL IS ACTUALLY MODERATOR ADJUSTED FOR THE VOLUME
' FRACTION OF THE VOID FILLED BETWEEN CORE AND REFLECTOR.
ARBM-AL1100 1.0 3 0 0 1 13027 99.18 26000 0.5 29000 0.2 7 2.715 END
SOLNUO2(NO3)2 8 351.18 0.549 1.0 293.0 92234 1.022 92235 93.172
92236 0.434 92238 5.372 END
SS304 9 1.0 END
END COMP
ROCKY FLATS CRITICALS NUREG/CR-0674 EXPERIMENT NUMBER ? (27 GROUP MODEL)
' FUEL CUBE 15.28 CM, U(4.46)308 @ H/U=0.77, HI CONC. SOLUTION DRIVEN
READ PARM NPG=600 NUB=YES FDN=YES PLT=NO END PARM
READ GROM
UNIT 1
COM='FUEL BOX WITH VOID AND PART OF AL BOX'
CUBOID 0 1 9.80 0.0 3.75 0.0 14.98 0.0
CUBOID 2 1 9.95 0.0 3.90 -0.15 14.98 0.0
CUBOID 1 1 14.98 0.0 9.365 -5.615 14.98 0.0
UNIT 2
COM='FRONT OF FUEL BOX'
CUBOID 2 1 0.15 0.0 5.615 0.0 14.98 0.0
CUBOID 0 1 0.15 0.0 9.365 0.0 14.98 0.0
CUBOID 2 1 0.15 0.0 14.98 0.0 14.98 0.0
UNIT 3
COM='REAR OF FUEL BOX'
CUBOID 2 1 0.15 0.0 14.98 0.0 14.98 0.0
UNIT 4
COM='ARRAY TO ASSEMBLE PART OF BOX'
ARRAY 26 3*0
UNIT 5
COM='TOP AND BOTTOM OF BOX'
CUBOID 0 1 9.80 0.0 3.750 0.0 0.15 0.0
CUBOID 2 1 15.28 0.0 9.365 -5.615 0.15 0.0
GLOBAL

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Table A.3 (continued)

UNIT 6
 COM='ARRAY TO ASSEMBLE TOP AND BOTTOM'
 ARRAY 27 3*0
 CUBOID 2 1 15.28 0.0 15.13 -0.15 15.28 0.0
 CUBOID 0 1 15.305 -0.025 15.155 -0.175 15.305 -0.025
 UNIT 7
 COM='FUEL BOX 15.28 CM ON A SIDE WITH .15 CM WALLS .05CM STACKING VOID'
 CUBOID 1 1 6P7.49
 CUBOID 2 1 6P7.64
 CUBOID 0 1 6P7.6650
 UNIT 34
 COM='ALUMINUM WEIGHT DISTRIBUTION PLATE FOR SPECIAL BOX'
 CUBOID 0 1 9.80 0.0 3.750 0.0 0.16 0.0
 CUBOID 7 1 15.33 0.0 9.54 -5.79 0.16 0.0
 UNIT 35
 COM='ALUMINUM WEIGHT DISTRIBUTION PLATE FOR BOXES'
 CUBOID 7 1 4P7.665 0.16 0.0
 UNIT 9
 COM='NORTH SPLIT TABLE CORE'
 ARRAY 1 3*0.0
 CUBOID 0 1 30.66 -0.94 77.5 0.0 83.475 0.0
 UNIT 10
 COM='SOUTH SPLIT TABLE CORE'
 ARRAY 2 3*0.0
 CUBOID 0 1 49.4 0.0 77.5 0.0 83.475 0.0
 UNIT 11
 COM='PLEXIGLASS REFLECTOR SHEET WITHOUT TRIS, NORTH BOTTOM REFLECTOR'
 CUBOID 4 1 2P15.8000 2P38.7500 2P0.6150
 UNIT 12
 COM='PLEXIGLASS REFLECTOR SHEET WITH TRIS, NORTH BOTTOM REFLECTOR'
 CUBOID 5 1 2P15.8000 2P38.7500 2P0.6150
 UNIT 13
 COM='UPPER PORTION NORTH BOTTOM REFLECTOR WITH TRIS'
 CUBOID 5 1 2P15.8 2P38.75 2P8.24
 UNIT 14
 COM='LOWER PORTION NORTH BOTTOM REFLECTOR WITH TRIS'
 CUBOID 5 1 2P15.8 2P38.75 2P3.69
 UNIT 15
 COM='NORTH BOTTOM REFLECTOR INCLUDES REGULAR AND TRIS'
 ARRAY 3 3*0.0
 UNIT 16
 COM='PLEXIGLAS SHEET BOTTOM SOUTH REFLECTOR WITHOUT TRIS'
 CUBOID 0 1 2P5.1 2P2.5 2P0.6150
 CUBOID 4 1 44.3 -5.1 2P38.75 2P0.615
 UNIT 17
 COM='PLEXIGLAS SHEET BOTTOM SOUTH REFLECTOR WITH TRIS'
 CUBOID 0 1 2P5.1 2P2.5 2P0.6150
 CUBOID 5 1 44.3 -5.1 2P38.75 2P0.6150
 UNIT 18
 COM='LOWER PORTION SOUTH BOTTOM REFLECTOR WITH TRIS'
 CUBOID 0 1 2P5.1 2P2.5 2P8.855
 CUBOID 5 1 44.3 -5.1 2P38.75 2P8.855
 UNIT 19
 COM='SOUTH BOTTOM REFLECTOR WITH REGULAR AND TRIS'
 ARRAY 4 3*0.0
 UNIT 20
 COM='EAST AND WEST REFLECTORS FOR NORTH REFLECTOR WITH TRIS'
 CUBOID 5 1 2P15.8 2P12.65 2P54.2825
 UNIT 21
 COM='ARRAY FOR EAST AND WEST REFLECTORS FOR NORTH REFLECTOR'
 ARRAY 5 3*0.0
 UNIT 22
 COM='EAST AND WEST REFLECTORS FOR SOUTH REFLECTOR WITH TRIS'
 CUBOID 5 1 2P24.700 2P12.65 2P54.2825

UNIT 23
 COM='ARRAY FOR EAST AND WEST REFLECTORS FOR SOUTH REFLECTOR'
 ARRAY 6 3*0.0
 UNIT 24
 COM='NORTH TOP REFLECTOR WITH TRIS'
 CUBOID 5 1 2P28.35 2P64.05 2P12.15
 UNIT 25
 COM='ARRAY FOR NORTH TOP REFLECTOR'
 ARRAY 7 3*0.0
 UNIT 26
 COM='SOUTH TOP REFLECTOR WITH TRIS'
 CUBOID 0 1 2P5.1 2P2.5 2P12.15
 CUBOID 5 1 69.4 -5.1 2P64.05 2P12.15
 UNIT 27
 COM='ARRAY FOR SOUTH TOP REFLECTOR'
 ARRAY 8 3*0.0
 UNIT 28
 COM='NORTH END REFLECTOR 9.8CM PORTION WITHOUT TRIS'
 CUBOID 4 1 2P4.9000 2P64.0500 2P54.2825
 UNIT 29
 COM='NORTH END REFLECTOR 5.2 CM PORTION WITH TRIS'
 CUBOID 5 1 2P2.6 2P64.0500 2P54.2825
 UNIT 30
 COM='NORTH END REFLECTOR 10.1 CM PORTION WITHOUT TRIS'
 CUBOID 4 1 2P5.05 2P64.05 2P54.2825
 UNIT 31
 COM='ARRAY FOR NORTH END REFLECTOR'
 ARRAY 9 3*0.0
 UNIT 32
 COM='SOUTH END REFLECTOR'
 CUBOID 5 1 2P12.55 2P64.05 2P54.2825
 UNIT 33
 COM='ARRAY FOR SOUTH END REFLECTOR'
 ARRAY 10 3*0.0
 UNIT 38
 COM='NORTH CORE WITH BOTTOM REFLECTOR'
 ARRAY 13 3* 0.0
 UNIT 39
 COM='NORTH CORE WITH EAST AND WEST REFLECTOR'
 ARRAY 14 3*0.0
 UNIT 40
 COM='NORTH CORE WITH END REFLECTOR'
 ARRAY 15 3*0.0
 UNIT 42
 COM='NORTH CORE WITH TOP REFLECTOR'
 ARRAY 16 3*0.0
 UNIT 48
 COM='SOUTH CORE WITH BOTTOM REFLECTORS'
 ARRAY 20 3*0.0
 UNIT 49
 COM='SOUTH CORE WITH EAST WEST REFLECTORS'
 ARRAY 21 3*0.0
 UNIT 50
 COM='SOUTH CORE END REFLECTOR'
 ARRAY 22 3*0.0
 UNIT 52
 COM='SOUTH CORE WITH TOP REFLECTOR'
 ARRAY 23 3*0.0
 UNIT 54
 COM='AIR GAP'
 CUBOID 0 1 0.942 0.0 64.475 -63.625 69.13 -63.735
 GLOBAL
 UNIT 55
 COM='TOTAL'
 ARRAY 25 3*0.0

Table A.3 (continued)

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UNIT 56
COM='COMBINATION OF TWO REGULAR FUEL BOXES'
ARRAY 28 3*0.0
UNIT 57
COM='COMBINATION OF REGULAR FUEL BOX AND SPECIAL FUEL BOX'
ARRAY 29 3*0.0
UNIT 58
COM='COMBINATION OF TWO REGULAR WEIGHT DISTRIBUTION PLATES'
ARRAY 30 3*0.0
UNIT 59
COM='COMBINATION OF REGULAR AND SPECIAL WEIGHT DISTRIBUTION PLATES'
ARRAY 31 3*0.0
UNIT 60
COM='NORTH CORE SOLUTION DRIVER'
CUBOID 8 1 2P7.5 2P14.9 3.710 -7.5
CUBOID 0 1 2P7.5 2P14.9 2P7.5
CUBOID 9 1 2P7.65 2P15.05 2P7.65
CUBOID 0 1 2P7.665 2P15.33 2P7.665
UNIT 61
COM='NORTH CORE SOLUTION DRIVER'
CUBOID 8 1 2P7.5 2P14.9 3.630 -7.5
CUBOID 0 1 2P7.5 2P14.9 2P7.5
CUBOID 9 1 2P7.65 2P15.05 2P7.65
CUBOID 0 1 2P7.665 2P15.33 2P7.665
END GEOMETRY
READ ARRAY
ARA=1 NUX=2 NUY=4 NUZ=9
COM='NORTH SPLIT TABLE CORE'
FILL 2R7 2R56 4R7
      2R35 2R58 4R35
      2R7 2R56 4R7
      2R35 2R58 4R35
      2R7 56 60 4R7
      2R35 2R58 4R35
      2R7 2R56 4R7
      2R35 2R58 4R35
      2R7 2R56 4R7
END FILL
ARA=2 NUX=3 NUY=4 NUZ=9
COM='SOUTH SPLIT TABLE CORE'
FILL 3R7 3R56 6R7
      3R35 3R58 6R35
      3R7 3R56 6R7
      3R35 3R58 6R35
      3R7 61 56 56 6R7
      3R35 3R58 6R35
      3R7 57 56 56 6R7
      3R35 59 58 58 6R35
      3R7 57 56 56 6R7
END FILL
ARA=3 NUX=1 NUY=1 NUZ=3
COM='NORTH BOTTOM REFLECTOR'
FILL 14 11 13 END FILL
ARA=4 NUX=1 NUY=1 NUZ=7
COM='SOUTH BOTTOM REFLECTOR'
FILL 18 16 17 16 17 17 END FILL
ARA=5 NUX=1 NUY=1 NUZ=1
COM='EAST AND WEST WALLS OF NORTH REFLECTOR'
FILL 20 END FILL
ARA=6 NUX=1 NUY=1 NUZ=1
COM='EAST AND WEST WALLS OF SOUTH REFLECTOR'
FILL 22 END FILL
ARA=7 NUX=1 NUY=1 NUZ=1
COM='ARRAY FOR NORTH TOP REFLECTOR'
FILL 24 END FILL

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ARA=8 NUX=1 NUY=1 NUZ=1
COM='ARRAY FOR SOUTH TOP REFLECTOR'
FILL 26 END FILL
ARA=9 NUX=3 NUY=1 NUZ=1
COM='ARRAY FOR NORTH END REFLECTOR'
FILL 28 29 30 END FILL
ARA=10 NUX=1 NUY=1 NUZ=1
COM='ARRAY FOR SOUTH END REFLECTOR'
FILL 32 END FILL
ARA=13 NUX=1 NUY=1 NUZ=2
COM='COMBINATION OF NORTH CORE WITH BOTTOM REFLECTOR'
FILL 15 9 END FILL
ARA=14 NUX=1 NUY=3 NUZ=1
COM='NORTH CORE WITH SIDE REFLECTORS'
FILL 21 38 21 END FILL
ARA=15 NUX=2 NUY=1 NUZ=1
COM='NORTH CORE WITH END REFLECTOR'
FILL 31 39 END FILL
ARA=16 NUX=1 NUY=1 NUZ=2
COM='NORTH CORE WITH TOP REFLECTOR'
FILL 40 25 END FILL
ARA=20 NUX=1 NUY=1 NUZ=2
COM='SOUTH CORE WITH BOTTOM REFLECTOR'
FILL 19 10 END FILL
ARA=21 NUX=1 NUY=3 NUZ=1
COM='SOUTH CORE WITH EAST WEST REFLECTORS'
FILL 23 48 23 END FILL
ARA=22 NUX=2 NUY=1 NUZ=1
COM='SOUTH CORE WITH END REFLECTOR'
FILL 49 33 END FILL
ARA=23 NUX=1 NUY=1 NUZ=2
COM='COMBINATION OF CORE WITH TOP REFLECTOR'
FILL 50 27 END FILL
ARA=25 NUX=3 NUY=1 NUZ=1
COM='TOTAL'
FILL 42 54 52 END FILL
ARA=26 NUX=3 NUY=1 NUZ=1
COM='ASSEMBLY OF FUEL BOX FRONT AND REAR'
FILL 2 1 3 END FILL
ARA=27 NUX=1 NUY=1 NUZ=3
COM='ASSEMBLY OF FUEL BOX TOP AND BOTTOM'
FILL 5 4 5 END FILL
ARA=28 NUX=1 NUY=2 NUZ=1
COM='COMBINATION OF TWO FUEL BOXES'
FILL 7 7 END FILL
ARA=29 NUX=1 NUY=2 NUZ=1
COM='COMBINATION OF SPECIAL AND REGULAR FUEL BOXES'
FILL 7 6 END FILL
ARA=30 NUX=1 NUY=2 NUZ=1
COM='COMBINATION OF TWO WEIGHT DISTRIBUTION PLATES'
FILL 35 35 END FILL
ARA=31 NUX=1 NUY=2 NUZ=1
COM='COMBINATION OF SPECIAL AND REGULAR WEIGHT DISTRIBUTION PLATES'
FILL 35 34 END FILL
END ARRAY
READ PLOT TTL='YZ SLICE OF SOUTH CORE FIRST ROW'
XUL=64.319 YUL=40.000 ZUL=72.000
XLR=64.319 YLR=72.000 ZLR=56.000
VAX=1 WDN=-1 NAX=130 NCH='012345678'END
TTL='XZ SLICE OF SPHERE CUBOID'
XUL=56.0 YUL=63.625 ZUL=71.735
XLR=72.0 YLR=63.625 ZLR=55.735
UAX=1 WDN=-1 NAX=130 NCH='012345678'
END PLOT

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Table A.3 (continued)

READ START NST=1 XSM=41.37 XSP=72.894 YSM=40.63 YSP=71.29
 ZSM=56.071 ZSP=71.4 END START
 END DATA
 END

CAR08
 =CSAS25
 ROCKY FLATS CRITICALS NUREG/CR-0674 EXPERIMENT NUMBER ? (27 GROUP MODEL)
 ' FUEL CUBE 15.28 CM, U(4.46)308 @ H/U=0.77, LOW CONC. SOLUTION DRIVEN
 27GROUPNDF4 INFHOMMEDIUM
 U308 1 5.4078E-1 293.0 92234 0.03 92235 4.46 92236 0.08 92238 95.43 END
 H2O 1 8.9514E-2 END
 ARBM-BAGGIE 1.0 3 0 0 0 1001 14.01 6012 84.9 8016 1.20 1 1.9134E-2
 END
 ARBM-AL1100 1.0 3 0 0 1 13027 99.18 26000 0.5 29000 0.2 2 9.5390E-1
 END
 ARBM-TAPE(VINYL) 1.0 7 0 0 0 1001 5.92 6012 45.91 8016 10.82 17000
 25.73 20040 6.9 22000 1.6 82000 1.1 2 1.1115E-2 END
 ARBM-TAPE(MYLAR) 1.0 3 0 0 0 1001 6.83 6012 65.50 8016 27.02 2
 1.7491E-2 END
 ARBM-MODERATOR 1.185 3 0 0 0 1001 7.83 6012 59.49 8016 32.48 3 END
 ARBM-PLEX(REG) 1.0 3 0 0 0 1001 7.84 6012 59.59 8016 32.23 4
 1.1773 END
 ARBM-PLEX(PAPER) 1.0 3 0 0 0 1001 6.48 6012 42.17 8016 49.5 4
 3.7534E-3 END
 ARBM-PLEX(GLUE) 1.0 3 0 0 0 1001 11.67 6012 86.29 8016 1.20 4
 1.1648E-3 END
 ARBM-PLEX(TRIS) 1.0 8 0 0 1 1001 7.16 6012 52.03 7014 0.16 8016 29.82
 15031 1.02 17000 1.81 35079 4.260 35081 2.840 5 1.2757 END
 ARBM-PLEX(PAPER) 1.0 3 0 0 0 1001 6.48 6012 42.17 8016 49.5 5
 3.7534E-3 END
 ARBM-PLEX(GLUE) 1.0 3 0 0 0 1001 11.67 6012 86.29 8016 1.20 5
 1.1648E-3 END
 ARBM-FILLER 1.185 3 0 0 0 1001 7.83 6012 59.49 8016 32.48 6 0.7 END
 ' THIS MATERIAL IS ACTUALLY MODERATOR ADJUSTED FOR THE VOLUME
 ' FRACTION OF THE VOID FILLED BETWEEN CORE AND REFLECTOR.
 ARBM-AL1100 1.0 3 0 0 1 13027 99.18 26000 0.5 29000 0.2 7 2.715 END
 SOLNUO2(NO3)2 8 86.42 0.149 1.0 293.0 92234 1.022 92235 93.172
 92236 0.434 92238 5.372 END
 SS304 9 1.0 END
 END COMP
 ROCKY FLATS CRITICALS NUREG/CR-0674 EXPERIMENT NUMBER ? (27 GROUP MODEL)
 ' FUEL CUBE 15.28 CM, U(4.46)308 @ H/U=0.77, LOW CONC. SOLUTION DRIVEN
 READ PARM NPG=600 NUB=YES PDN=YES PLT=NO END PARM
 READ GEOM
 UNIT 1
 COM='FUEL BOX WITH VOID AND PART OF AL BOX'
 CUBOID 0 1 9.80 0.0 3.75 0.0 14.98 0.0
 CUBOID 2 1 9.95 0.0 3.90 -0.15 14.98 0.0
 CUBOID 1 1 14.98 0.0 9.365 -5.615 14.98 0.0
 UNIT 2
 COM='FRONT OF FUEL BOX'
 CUBOID 2 1 0.15 0.0 5.615 0.0 14.98 0.0
 CUBOID 0 1 0.15 0.0 9.365 0.0 14.98 0.0
 CUBOID 2 1 0.15 0.0 14.98 0.0 14.98 0.0
 UNIT 3
 COM='REAR OF FUEL BOX'
 CUBOID 2 1 0.15 0.0 14.98 0.0 14.98 0.0

UNIT 4
 COM='ARRAY TO ASSEMBLE PART OF BOX'
 ARRAY 26 3*0
 UNIT 5
 COM='TOP AND BOTTOM OF BOX'
 CUBOID 0 1 9.80 0.0 3.750 0.0 0.15 0.0
 CUBOID 2 1 15.28 0.0 9.365 -5.615 0.15 0.0
 GLOBAL
 UNIT 6
 COM='ARRAY TO ASSEMBLE TOP AND BOTTOM'
 ARRAY 27 3*0
 CUBOID 2 1 15.28 0.0 15.13 -0.15 15.28 0.0
 CUBOID 0 1 15.305 -0.025 15.155 -0.175 15.305 -0.025
 UNIT 7
 COM='FUEL BOX 15.28 CM ON A SIDE WITH .15 CM WALLS .05CM STACKING VOID'
 CUBOID 1 1 6P7.49
 CUBOID 2 1 6P7.64
 CUBOID 0 1 6P7.6650
 UNIT 34
 COM='ALUMINUM WEIGHT DISTRIBUTION PLATE FOR SPECIAL BOX'
 CUBOID 0 1 9.80 0.0 3.750 0.0 0.16 0.0
 CUBOID 7 1 15.33 0.0 9.54 -5.79 0.16 0.0
 UNIT 35
 COM='ALUMINUM WEIGHT DISTRIBUTION PLATE FOR BOXES'
 CUBOID 7 1 4P7.665 0.16 0.0
 UNIT 9
 COM='NORTH SPLIT TABLE CORE'
 ARRAY 1 3*0.0
 CUBOID 0 1 30.66 -0.94 77.5 0.0 83.475 0.0
 UNIT 10
 COM='SOUTH SPLIT TABLE CORE'
 ARRAY 2 3*0.0
 CUBOID 0 1 49.4 0.0 77.5 0.0 83.475 0.0
 UNIT 11
 COM='PLEXIGLASS REFLECTOR SHEET WITHOUT TRIS, NORTH BOTTOM REFLECTOR'
 CUBOID 4 1 2P15.8000 2P38.7500 2P0.6150
 UNIT 12
 COM='PLEXIGLASS REFLECTOR SHEET WITH TRIS, NORTH BOTTOM REFLECTOR'
 CUBOID 5 1 2P15.8000 2P38.7500 2P0.6150
 UNIT 13
 COM='UPPER PORTION NORTH BOTTOM REFLECTOR WITH TRIS'
 CUBOID 5 1 2P15.8 2P38.75 2P8.24
 UNIT 14
 COM='LOWER PORTION NORTH BOTTOM REFLECTOR WITH TRIS'
 CUBOID 5 1 2P15.8 2P38.75 2P3.69
 UNIT 15
 COM='NORTH BOTTOM REFLECTOR INCLUDES REGULAR AND TRIS'
 ARRAY 3 3*0.0
 UNIT 16
 COM='PLEXIGLAS SHEET BOTTOM SOUTH REFLECTOR WITHOUT TRIS'
 CUBOID 0 1 2P5.1 2P2.5 2P0.6150
 CUBOID 4 1 44.3 -5.1 2P38.75 2P0.615
 UNIT 17
 COM='PLEXIGLAS SHEET BOTTOM SOUTH REFLECTOR WITH TRIS'
 CUBOID 0 1 2P5.1 2P2.5 2P0.6150
 CUBOID 5 1 44.3 -5.1 2P38.75 2P0.6150
 UNIT 18
 COM='LOWER PORTION SOUTH BOTTOM REFLECTOR WITH TRIS'
 CUBOID 0 1 2P5.1 2P2.5 2P8.855
 CUBOID 5 1 44.3 -5.1 2P38.75 2P8.855
 UNIT 19
 COM='SOUTH BOTTOM REFLECTOR WITH REGULAR AND TRIS'
 ARRAY 4 3*0.0

Table A.3 (continued)

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UNIT 20
COM='EAST AND WEST REFLECTORS FOR NORTH REFLECTOR WITH TRIS'
CUBOID 5 1 2P15.8 2P12.65 2P54.2825
UNIT 21
COM='ARRAY FOR EAST AND WEST REFLECTORS FOR NORTH REFLECTOR'
ARRAY 5 3*0.0
UNIT 22
COM='EAST AND WEST REFLECTORS FOR SOUTH REFLECTOR WITH TRIS'
CUBOID 5 1 2P24.700 2P12.65 2P54.2825
UNIT 23
COM='ARRAY FOR EAST AND WEST REFLECTORS FOR SOUTH REFLECTOR'
ARRAY 6 3*0.0
UNIT 24
COM='NORTH TOP REFLECTOR WITH TRIS'
CUBOID 5 1 2P28.35 2P64.05 2P12.15
UNIT 25
COM='ARRAY FOR NORTH TOP REFLECTOR'
ARRAY 7 3*0.0
UNIT 26
COM='SOUTH TOP REFLECTOR WITH TRIS'
CUBOID 0 1 2P5.1 2P2.5 2P12.15
CUBOID 5 1 69.4 -5.1 2P64.05 2P12.15
UNIT 27
COM='ARRAY FOR SOUTH TOP REFLECTOR'
ARRAY 8 3*0.0
UNIT 28
COM='NORTH END REFLECTOR 9.8CM PORTION WITHOUT TRIS'
CUBOID 4 1 2P4.9000 2P64.0500 2P54.2825
UNIT 29
COM='NORTH END REFLECTOR 5.2 CM PORTION WITH TRIS'
CUBOID 5 1 2P2.6 2P64.0500 2P54.2825
UNIT 30
COM='NORTH END REFLECTOR 10.1 CM PORTION WITHOUT TRIS'
CUBOID 4 1 2P5.05 2P64.05 2P54.2825
UNIT 31
COM='ARRAY FOR NORTH END REFLECTOR'
ARRAY 9 3*0.0
UNIT 32
COM='SOUTH END REFLECTOR'
CUBOID 5 1 2P12.55 2P64.05 2P54.2825
UNIT 33
COM='ARRAY FOR SOUTH END REFLECTOR'
ARRAY 10 3*0.0
UNIT 38
COM='NORTH CORE WITH BOTTOM REFLECTOR'
ARRAY 13 3* 0.0
UNIT 39
COM='NORTH CORE WITH EAST AND WEST REFLECTOR'
ARRAY 14 3*0.0
UNIT 40
COM='NORTH CORE WITH END REFLECTOR'
ARRAY 15 3*0.0
UNIT 42
COM='NORTH CORE WITH TOP REFLECTOR'
ARRAY 16 3*0.0
UNIT 48
COM='SOUTH CORE WITH BOTTOM REFLECTORS'
ARRAY 20 3*0.0
UNIT 49
COM='SOUTH CORE WITH EAST WEST REFLECTORS'
ARRAY 21 3*0.0

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UNIT 50
COM='SOUTH CORE END REFLECTOR'
ARRAY 22 3*0.0
UNIT 52
COM='SOUTH CORE WITH TOP REFLECTOR'
ARRAY 23 3*0.0
UNIT 54
COM='AIR GAP'
CUBOID 0 1 0.912 0.0 64.475 -63.625 69.13 -63.735
GLOBAL
UNIT 55
COM='TOTAL'
ARRAY 25 3*0.0
UNIT 56
COM='COMBINATION OF TWO REGULAR FUEL BOXES'
ARRAY 28 3*0.0
UNIT 57
COM='COMBINATION OF REGULAR FUEL BOX AND SPECIAL FUEL BOX'
ARRAY 29 3*0.0
UNIT 58
COM='COMBINATION OF TWO REGULAR WEIGHT DISTRIBUTION PLATES'
ARRAY 30 3*0.0
UNIT 59
COM='COMBINATION OF REGULAR AND SPECIAL WEIGHT DISTRIBUTION PLATES'
ARRAY 31 3*0.0
UNIT 60
COM='NORTH CORE SOLUTION DRIVER'
CUBOID 8 1 2P7.5 2P14.9 5.374 -7.5
CUBOID 0 1 2P7.5 2P14.9 2P7.5
CUBOID 9 1 2P7.65 2P15.05 2P7.65
CUBOID 0 1 2P7.665 2P15.33 2P7.665
UNIT 61
COM='NORTH CORE SOLUTION DRIVER'
CUBOID 8 1 2P7.5 2P14.9 5.328 -7.5
CUBOID 0 1 2P7.5 2P14.9 2P7.5
CUBOID 9 1 2P7.65 2P15.05 2P7.65
CUBOID 0 1 2P7.665 2P15.33 2P7.665
END GEOMETRY
READ ARRAY
ARA=1 NUX=2 NUY=4 NUZ=9
COM='NORTH SPLIT TABLE CORE'
FILL 2R7 2R56 4R7
      2R35 2R58 4R35
      2R7 2R56 4R7
      2R35 2R58 4R35
      2R7 56 60 4R7
      2R35 2R58 4R35
      2R7 2R56 4R7
      2R35 2R58 4R35
      2R7 2R56 4R7
END FILL
ARA=2 NUX=3 NUY=4 NUZ=9
COM='SOUTH SPLIT TABLE CORE'
FILL 3R7 3R56 6R7
      3R35 3R58 6R35
      3R7 3R56 6R7
      3R35 3R58 6R35
      3R7 61 56 56 6R7
      3R35 3R58 6R35
      3R7 57 56 56 6R7
      3R35 59 58 58 6R35
      3R7 57 56 56 6R7
END FILL

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Table A.3 (continued)

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ARA=3  NUX=1  NUY=1  NUZ=3
COM='NORTH BOTTOM REFLECTOR'
FILL 14 11 13  END FILL
ARA=4  NUX=1  NUY=1  NUZ=7
COM='SOUTH BOTTOM REFLECTOR'
FILL 18 16 17 16 17 17  END FILL
ARA=5  NUX=1  NUY=1  NUZ=1
COM='EAST AND WEST WALLS OF NORTH REFLECTOR'
FILL 20  END FILL
ARA=6  NUX=1  NUY=1  NUZ=1
COM='EAST AND WEST WALLS OF SOUTH REFLECTOR'
FILL 22  END FILL
ARA=7  NUX=1  NUY=1  NUZ=1
COM='ARRAY FOR NORTH TOP REFLECTOR'
FILL 24  END FILL
ARA=8  NUX=1  NUY=1  NUZ=1
COM='ARRAY FOR SOUTH TOP REFLECTOR'
FILL 26  END FILL
ARA=9  NUX=3  NUY=1  NUZ=1
COM='ARRAY FOR NORTH END REFLECTOR'
FILL 28 29 30  END FILL
ARA=10 NUX=1  NUY=1  NUZ=1
COM='ARRAY FOR SOUTH END REFLECTOR'
FILL 32  END FILL
ARA=13 NUX=1  NUY=1  NUZ=2
COM='COMBINATION OF NORTH CORE WITH BOTTOM REFLECTOR'
FILL 15 9  END FILL
ARA=14 NUX=1  NUY=3  NUZ=1
COM='NORTH CORE WITH SIDE REFLECTORS'
FILL 21 38 21  END FILL
ARA=15 NUX=2  NUY=1  NUZ=1
COM='NORTH CORE WITH END REFLECTOR'
FILL 31 39  END FILL
ARA=16 NUX=1  NUY=1  NUZ=2
COM='NORTH CORE WITH TOP REFLECTOR'
FILL 40 25  END FILL
ARA=20 NUX=1  NUY=1  NUZ=2
COM='SOUTH CORE WITH BOTTOM REFLECTOR'
FILL 19 10  END FILL
ARA=21 NUX=1  NUY=3  NUZ=1
COM='SOUTH CORE WITH EAST WEST REFLECTORS'
FILL 23 48 23  END FILL
ARA=22 NUX=2  NUY=1  NUZ=1
COM='SOUTH CORE WITH END REFLECTOR'
FILL 49 33  END FILL
ARA=23 NUX=1  NUY=1  NUZ=2
COM='COMBINATION OF CORE WITH TOP REFLECTOR'
FILL 50 27  END FILL
ARA=25 NUX=3  NUY=1  NUZ=1
COM='TOTAL'
FILL 42 54 52  END FILL
ARA=26 NUX=3  NUY=1  NUZ=1
COM='ASSEMBLY OF FUEL BOX FRONT AND REAR'
FILL 2 1 3  END FILL
ARA=27 NUX=1  NUY=1  NUZ=3
COM='ASSEMBLY OF FUEL BOX TOP AND BOTTOM'
FILL 5 4 5  END FILL
ARA=28 NUX=1  NUY=2  NUZ=1
COM='COMBINATION OF TWO FUEL BOXES'
FILL 7 7  END FILL
ARA=29 NUX=1  NUY=2  NUZ=1
COM='COMBINATION OF SPECIAL AND REGULAR FUEL BOXES'
FILL 7 6  END FILL

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ARA=30 NUX=1  NUY=2  NUZ=1
COM='COMBINATION OF TWO WEIGHT DISTRIBUTION PLATES'
FILL 35 35  END FILL
ARA=31 NUX=1  NUY=2  NUZ=1
COM='COMBINATION OF SPECIAL AND REGULAR WEIGHT DISTRIBUTION PLATES'
FILL 35 34  END FILL
END ARRAY
READ PLOT TTL='YZ SLICE OF SOUTH CORE FIRST ROW'
XUL=64.319 YUL=40.000 ZUL=72.000
XLR=64.319 YLR=72.000 ZLR=56.000
VAX=1  WDN=-1  NAX=130  NCH='012345678' END
TTL='XZ SLICE OF SPHERE CUBOID'
XUL=56.0 YUL=63.625 ZUL=71.735
XLR=72.0 YLR=63.625 ZLR=55.735
UAX=1  WDN=-1  NAX=130  NCH='012345678'
END PLOT
READ START NST=1 XSM=41.37 XSP=72.894 YSM=40.63 YSP=71.29
ZSM=56.071 ZSP=71.4  END START
END DATA
END

```

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CAR09
=CSAS25
ROCKY FLATS CRITICALS NUREG/CR-0674 EXPERIMENT NUMBER 2 (27 GROUP MODEL)
' FUEL CUBE 15.28 CM, U(4.46)308 @ H/U=0.77, LOW CONC. SOLUTION DRIVEN
27GROUPNDF4 INFHOMMEDIUM
U308 1 5.4078E-1 293.0 92234 0.03 92235 4.46 92236 0.08 92238 95.43 END
H2O 1 8.9514E-2 END
ARBM-BAGGIE 1.0 3 0 0 0 1001 14.01 6012 84.9 8016 1.20 1 1.9134E-2
END
ARBM-AL1100 1.0 3 0 0 1 13027 99.18 26000 0.5 29000 0.2 2 9.5390E-1
END
ARBM-TAPE(VINYL) 1.0 7 0 0 0 1001 5.92 6012 45.91 8016 10.82 17000
25.73 20040 6.9 22000 1.6 82000 1.1 2 1.1115E-2 END
ARBM-TAPE(MYLAR) 1.0 3 0 0 0 1001 6.83 6012 65.50 8016 27.02 2
1.7491E-2 END
ARBM-MODERATOR 1.185 3 0 0 0 1001 7.83 6012 59.49 8016 32.48 3 END
ARBM-PLEX(REG) 1.0 3 0 0 0 1001 7.84 6012 59.59 8016 32.23 4
1.1773 END
ARBM-PLEX(PAPER) 1.0 3 0 0 0 1001 6.48 6012 42.17 8016 49.5 4
3.7534E-3 END
ARBM-PLEX(GLUE) 1.0 3 0 0 0 1001 11.67 6012 86.29 8016 1.20 4
1.1648E-3 END
ARBM-PLEX(TRIS) 1.0 8 0 0 1 1001 7.16 6012 52.03 7014 0.16 8016 29.82
15031 1.02 17000 1.81 35079 4.260 35081 2.840 5 1.2757 END
ARBM-PLEX(PAPER) 1.0 3 0 0 0 1001 6.48 6012 42.17 8016 49.5 5
3.7534E-3 END
ARBM-PLEX(GLUE) 1.0 3 0 0 0 1001 11.67 6012 86.29 8016 1.20 5
1.1648E-3 END
ARBM-FILLER 1.185 3 0 0 0 1001 7.83 6012 59.49 8016 32.48 6 0.7 END
' THIS MATERIAL IS ACTUALLY MODERATOR ADJUSTED FOR THE VOLUME
' FRACTION OF THE VOID FILLED BETWEEN CORE AND REFLECTOR.
ARBM-AL1100 1.0 3 0 0 1 13027 99.18 26000 0.5 29000 0.2 7 2.715 END
SOLNUO2(NO3)2 8 86.42 0.149 1.0 293.0 92234 1.022 92235 93.172
92236 0.434 92238 5.372 END
SS304 9 1.0 END
END COMP
ROCKY FLATS CRITICALS NUREG/CR-0674 EXPERIMENT NUMBER 2 (27 GROUP MODEL)
' FUEL CUBE 15.28 CM, U(4.46)308 @ H/U=0.77, LOW CONC. SOLUTION DRIVEN
READ PARM NPG=600 NUB=YES FDN=YES PLT=NO END PARM
READ GEOM

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Table A.3 (continued)

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UNIT 1
COM='FUEL BOX WITH VOID AND PART OF AL BOX'
CUBOID 0 1 9.80 0.0 3.75 0.0 14.98 0.0
CUBOID 2 1 9.95 0.0 3.90 -0.15 14.98 0.0
CUBOID 1 1 14.98 0.0 9.365 -5.615 14.98 0.0
UNIT 2
COM='FRONT OF FUEL BOX'
CUBOID 2 1 0.15 0.0 5.615 0.0 14.98 0.0
CUBOID 0 1 0.15 0.0 9.365 0.0 14.98 0.0
CUBOID 2 1 0.15 0.0 14.98 0.0 14.98 0.0
UNIT 3
COM='REAR OF FUEL BOX'
CUBOID 2 1 0.15 0.0 14.98 0.0 14.98 0.0
UNIT 4
COM='ARRAY TO ASSEMBLE PART OF BOX'
ARRAY 26 3*0
UNIT 5
COM='TOP AND BOTTOM OF BOX'
CUBOID 0 1 9.80 0.0 3.750 0.0 0.15 0.0
CUBOID 2 1 15.28 0.0 9.365 -5.615 0.15 0.0
GLOBAL
UNIT 6
COM='ARRAY TO ASSEMBLE TOP AND BOTTOM'
ARRAY 27 3*0
CUBOID 2 1 15.28 0.0 15.13 -0.15 15.28 0.0
CUBOID 0 1 15.305 -0.025 15.155 -0.175 15.305 -0.025
UNIT 7
COM='FUEL BOX 15.28 CM ON A SIDE WITH .15 CM WALLS .05CM STACKING VOID'
CUBOID 1 1 6P7.49
CUBOID 2 1 6P7.64
CUBOID 0 1 6P7.6650
UNIT 34
COM='ALUMINUM WEIGHT DISTRIBUTION PLATE FOR SPECIAL BOX'
CUBOID 0 1 9.80 0.0 3.750 0.0 0.16 0.0
CUBOID 7 1 15.33 0.0 9.54 -5.79 0.16 0.0
UNIT 35
COM='ALUMINUM WEIGHT DISTRIBUTION PLATE FOR BOXES'
CUBOID 7 1 4P7.665 0.16 0.0
UNIT 9
COM='NORTH SPLIT TABLE CORE'
ARRAY 1 3*0.0
CUBOID 0 1 30.66 -0.94 77.5 0.0 83.475 0.0
UNIT 10
COM='SOUTH SPLIT TABLE CORE'
ARRAY 2 3*0.0
CUBOID 0 1 49.4 0.0 77.5 0.0 83.475 0.0
UNIT 11
COM='PLEXIGLASS REFLECTOR SHEET WITHOUT TRIS, NORTH BOTTOM REFLECTOR'
CUBOID 4 1 2P15.8000 2P38.7500 2P0.6150
UNIT 12
COM='PLEXIGLASS REFLECTOR SHEET WITH TRIS, NORTH BOTTOM REFLECTOR'
CUBOID 5 1 2P15.8000 2P38.7500 2P0.6150
UNIT 13
COM='UPPER PORTION NORTH BOTTOM REFLECTOR WITH TRIS'
CUBOID 5 1 2P15.8 2P38.75 2P8.24
UNIT 14
COM='LOWER PORTION NORTH BOTTOM REFLECTOR WITH TRIS'
CUBOID 5 1 2P15.8 2P38.75 2P3.69
UNIT 15
COM='NORTH BOTTOM REFLECTOR INCLUDES REGULAR AND TRIS'
ARRAY 3 3*0.0

UNIT 16
COM='PLEXIGLAS SHEET BOTTOM SOUTH REFLECTOR WITHOUT TRIS'
CUBOID 0 1 2P5.1 2P2.5 2P0.6150
CUBOID 4 1 44.3 -5.1 2P38.75 2P0.615
UNIT 17
COM='PLEXIGLAS SHEET BOTTOM SOUTH REFLECTOR WITH TRIS'
CUBOID 0 1 2P5.1 2P2.5 2P0.6150
CUBOID 5 1 44.3 -5.1 2P38.75 2P0.6150
UNIT 18
COM='LOWER PORTION SOUTH BOTTOM REFLECTOR WITH TRIS'
CUBOID 0 1 2P5.1 2P2.5 2P8.855
CUBOID 5 1 44.3 -5.1 2P38.75 2P8.855
UNIT 19
COM='SOUTH BOTTOM REFLECTOR WITH REGULAR AND TRIS'
ARRAY 4 3*0.0
UNIT 20
COM='EAST AND WEST REFLECTORS FOR NORTH REFLECTOR WITH TRIS'
CUBOID 5 1 2P15.8 2P12.65 2P54.2825
UNIT 21
COM='ARRAY FOR EAST AND WEST REFLECTORS FOR NORTH REFLECTOR'
ARRAY 5 3*0.0
UNIT 22
COM='EAST AND WEST REFLECTORS FOR SOUTH REFLECTOR WITH TRIS'
CUBOID 5 1 2P24.700 2P12.65 2P54.2825
UNIT 23
COM='ARRAY FOR EAST AND WEST REFLECTORS FOR SOUTH REFLECTOR'
ARRAY 6 3*0.0
UNIT 24
COM='NORTH TOP REFLECTOR WITH TRIS'
CUBOID 5 1 2P28.35 2P64.05 2P12.15
UNIT 25
COM='ARRAY FOR NORTH TOP REFLECTOR'
ARRAY 7 3*0.0
UNIT 26
COM='SOUTH TOP REFLECTOR WITH TRIS'
CUBOID 0 1 2P5.1 2P2.5 2P12.15
CUBOID 5 1 69.4 -5.1 2P64.05 2P12.15
UNIT 27
COM='ARRAY FOR SOUTH TOP REFLECTOR'
ARRAY 8 3*0.0
UNIT 28
COM='NORTH END REFLECTOR 9.8CM PORTION WITHOUT TRIS'
CUBOID 4 1 2P4.9000 2P64.0500 2P54.2825
UNIT 29
COM='NORTH END REFLECTOR 5.2 CM PORTION WITH TRIS'
CUBOID 5 1 2P2.6 2P64.0500 2P54.2825
UNIT 30
COM='NORTH END REFLECTOR 10.1 CM PORTION WITHOUT TRIS'
CUBOID 4 1 2P5.05 2P64.05 2P54.2825
UNIT 31
COM='ARRAY FOR NORTH END REFLECTOR'
ARRAY 9 3*0.0
UNIT 32
COM='SOUTH END REFLECTOR'
CUBOID 5 1 2P12.55 2P64.05 2P54.2825
UNIT 33
COM='ARRAY FOR SOUTH END REFLECTOR'
ARRAY 10 3*0.0
UNIT 38
COM='NORTH CORE WITH BOTTOM REFLECTOR'
ARRAY 13 3* 0.0
UNIT 39
COM='NORTH CORE WITH EAST AND WEST REFLECTOR'
ARRAY 14 3*0.0

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Table A.3 (continued)

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UNIT 40
COM='NORTH CORE WITH END REFLECTOR'
ARRAY 15 3*0.0
UNIT 42
COM='NORTH CORE WITH TOP REFLECTOR'
ARRAY 16 3*0.0
UNIT 48
COM='SOUTH CORE WITH BOTTOM REFLECTORS'
ARRAY 20 3*0.0
UNIT 49
COM='SOUTH CORE WITH EAST WEST REFLECTORS'
ARRAY 21 3*0.0
UNIT 50
COM='SOUTH CORE END REFLECTOR'
ARRAY 22 3*0.0
UNIT 52
COM='SOUTH CORE WITH TOP REFLECTOR'
ARRAY 23 3*0.0
UNIT 54
COM='AIR GAP'
CUBOID 0 1 1.117 0.0 64.475 -63.625 69.13 -63.735
GLOBAL
UNIT 55
COM='TOTAL'
ARRAY 25 3*0.0
UNIT 56
COM='COMBINATION OF TWO REGULAR FUEL BOXES'
ARRAY 28 3*0.0
UNIT 57
COM='COMBINATION OF REGULAR FUEL BOX AND SPECIAL FUEL BOX'
ARRAY 29 3*0.0
UNIT 58
COM='COMBINATION OF TWO REGULAR WEIGHT DISTRIBUTION PLATES'
ARRAY 30 3*0.0
UNIT 59
COM='COMBINATION OF REGULAR AND SPECIAL WEIGHT DISTRIBUTION PLATES'
ARRAY 31 3*0.0
UNIT 60
COM='NORTH CORE SOLUTION DRIVER'
CUBOID 8 1 2P7.5 2P14.9 5.499 -7.5
CUBOID 0 1 2P7.5 2P14.9 2P7.5
CUBOID 9 1 2P7.65 2P15.05 2P7.65
CUBOID 0 1 2P7.665 2P15.33 2P7.665
UNIT 61
COM='NORTH CORE SOLUTION DRIVER'
CUBOID 8 1 2P7.5 2P14.9 5.445 -7.5
CUBOID 0 1 2P7.5 2P14.9 2P7.5
CUBOID 9 1 2P7.65 2P15.05 2P7.65
CUBOID 0 1 2P7.665 2P15.33 2P7.665
END GEOMETRY
READ ARRAY
ARA=1 NUX=2 NUY=4 NUZ=9
COM='NORTH SPLIT TABLE CORE'
FILL 2R7 2R56 4R7
      2R35 2R58 4R35
      2R7 2R56 4R7
      2R35 2R58 4R35
      2R7 56 60 4R7
      2R35 2R58 4R35
      2R7 2R56 4R7
      2R35 2R58 4R35
      2R7 2R56 4R7
END FILL

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ARA=2 NUX=3 NUY=4 NUZ=9
COM='SOUTH SPLIT TABLE CORE'
FILL 3R7 3R56 6R7
      3R35 3R58 6R35
      3R7 3R56 6R7
      3R35 3R58 6R35
      3R7 61 56 56 6R7
      3R35 3R58 6R35
      3R7 57 56 56 6R7
      3R35 59 58 58 6R35
      3R7 57 56 56 6R7
END FILL
ARA=3 NUX=1 NUY=1 NUZ=3
COM='NORTH BOTTOM REFLECTOR'
FILL 14 11 13 END FILL
ARA=4 NUX=1 NUY=1 NUZ=7
COM='SOUTH BOTTOM REFLECTOR'
FILL 18 16 17 16 16 17 17 END FILL
ARA=5 NUX=1 NUY=1 NUZ=1
COM='EAST AND WEST WALLS OF NORTH REFLECTOR'
FILL 20 END FILL
ARA=6 NUX=1 NUY=1 NUZ=1
COM='EAST AND WEST WALLS OF SOUTH REFLECTOR'
FILL 22 END FILL
ARA=7 NUX=1 NUY=1 NUZ=1
COM='ARRAY FOR NORTH TOP REFLECTOR'
FILL 24 END FILL
ARA=8 NUX=1 NUY=1 NUZ=1
COM='ARRAY FOR SOUTH TOP REFLECTOR'
FILL 26 END FILL
ARA=9 NUX=3 NUY=1 NUZ=1
COM='ARRAY FOR NORTH END REFLECTOR'
FILL 28 29 30 END FILL
ARA=10 NUX=1 NUY=1 NUZ=1
COM='ARRAY FOR SOUTH END REFLECTOR'
FILL 32 END FILL
ARA=13 NUX=1 NUY=1 NUZ=2
COM='COMBINATION OF NORTH CORE WITH BOTTOM REFLECTOR'
FILL 15 9 END FILL
ARA=14 NUX=1 NUY=3 NUZ=1
COM='NORTH CORE WITH SIDE REFLECTORS'
FILL 21 38 21 END FILL
ARA=15 NUX=2 NUY=1 NUZ=1
COM='NORTH CORE WITH END REFLECTOR'
FILL 31 39 END FILL
ARA=16 NUX=1 NUY=1 NUZ=2
COM='NORTH CORE WITH TOP REFLECTOR'
FILL 40 25 END FILL
ARA=20 NUX=1 NUY=1 NUZ=2
COM='SOUTH CORE WITH BOTTOM REFLECTOR'
FILL 19 10 END FILL
ARA=21 NUX=1 NUY=3 NUZ=1
COM='SOUTH CORE WITH EAST WEST REFLECTORS'
FILL 23 48 23 END FILL
ARA=22 NUX=2 NUY=1 NUZ=1
COM='SOUTH CORE WITH END REFLECTOR'
FILL 49 33 END FILL
ARA=23 NUX=1 NUY=1 NUZ=2
COM='COMBINATION OF CORE WITH TOP REFLECTOR'
FILL 50 27 END FILL
ARA=25 NUX=3 NUY=1 NUZ=1
COM='TOTAL'
FILL 42 54 52 END FILL

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Table A.3 (continued)

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ARA=26 NUX=3 NUY=1 NUZ=1
COM='ASSEMBLY OF FUEL BOX FRONT AND REAR'
FILL 2 1 3 END FILL
ARA=27 NUX=1 NUY=1 NUZ=3
COM='ASSEMBLY OF FUEL BOX TOP AND BOTTOM'
FILL 5 4 5 END FILL
ARA=28 NUX=1 NUY=2 NUZ=1
COM='COMBINATION OF TWO FUEL BOXES'
FILL 7 7 END FILL
ARA=29 NUX=1 NUY=2 NUZ=1
COM='COMBINATION OF SPECIAL AND REGULAR FUEL BOXES'
FILL 7 6 END FILL
ARA=30 NUX=1 NUY=2 NUZ=1
COM='COMBINATION OF TWO WEIGHT DISTRIBUTION PLATES'
FILL 35 35 END FILL
ARA=31 NUX=1 NUY=2 NUZ=1
COM='COMBINATION OF SPECIAL AND REGULAR WEIGHT DISTRIBUTION PLATES'
FILL 35 34 END FILL
END ARRAY
READ PLOT TTL='YZ SLICE OF SOUTH CORE FIRST ROW'
XUL=64.319 YUL=40.000 ZUL=72.000
XLR=64.319 YLR=72.000 ZLR=56.000
VAX=1 WDN=-1 NAX=130 NCH='012345678'END
TTL='XZ SLICE OF SPHERE CUBOID'
XUL=56.0 YUL=63.625 ZUL=71.735
XLR=72.0 YLR=63.625 ZLR=55.735
UAX=1 WDN=-1 NAX=130 NCH='012345678'
END PLOT
READ START NST=1 XSM=41.37 XSP=72.894 YSM=40.63 YSP=71.29
ZSM=56.071 ZSP=71.4 END START
END DATA
END

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CAR10
=CSA525
ROCKY FLATS CRITICALS NUREG/CR-0674 CONCRETE REFLECTED (27 GROUP MODEL)
' FUEL CUBE 15.28 CM, U(4.46)308 @ H/U=0.77, HI CONC. SOLUTION DRIVEN
27GROUPNDF4 INFHOMMEDIUM
U308 1 5.4078E-1 293.0 92234 0.03 92235 4.46 92236 0.08 92238 95.43 END
H20 1 8.9514E-2 END
ARBM-BAGGIE 1.0 3 0 0 0 1001 14.01 6012 84.9 8016 1.20 1 1.9134E-2
END
ARBM-AL1100 1.0 3 0 0 1 13027 99.18 26000 0.5 29000 0.2 2 9.5390E-1
END
ARBM-TAPE(VINYL) 1.0 7 0 0 0 1001 5.92 6012 45.91 8016 10.82 17000
25.73 20040 6.9 22000 1.6 82000 1.1 2 1.1115E-2 END
ARBM-TAPE(MYLAR) 1.0 3 0 0 0 1001 6.83 6012 65.50 8016 27.02 2
1.7491E-2 END
ARBM-AL1100 1.0 3 0 0 1 13027 99.18 26000 0.5 29000 0.2 7 2.715 END
RFCONCRETE 5 1.0 END
SOLNUO2(NO3)2 8 351.18 0.549 1.0 293.0 92234 1.022 92235 93.172
92236 0.434 92238 5.372 END
SS304 9 1.0 END
END COMP
ROCKY FLATS CRITICALS NUREG/CR-0674 CONCRETE REFLECTED (27 GROUP MODEL)
' FUEL CUBE 15.28 CM, U(4.46)308 @ H/U=0.77, HI CONC. SOLUTION DRIVEN
READ PARM NPG=600 NUB=YES FDN=YES PLT=NO END PARM
READ GEOM
UNIT 1
COM='FUEL BOX WITH VOID AND PART OF AL BOX'
CUBOID 0 1 9.80 0.0 3.75 0.0 14.98 0.0
CUBOID 2 1 9.95 0.0 3.90 -0.15 14.98 0.0
CUBOID 1 1 14.98 0.0 9.365 -5.615 14.98 0.0

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UNIT 2
COM='FRONT OF FUEL BOX'
CUBOID 2 1 0.15 0.0 5.615 0.0 14.98 0.0
CUBOID 0 1 0.15 0.0 9.365 0.0 14.98 0.0
CUBOID 2 1 0.15 0.0 14.98 0.0 14.98 0.0
UNIT 3
COM='REAR OF FUEL BOX'
CUBOID 2 1 0.15 0.0 14.98 0.0 14.98 0.0
UNIT 4
COM='ARRAY TO ASSEMBLE PART OF BOX'
ARRAY 26 3*0
UNIT 5
COM='TOP AND BOTTOM OF BOX'
CUBOID 0 1 9.80 0.0 3.750 0.0 0.15 0.0
CUBOID 2 1 15.28 0.0 9.365 -5.615 0.15 0.0
GLOBAL
UNIT 6
COM='ARRAY TO ASSEMBLE TOP AND BOTTOM'
ARRAY 27 3*0
CUBOID 2 1 15.28 0.0 15.13 -0.15 15.28 0.0
CUBOID 0 1 15.305 -0.025 15.155 -0.175 15.305 -0.025
UNIT 7
COM='FUEL BOX 15.28 CM ON A SIDE WITH .15 CM WALLS .05CM STACKING VOID'
CUBOID 1 1 6P7.49
CUBOID 2 1 6P7.64
CUBOID 0 1 6P7.6650
UNIT 34
COM='ALUMINUM WEIGHT DISTRIBUTION PLATE FOR SPECIAL BOX'
CUBOID 0 1 9.80 0.0 3.750 0.0 0.16 0.0
CUBOID 7 1 15.33 0.0 9.54 -5.79 0.16 0.0
UNIT 35
COM='ALUMINUM WEIGHT DISTRIBUTION PLATE FOR BOXES'
CUBOID 7 1 4P7.665 0.16 0.0
UNIT 9
COM='NORTH SPLIT TABLE CORE AND REFLECTOR'
ARRAY 1 -30.66 0.0 0.0
CUBOID 0 1 0.0 -32.3 77.5 0.0 83.2 0.0
CUBOID 5 1 0.0 -57.8 103.0 -25.5 108.7 -25.5
UNIT 10
COM='SOUTH SPLIT TABLE CORE AND REFLECTOR'
ARRAY 2 3*0.0
CUBOID 0 1 47.5 0.0 77.5 0.0 83.2 0.0
CUBOID 5 1 73.0 0.0 103.0 -25.5 108.7 -25.5
HOLE 11 0.0 38.75 -25.5
HOLE 11 0.0 38.75 83.2
UNIT 11
CUBOID 0 1 10.2 0.0 2P2.55 25.5 0.0
UNIT 54
COM='AIR GAP'
CUBOID 0 1 2P.334 2P64.25 2P67.1
GLOBAL
UNIT 55
COM='TOTAL'
ARRAY 25 3*0.0
UNIT 56
COM='COMBINATION OF TWO REGULAR FUEL BOXES'
ARRAY 28 3*0.0
UNIT 57
COM='COMBINATION OF REGULAR FUEL BOX AND SPECIAL FUEL BOX'
ARRAY 29 3*0.0
UNIT 58
COM='COMBINATION OF TWO REGULAR WEIGHT DISTRIBUTION PLATES'
ARRAY 30 3*0.0

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Table A.3 (continued)

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UNIT 59
COM='COMBINATION OF REGULAR AND SPECIAL WEIGHT DISTRIBUTION PLATES'
ARRAY 31 3*0.0
UNIT 60
COM='NORTH CORE SOLUTION DRIVER'
CUBOID 8 1 2P7.5 2P14.9 3.122 -7.5
CUBOID 0 1 2P7.5 2P14.9 2P7.5
CUBOID 9 1 2P7.65 2P15.05 2P7.65
CUBOID 0 1 2P7.665 2P15.33 2P7.665
UNIT 61
COM='SOUTH CORE SOLUTION DRIVER'
CUBOID 8 1 2P7.5 2P14.9 3.047 -7.5
CUBOID 0 1 2P7.5 2P14.9 2P7.5
CUBOID 9 1 2P7.65 2P15.05 2P7.65
CUBOID 0 1 2P7.665 2P15.33 2P7.665
END GEOMETRY
READ ARRAY
ARA-1 NUX=2 NUY=4 NUZ=9
COM='NORTH SPLIT TABLE CORE'
FILL 2R7 2R56 4R7
      2R35 2R58 4R35
      2R7 2R56 4R7
      2R35 2R58 4R35
      2R7 56 60 4R7
      2R35 2R58 4R35
      2R7 2R56 4R7
      2R35 2R58 4R35
      2R7 2R56 4R7
END FILL
ARA-2 NUX=3 NUY=4 NUZ=9
COM='SOUTH SPLIT TABLE CORE'
FILL 3R7 3R56 6R7
      3R35 3R58 6R35
      3R7 3R56 6R7
      3R35 3R58 6R35
      3R7 61 56 56 6R7
      3R35 3R58 6R35
      3R7 57 56 56 6R7
      3R35 59 58 58 6R35
      3R7 57 56 56 6R7
END FILL
ARA-25 NUX=3 NUY=1 NUZ=1
COM='TOTAL'
FILL 9 54 10 END FILL
ARA-26 NUX=3 NUY=1 NUZ=1
COM='ASSEMBLY OF FUEL BOX FRONT AND REAR'
FILL 2 1 3 END FILL
ARA-27 NUX=1 NUY=1 NUZ=3
COM='ASSEMBLY OF FUEL BOX TOP AND BOTTOM'
FILL 5 4 5 END FILL
ARA-28 NUX=1 NUY=2 NUZ=1
COM='COMBINATION OF TWO FUEL BOXES'
FILL 7 7 END FILL
ARA-29 NUX=1 NUY=2 NUZ=1
COM='COMBINATION OF SPECIAL AND REGULAR FUEL BOXES'
FILL 7 6 END FILL
ARA-30 NUX=1 NUY=2 NUZ=1
COM='COMBINATION OF TWO WEIGHT DISTRIBUTION PLATES'
FILL 35 35 END FILL
ARA-31 NUX=1 NUY=2 NUZ=1
COM='COMBINATION OF SPECIAL AND REGULAR WEIGHT DISTRIBUTION PLATES'
FILL 35 34 END FILL
END ARRAY

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READ PLOT TTL='YZ SLICE OF SOUTH CORE FIRST ROW'
XUL=64.319 YUL=40.000 ZUL=72.000
XLR=64.319 YLR=72.000 ZLR=56.000
VAX=1 WDN=-1 NAX=130 NCH='012345678' END
TTL='XZ SLICE OF SPHERE CUBOID'
XUL=56.0 YUL=63.625 ZUL=71.735
XLR=72.0 YLR=63.625 ZLR=55.735
UAX=1 WDN=-1 NAX=130 NCH='012345678'
END PLOT
READ START NST=1 XSM=15.0 XSP=122.0 YSM=15.0 YSP=122.0
      ZSM=15.0 ZSP=122.0 END START
END DATA
END

CAR11
=CSAS25
ROCKY FLATS CRITICALS NUREG/CR-1653 EXPERIMENT A (27 GROUP)
' 48 FUEL CANS 2.44 CM MODERATOR GEE.HU125.DATA(OPT)
27GROUPNDF4 LATTICECELL
U308 1 5.4078E-1 293.0 92234 0.03 92235 4.46 92236 0.08 92238 95.43 END
H2O 1 1.5627E-1 END
ARBM-BAGGIE 1.0 3 0 0 0 1001 14.01 6012 84.9 8016 1.20 1 1.9134E-2
      END
ARBM-AL1100 1.0 3 0 0 1 13027 99.18 26000 0.5 29000 0.2 2 9.5390E-1
      END
ARBM-TAPE(VINYL) 1.0 7 0 0 0 1001 5.92 6012 45.91 8016 10.82 17000
      25.73 20040 6.9 22000 1.6 82000 1.1 2 1.1115E-2 END
ARBM-TAPE(MYLAR) 1.0 3 0 0 0 1001 6.83 6012 65.50 8016 27.02 2
      1.7491E-2 END
ARBM-MODERATOR 1.185 3 0 0 0 1001 7.83 6012 59.49 8016 32.48 3 END
ARBM-PLEX(REG) 1.0 3 0 0 0 1001 7.84 6012 59.59 8016 32.23 4
      1.1773 END
ARBM-PLEX(PAPER) 1.0 3 0 0 0 1001 6.48 6012 42.17 8016 49.5 4
      3.7534E-3 END
ARBM-PLEX(GLUE) 1.0 3 0 0 0 1001 11.67 6012 86.29 8016 1.20 4
      1.1648E-3 END
ARBM-PLEX(TRIS) 1.0 8 0 0 1 1001 7.16 6012 52.03 7014 0.16 8016 29.82
      15031 1.02 17000 1.81 35079 4.260 35081 2.840 5 1.2757 END
ARBM-PLEX(PAPER) 1.0 3 0 0 0 1001 6.48 6012 42.17 8016 49.5 5
      3.7534E-3 END
ARBM-PLEX(GLUE) 1.0 3 0 0 0 1001 11.67 6012 86.29 8016 1.20 5
      1.1648E-3 END
ARBM-FILLER 1.185 3 0 0 0 1001 7.83 6012 59.49 8016 32.48 6 .888 END
' THIS MATERIAL IS ACTUALLY MODERATOR ADJUSTED FOR THE VOLUME
' FRACTION OF THE VOID FILLED BETWEEN CORE AND REFLECTOR.
END COMP
SPHTRIANGP 19.9462 18.5857 1 3 18.9579 2 END
ROCKY FLATS CRITICALS NUREG/CR-1653 EXPERIMENT A (27 GROUP)
' 48 FUEL CANS 2.44 CM MODERATOR GEE.HU125.DATA(OPT)
READ PARM RUN=YES NPG=600 FDN=YES NUB=YES PLT=NO END PARM
READ GEOM
UNIT 1
COM='FUEL BOX 15.28 CM ON A SIDE WITH .15 CM WALLS .05CM STACKING VOID'
CUBOID 1 1 6P7.49
CUBOID 2 1 6P7.64
CUBOID 0 1 6P7.6650
UNIT 2
COM='X-FACE INTERSTITIAL MODERATOR'
CUBOID 3 1 2P1.2200 4P7.665

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Table A.3 (continued)

UNIT 3
 COM='Y-FACE INTERSTITIAL MODERATOR'
 CUBOID 3 1 2P7.665 2P1.2200 2P7.665
 UNIT 4
 COM='Z-FACE INTERSTITIAL MODERATOR'
 CUBOID 3 1 4P7.665 2P1.2200
 UNIT 5
 COM='MORE X-FACE MODERATOR'
 CUBOID 3 1 4P1.2200 2P7.665
 UNIT 6
 COM='MORE Y-FACE MODERATOR'
 CUBOID 3 1 2P7.665 4P1.2200
 UNIT 7
 COM='MORE Z-FACE MODERATOR'
 CUBOID 3 1 2P1.2200 2P7.665 2P1.2200
 UNIT 8
 COM='LAST OF INTERSTITIAL MODERATOR'
 CUBOID 3 1 6P1.2200
 UNIT 9
 COM='NORTH SPLIT TABLE CORE'
 ARRAY 1 3*0.0
 UNIT 10
 COM='SOUTH SPLIT TABLE CORE'
 ARRAY 2 3*0.0
 UNIT 11
 COM='PLEXIGLASS REFLECTOR SHEET WITHOUT TRIS, NORTH BOTTOM REFLECTOR'
 CUBOID 4 1 2P16.5500 2P38.7500 2P0.6150
 UNIT 12
 COM='PLEXIGLASS REFLECTOR SHEET WITH TRIS, NORTH BOTTOM REFLECTOR'
 CUBOID 5 1 2P16.5500 2P38.7500 2P0.6150
 UNIT 13
 COM='UPPER PORTION NORTH BOTTOM REFLECTOR WITH TRIS'
 CUBOID 5 1 2P16.550 2P38.75 2P8.24
 UNIT 14
 COM='LOWER PORTION NORTH BOTTOM REFLECTOR WITH TRIS'
 CUBOID 5 1 2P16.550 2P38.75 2P3.69
 UNIT 15
 COM='NORTH BOTTOM REFLECTOR INCLUDES REGULAR AND TRIS'
 ARRAY 3 3*0.0
 UNIT 16
 COM='PLEXIGLAS SHEET BOTTOM SOUTH REFLECTOR WITHOUT TRIS'
 CUBOID 0 1 2P5.1 2P2.55 2P0.615
 CUBOID 4 1 44.3 -5.1 2P38.75 2P0.615
 UNIT 17
 COM='PLEXIGLAS SHEET BOTTOM SOUTH REFLECTOR WITH TRIS'
 CUBOID 0 1 2P5.1 2P2.55 2P0.615
 CUBOID 5 1 44.3 -5.1 2P38.75 2P0.6150
 UNIT 18
 COM='LOWER PORTION SOUTH BOTTOM REFLECTOR WITH TRIS'
 CUBOID 0 1 2P5.1 2P2.55 2P8.855
 CUBOID 5 1 44.3 -5.1 2P38.75 2P8.855
 UNIT 19
 COM='SOUTH BOTTOM REFLECTOR WITH REGULAR AND TRIS'
 ARRAY 4 3*0.0
 UNIT 20
 COM='EAST AND WEST REFLECTORS FOR NORTH REFLECTOR WITH TRIS'
 CUBOID 5 1 2P16.550 2P12.65 2P54.2825
 UNIT 21
 COM='ARRAY FOR EAST AND WEST REFLECTORS FOR NORTH REFLECTOR'
 ARRAY 5 3*0.0
 UNIT 22
 COM='EAST AND WEST REFLECTORS FOR SOUTH REFLECTOR WITH TRIS'
 CUBOID 5 1 2P24.700 2P12.65 2P54.2825

UNIT 23
 COM='ARRAY FOR EAST AND WEST REFLECTORS FOR SOUTH REFLECTOR'
 ARRAY 6 3*0.0
 UNIT 24
 COM='NORTH TOP REFLECTOR WITH TRIS'
 CUBOID 5 1 2P29.100 2P64.05 2P12.15
 UNIT 25
 COM='ARRAY FOR NORTH TOP REFLECTOR'
 ARRAY 7 3*0.0
 UNIT 26
 COM='SOUTH TOP REFLECTOR WITH TRIS'
 CUBOID 0 1 2P5.1 2P2.55 2P12.15
 CUBOID 5 1 69.4 -5.1 2P64.05 2P12.15
 UNIT 27
 COM='ARRAY FOR SOUTH TOP REFLECTOR'
 ARRAY 8 3*0.0
 UNIT 28
 COM='NORTH END REFLECTOR 9.8CM PORTION WITHOUT TRIS'
 CUBOID 4 1 2P4.9000 2P64.0500 2P54.2825
 UNIT 29
 COM='NORTH END REFLECTOR 5.2 CM PORTION WITH TRIS'
 CUBOID 5 1 2P2.6 2P64.0500 2P54.2825
 UNIT 30
 COM='NORTH END REFLECTOR 10.1 CM PORTION WITHOUT TRIS'
 CUBOID 4 1 2P5.05 2P64.05 2P54.2825
 UNIT 31
 COM='ARRAY FOR NORTH END REFLECTOR'
 ARRAY 9 3*0.0
 UNIT 32
 COM='SOUTH END REFLECTOR'
 CUBOID 5 1 2P12.55 2P64.05 2P54.2825
 UNIT 33
 COM='ARRAY FOR SOUTH END REFLECTOR'
 ARRAY 10 3*0.0
 UNIT 34
 COM='BOTTOM MODERATING PLASTIC NORTH CORE'
 CUBOID 6 1 2P16.550 2P38.7500 2P13.0500
 UNIT 35
 COM='TOP MODERATING PLASTIC NORTH CORE'
 CUBOID 6 1 2P16.550 2P38.7500 2P3.2525
 UNIT 36
 ARRAY 11 3*0.0
 UNIT 37
 ARRAY 12 3*0.0
 UNIT 38
 COM='NORTH CORE WITH BOTTOM REFLECTOR'
 ARRAY 13 3*0.0
 UNIT 39
 COM='NORTH CORE WITH EAST AND WEST REFLECTOR'
 ARRAY 14 3*0.0
 UNIT 40
 COM='NORTH CORE WITH END REFLECTOR'
 ARRAY 15 3*0.0
 UNIT 41
 COM='NORTH SPLIT TABLE FACEPLATE'
 CUBOID 3 1 2P0.6150 2P64.0500 2P66.4325
 UNIT 42
 COM='NORTH CORE WITH TOP REFLECTOR'
 ARRAY 16 3*0.0
 UNIT 43
 COM='NORTH CORE WITH FACEPLATE'
 ARRAY 17 3*0.0

Table A.3 (continued)

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UNIT 44
COM='12.95 CM THICK MODERATOR SOUTH CORE'
CUBOID 6 1 2P23.924 2P6.475 2P40.183
UNIT 45
COM='2.95 THICK MODERATOR SOUTH CORE'
CUBOID 6 1 2P23.924 2P38.5285 2P1.475
UNIT 46
COM='COMBINATION OF CORE WITH 12.95 THICK MODERATOR'
ARRAY 18 3*0.0
UNIT 47
COM='COMBINATION OF CORE WITH 2.95 THICK MODERATOR'
ARRAY 19 3*0.0
UNIT 48
COM='SOUTH CORE WITH EAST WEST REFLECTORS'
ARRAY 20 3*0.0
UNIT 49
COM='SOUTH CORE WITH EAST WEST REFLECTORS'
ARRAY 21 3*0.0
UNIT 50
COM='SOUTH CORE END REFLECTOR'
ARRAY 22 3*0.0
UNIT 51
COM='FACEPLATE FOR SOUTH SPLIT TABLE'
CUBOID 3 1 2P0.4620 2P64.0500 2P66.4325
UNIT 52
COM='SOUTH CORE WITH TOP REFLECTOR'
ARRAY 23 3*0.0
UNIT 53
COM='SOUTH CORE WITH FACEPLATE'
ARRAY 24 3*0.0
UNIT 54
COM='AIR GAP'
CUBOID 0 1 2P0.1550 2P64.0500 2P66.4325
GLOBAL
UNIT 55
COM='TOTAL'
ARRAY 25 3*0.0
UNIT 56
COM='EMPTY FUEL LOCATION'
CUBOID 0 1 6P7.6650
UNIT 57
COM='SIDE MODERATOR'
CUBOID 5 1 2P16.550 2P4.4300 2P25.4350
UNIT 58
COM='END MODERATOR'
CUBOID 6 1 2P8.1500 2P38.7500 2P25.4350
UNIT 59
COM='SOUTH CORE BOTTOM MODERATING PLASTIC'
CUBOID 6 1 2P24.7000 2P38.7500 2P13.0500
UNIT 60
COM='SOUTH CORE TOP MODERATING PLASTIC'
CUBOID 6 1 2P24.7000 2P38.7500 2P3.2525
UNIT 61
COM='Y-FACE MODERATOR VOID'
CUBOID 0 1 2P7.665 2P1.2200 2P7.665
UNIT 62
COM='X-FACE MODERATOR VOID'
CUBOID 0 1 2P1.2200 4P7.665
END GEOMETRY
READ ARRAY
ARA=1 NUX=3 NUY=7 NUZ=5
COM='NORTH SPLIT TABLE CORE'

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```

FILL 1 2 1 3 5 3 2Q6 1 2 1
      4 7 4 6 8 6 2Q6 4 7 4
      1Q42
      56 2 1 61 5 3 56 2 1 61 5 3 1Q6 56 62 56 END FILL
ARA=2 NUX=3 NUY=7 NUZ=5
COM='SOUTH SPLIT TABLE CORE'
FILL 1 2 1 3 5 3 2Q6 1 2 1
      4 7 4 6 8 6 2Q6 4 7 4
      1Q42
      1 2 56 3 5 61 2Q6 56 62 56 END FILL
ARA=3 NUX=1 NUY=1 NUZ=3
COM='NORTH BOTTOM REFLECTOR'
FILL 14 11 13 END FILL
ARA=4 NUX=1 NUY=1 NUZ=7
COM='SOUTH BOTTOM REFLECTOR'
FILL 18 16 17 16 16 17 17 END FILL
ARA=5 NUX=1 NUY=1 NUZ=1
COM='EAST AND WEST WALLS OF NORTH REFLECTOR'
FILL 20 END FILL
ARA=6 NUX=1 NUY=1 NUZ=1
COM='EAST AND WEST WALLS OF SOUTH REFLECTOR'
FILL 22 END FILL
ARA=7 NUX=1 NUY=1 NUZ=1
COM='ARRAY FOR NORTH TOP REFLECTOR'
FILL 24 END FILL
ARA=8 NUX=1 NUY=1 NUZ=1
COM='ARRAY FOR SOUTH TOP REFLECTOR'
FILL 26 END FILL
ARA=9 NUX=3 NUY=1 NUZ=1
COM='ARRAY FOR NORTH END REFLECTOR'
FILL 28 29 30 END FILL
ARA=10 NUX=1 NUY=1 NUZ=1
COM='ARRAY FOR SOUTH END REFLECTOR'
FILL 32 END FILL
ARA=11 NUX=1 NUY=2 NUZ=1
COM='COMBINARION OF CORE WITH SIDE MODERATOR'
FILL 9 57 END FILL
ARA=12 NUX=1 NUY=1 NUZ=3
COM='COMBINATION OF PREVIOUS ARRAY WITH TOP AND BOTTOM MODERATOR'
FILL 34 36 35 END FILL
ARA=13 NUX=1 NUY=1 NUZ=2
COM='COMBINATION OF NORTH CORE WITH BOTTOM REFLECTOR'
FILL 15 37 END FILL
ARA=14 NUX=1 NUY=3 NUZ=1
COM='NORTH CORE WITH SIDE REFLECTORS'
FILL 21 38 21 END FILL
ARA=15 NUX=2 NUY=1 NUZ=1
COM='NORTH CORE WITH END REFLECTOR'
FILL 31 39 END FILL
ARA=16 NUX=1 NUY=1 NUZ=2
COM='NORTH CORE WITH TOP REFLECTOR'
FILL 40 25 END FILL
ARA=17 NUX=2 NUY=1 NUZ=1
COM='NORTH CORE WITH FACEPLATE'
FILL 42 41 END FILL
ARA=18 NUX=1 NUY=2 NUZ=1
COM='COMBINATION OF S. CORE WITH SIDE MODERATOR'
FILL 10 57 END FILL
ARA=19 NUX=2 NUY=1 NUZ=1
COM='COMBINATION OF CORE WITH END MODERATOR'
FILL 46 58 END FILL
ARA=20 NUX=1 NUY=1 NUZ=4
COM='SOUTH CORE WITH BOTTOM MODERATOR AND REFLECTOR'
FILL 19 59 47 60 END FILL

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Table A.3 (continued)

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ARA=21 NUX=1 NUY=3 NUZ=1
COM='SOUTH CORE WITH EAST WEST REFLECTORS'
FILL 23 48 23 END FILL
ARA=22 NUX=2 NUY=1 NUZ=1
COM='SOUTH CORE WITH END REFLECTOR'
FILL 49 33 END FILL
ARA=23 NUX=1 NUY=1 NUZ=2
COM='COMBINATION OF CORE WITH TOP REFLECTOR'
FILL 50 27 END FILL
ARA=24 NUX=2 NUY=1 NUZ=1
COM='SOUTH CORE WITH FACEPLATE'
FILL 51 52 END FILL
ARA=25 NUX=3 NUY=1 NUZ=1
COM='TOTAL'
FILL 43 54 53 END FILL
END ARRAY
READ PLOT TTL='YZ SLICE OF RFP1 SHOWING MATERIAL REGIONS'
XUL=-2 YUL=64.05 ZUL=136
XLR=137 YLR=64.05 ZLR=-2
UAX=1 WDN=-1 NAX=130 NCH='0123456'END
TTL='YZ SLICE OF NORTH CORE FIRST ROW'
XUL=48 YUL=-2 ZUL=136
XLR=48 YLR=136 ZLR=-2
VAX=1 WDN=-1 NAX=130 NCH='0123456'END
TTL='YZ SLICE OF NORTH CORE SECOND ROW'
XUL=28 YUL=-2 ZUL=136
XLR=28 YLR=136 ZLR=-2
VAX=1 WDN=-1 NAX=130 NCH='0123456'END
TTL='YZ SLICE OF SOUTH CORE FIRST ROW'
XUL=62 YUL=-2 ZUL=136
XLR=62 YLR=136 ZLR=-2
VAX=1 WDN=-1 NAX=130 NCH='0123456'END
TTL='YZ SLICE OF SOUTH CORE SECOND ROW'
XUL=80 YUL=-2 ZUL=136
XLR=80 YLR=136 ZLR=-2
VAX=1 WDN=-1 NAX=130 NCH='0123456'END
END PLOT
END DATA
END

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CAR12
=CSAS25
ROCKY PLATS CRITICALS NUREG/CR-1653 EXPERIMENT B (27 GROUP)
' 78 FUEL CANS 0.929 CM MODERATOR GEE.HU125.DATA(UND1)
27GROUPNDP4 LATTICECELL
U308 1 5.4078E-1 293.0 92234 0.03 92235 4.46 92236 0.08 92238 95.43 END
H20 1 1.5627E-1 END
ARBM-BAGGIE 1.0 3 0 0 0 1001 14.01 6012 84.9 8016 1.20 1 1.9134E-2
END
ARBM-AL1100 1.0 3 0 0 1 13027 99.18 26000 0.5 29000 0.2 2 9.5390E-1
END
ARBM-TAPE(VINYL) 1.0 7 0 0 0 1001 5.92 6012 45.91 8016 10.82 17000
25.73 20040 6.9 22000 1.6 82000 1.1 2 1.1115E-2 END
ARBM-TAPE(MYLAR) 1.0 3 0 0 0 1001 6.83 6012 65.50 8016 27.02 2
1.7491E-2 END
ARBM-MODERATOR 1.185 3 0 0 0 1001 7.83 6012 59.49 8016 32.48 3 END
ARBM-PLEX(REG) 1.0 3 0 0 0 1001 7.84 6012 59.59 8016 32.23 4
1.1773 END
ARBM-PLEX(PAPER) 1.0 3 0 0 0 1001 6.48 6012 42.17 8016 49.5 4
3.7534E-3 END
ARBM-PLEX(GLUE) 1.0 3 0 0 0 1001 11.67 6012 86.29 8016 1.20 4
1.1648E-3 END
ARBM-PLEX(TRIS) 1.0 8 0 0 1 1001 7.16 6012 52.03 7014 0.16 8016 29.82
15031 1.02 17000 1.81 35079 4.260 35081 2.840 5 1.2757 END
ARBM-PLEX(PAPER) 1.0 3 0 0 0 1001 6.48 6012 42.17 8016 49.5 5
3.7534E-3 END
ARBM-PLEX(GLUE) 1.0 3 0 0 0 1001 11.67 6012 86.29 8016 1.20 5
1.1648E-3 END
ARBM-FILLER 1.185 3 0 0 0 1001 7.83 6012 59.49 8016 32.48 6 .854 END
' THIS MATERIAL IS ACTUALLY MODERATOR ADJUSTED FOR THE VOLUME
' FRACTION OF THE VOID FILLED BETWEEN CORE AND REFLECTOR.
END COMP
SPHTRIANGP 19.00 18.5857 1 3 18.9579 2 END
ROCKY PLATS CRITICALS NUREG/CR-1653 EXPERIMENT B (27 GROUP)
' 78 FUEL CANS 0.929 CM MODERATOR GEE.HU125.DATA(UND1)
READ PARM RUN=YES NPG=600 FDN=YES NUB=YES PLT=NO END PARM
READ GEOM
UNIT 1
COM='FUEL BOX 15.28 CM ON A SIDE WITH .15 CM WALLS .05CM STACKING VOID'
CUBOID 1 1 6P7.49
CUBOID 2 1 6P7.64
CUBOID 0 1 6P7.6650
UNIT 2
COM='X-FACE INTERSTITIAL MODERATOR'
CUBOID 3 1 2P0.4645 4P7.665
UNIT 3
COM='Y-FACE INTERSTITIAL MODERATOR'
CUBOID 3 1 2P7.665 2P0.4645 2P7.665
UNIT 4
COM='Z-FACE INTERSTITIAL MODERATOR'
CUBOID 3 1 4P7.665 2P0.4645
UNIT 5
COM='MORE X-FACE MODERATOR'
CUBOID 3 1 4P0.4645 2P7.665
UNIT 6
COM='MORE Y-FACE MODERATOR'
CUBOID 3 1 2P7.665 4P0.4645
UNIT 7
COM='MORE Z-FACE MODERATOR'
CUBOID 3 1 2P0.4645 2P7.665 2P0.4645
UNIT 8
COM='LAST OF INTERSTITIAL MODERATOR'
CUBOID 3 1 6P0.4645

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Table A.3 (continued)

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UNIT 9
COM='NORTH SPLIT TABLE CORE'
ARRAY 1 3*0.0
UNIT 10
COM='SOUTH SPLIT TABLE CORE'
ARRAY 2 3*0.0
UNIT 11
COM='PLEXIGLASS REFLECTOR SHEET WITHOUT TRIS, NORTH BOTTOM REFLECTOR'
CUBOID 4 1 2P15.8000 2P38.7500 2P0.6150
UNIT 12
COM='PLEXIGLASS REFLECTOR SHEET WITH TRIS, NORTH BOTTOM REFLECTOR'
CUBOID 5 1 2P15.8000 2P38.7500 2P0.6150
UNIT 13
COM='UPPER PORTION NORTH BOTTOM REFLECTOR WITH TRIS'
CUBOID 5 1 2P15.8 2P38.75 2P8.24
UNIT 14
COM='LOWER PORTION NORTH BOTTOM REFLECTOR WITH TRIS'
CUBOID 5 1 2P15.8 2P38.75 2P3.69
UNIT 15
COM='NORTH BOTTOM REFLECTOR INCLUDES REGULAR AND TRIS'
ARRAY 3 3*0.0
UNIT 16
COM='PLEXIGLAS SHEET BOTTOM SOUTH REFLECTOR WITHOUT TRIS'
CUBOID 0 1 2P5.1 2P2.55 2P0.615
CUBOID 4 1 44.3 -5.1 2P38.75 2P0.615
UNIT 17
COM='PLEXIGLAS SHEET BOTTOM SOUTH REFLECTOR WITH TRIS'
CUBOID 0 1 2P5.1 2P2.55 2P0.615
CUBOID 5 1 44.3 -5.1 2P38.75 2P0.6150
UNIT 18
COM='LOWER PORTION SOUTH BOTTOM REFLECTOR WITH TRIS'
CUBOID 0 1 2P5.1 2P2.55 2P8.855
CUBOID 5 1 44.3 -5.1 2P38.75 2P8.855
UNIT 19
COM='SOUTH BOTTOM REFLECTOR WITH REGULAR AND TRIS'
ARRAY 4 3*0.0
UNIT 20
COM='EAST AND WEST REFLECTORS FOR NORTH REFLECTOR WITH TRIS'
CUBOID 5 1 2P15.8 2P12.65 2P54.2825
UNIT 21
COM='ARRAY FOR EAST AND WEST REFLECTORS FOR NORTH REFLECTOR'
ARRAY 5 3*0.0
UNIT 22
COM='EAST AND WEST REFLECTORS FOR SOUTH REFLECTOR WITH TRIS'
CUBOID 5 1 2P24.700 2P12.65 2P54.2825
UNIT 23
COM='ARRAY FOR EAST AND WEST REFLECTORS FOR SOUTH REFLECTOR'
ARRAY 6 3*0.0
UNIT 24
COM='NORTH TOP REFLECTOR WITH TRIS'
CUBOID 5 1 2P28.35 2P64.05 2P12.15
UNIT 25
COM='ARRAY FOR NORTH TOP REFLECTOR'
ARRAY 7 3*0.0
UNIT 26
COM='SOUTH TOP REFLECTOR WITH TRIS'
CUBOID 0 1 2P5.1 2P2.55 2P12.15
CUBOID 5 1 69.4 -5.1 2P64.05 2P12.15
UNIT 27
COM='ARRAY FOR SOUTH TOP REFLECTOR'
ARRAY 8 3*0.0
UNIT 28
COM='NORTH END REFLECTOR 9.8CM PORTION WITHOUT TRIS'
CUBOID 4 1 2P4.9000 2P64.0500 2P54.2825

UNIT 29
COM='NORTH END REFLECTOR 5.2 CM PORTION WITH TRIS'
CUBOID 5 1 2P2.6 2P64.0500 2P54.2825
UNIT 30
COM='NORTH END REFLECTOR 10.1 CM PORTION WITHOUT TRIS'
CUBOID 4 1 2P5.05 2P64.05 2P54.2825
UNIT 31
COM='ARRAY FOR NORTH END REFLECTOR'
ARRAY 9 3*0.0
UNIT 32
COM='SOUTH END REFLECTOR'
CUBOID 5 1 2P12.55 2P64.05 2P54.2825
UNIT 33
COM='ARRAY FOR SOUTH END REFLECTOR'
ARRAY 10 3*0.0
UNIT 34
COM='12.95 THICK MODERATING PLASTIC NORTH CORE'
CUBOID 6 1 2P15.7945 2P6.4750 2P32.0535
UNIT 35
COM='2.95 THICK MODERATING PLASTIC NORTH CORE'
CUBOID 6 1 2P15.7945 2P38.5285 2P1.475
UNIT 36
ARRAY 11 3*0.0
UNIT 37
ARRAY 12 3*0.0
REPLICATE 0 1 0.0 0.011 0.443 0.0 0.1590 0.0 1
UNIT 38
COM='NORTH CORE WITH BOTTOM REFLECTOR'
ARRAY 13 3* 0.0
UNIT 39
COM='NORTH CORE WITH EAST AND WEST REFLECTOR'
ARRAY 14 3*0.0
UNIT 40
COM='NORTH CORE WITH END REFLECTOR'
ARRAY 15 3*0.0
UNIT 41
COM='NORTH SPLIT TABLE FACEPLATE'
CUBOID 3 1 2P0.6150 2P64.0500 2P66.4325
UNIT 42
COM='NORTH CORE WITH TOP REFLECTOR'
ARRAY 16 3*0.0
UNIT 43
COM='NORTH CORE WITH FACEPLATE'
ARRAY 17 3*0.0
UNIT 44
COM='12.95 CM THICK MODERATOR SOUTH CORE'
CUBOID 6 1 2P23.924 2P6.475 2P32.0535
UNIT 45
COM='2.95 THICK MODERATOR SOUTH CORE'
CUBOID 6 1 2P23.924 2P38.5285 2P1.475
UNIT 46
COM='COMBINATION OF CORE WITH 12.95 THICK MODERATOR'
ARRAY 18 3*0.0
UNIT 47
COM='COMBINATION OF CORE WITH 2.95 THICK MODERATOR'
ARRAY 19 3*0.0
REPLICATE 0 1 1.552 0.0 0.4430 0.0 0.159 0.0 1
UNIT 48
COM='SOUTH CORE WITH EAST WEST REFLECTORS'
ARRAY 20 3*0.0
UNIT 49
COM='SOUTH CORE WITH EAST WEST REFLECTORS'
ARRAY 21 3*0.0

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Table A.3 (continued)

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UNIT 50
COM='SOUTH CORE END REFLECTOR'
ARRAY 22 3*0.0
UNIT 51
COM='FACEPLATE FOR SOUTH SPLIT TABLE'
CUBOID 3 1 2P0.4620 2P64.0500 2P66.4325
UNIT 52
COM='SOUTH CORE WITH TOP REFLECTOR'
ARRAY 23 3*0.0
UNIT 53
COM='SOUTH CORE WITH FACEPLATE'
ARRAY 24 3*0.0
UNIT 54
COM='AIR GAP'
CUBOID 0 1 2P0.3990 2P64.0500 2P66.4325
GLOBAL
UNIT 55
COM='TOTAL'
ARRAY 25 3*0.0
UNIT 56
COM='NORTH BOTTOM MODERATOR'
CUBOID 6 1 2P15.8000 2P38.7500 2P8.1295
UNIT 57
COM='BOTTOM SOUTH MODERATOR'
CUBOID 6 1 2P24.700 2P38.75 2P8.1295
UNIT 58
COM='EMPTY FUEL LOCATION'
CUBOID 0 1 6P7.665
END GEOMETRY
READ ARRAY
ARA=1 NUX=3 NUY=7 NUZ=7
COM='NORTH SPLIT TABLE CORE'
FILL 1 2 1 3 5 3 2Q6 1 2 1
      4 7 4 6 8 6 2Q6 4 7 4
      2Q42
      1 2 1 3 5 3 2Q6 58 2 58 END FILL
ARA=2 NUX=5 NUY=7 NUZ=7
COM='SOUTH SPLIT TABLE CORE'
FILL 1 2 1 2 1 3 5 3 5 3 2Q10 1 2 1 2 1
      4 7 4 7 4 6 8 6 8 6 2Q10 4 7 4 7 4
      2Q70
      1 2 1 2 1 3 5 3 5 3 2Q10 1 2 1 2 1 END FILL
ARA=3 NUX=1 NUY=1 NUZ=4
COM='NORTH BOTTOM MODERATOR AND REFLECTOR'
FILL 14 11 13 56 END FILL
ARA=4 NUX=1 NUY=1 NUZ=8
COM='SOUTH BOTTOM MODERATOR AND REFLECTOR'
FILL 18 16 17 16 16 17 17 57 END FILL
ARA=5 NUX=1 NUY=1 NUZ=1
COM='EAST AND WEST WALLS OF NORTH REFLECTOR'
FILL 20 END FILL
ARA=6 NUX=1 NUY=1 NUZ=1
COM='EAST AND WEST WALLS OF SOUTH REFLECTOR'
FILL 22 END FILL
ARA=7 NUX=1 NUY=1 NUZ=1
COM='ARRAY FOR NORTH TOP REFLECTOR'
FILL 24 END FILL
ARA=8 NUX=1 NUY=1 NUZ=1
COM='ARRAY FOR SOUTH TOP REFLECTOR'
FILL 26 END FILL
ARA=9 NUX=3 NUY=1 NUZ=1
COM='ARRAY FOR NORTH END REFLECTOR'
FILL 28 29 30 END FILL

ARA=10 NUX=1 NUY=1 NUZ=1
COM='ARRAY FOR SOUTH END REFLECTOR'
FILL 32 END FILL
ARA=11 NUX=1 NUY=2 NUZ=1
COM='COMBINATION OF CORE WITH 12.95CM THICK MODERATOR'
FILL 9 34 END FILL
ARA=12 NUX=1 NUY=1 NUZ=2
COM='COMBINATION OF PREVIOUS ARRAY WITH 2.95CM THICK MODERATOR'
FILL 36 35 END FILL
ARA=13 NUX=1 NUY=1 NUZ=2
COM='COMBINATION OF NORTH CORE WITH BOTTOM REFLECTOR'
FILL 15 37 END FILL
ARA=14 NUX=1 NUY=3 NUZ=1
COM='NORTH CORE WITH SIDE REFLECTORS'
FILL 21 38 21 END FILL
ARA=15 NUX=2 NUY=1 NUZ=1
COM='NORTH CORE WITH END REFLECTOR'
FILL 31 39 END FILL
ARA=16 NUX=1 NUY=1 NUZ=2
COM='NORTH CORE WITH TOP REFLECTOR'
FILL 40 25 END FILL
ARA=17 NUX=2 NUY=1 NUZ=1
COM='NORTH CORE WITH FACEPLATE'
FILL 42 41 END FILL
ARA=18 NUX=1 NUY=2 NUZ=1
COM='COMBINATION OF S. CORE WITH 12.95 CM THICK MODERATOR'
FILL 10 44 END FILL
ARA=19 NUX=1 NUY=1 NUZ=2
COM='COMBINATION OF CORE WITH 2.95 CM THICK MODERATOR'
FILL 46 45 END FILL
ARA=20 NUX=1 NUY=1 NUZ=2
COM='SOUTH CORE WITH BOTTOM REFLECTOR'
FILL 19 47 END FILL
ARA=21 NUX=1 NUY=3 NUZ=1
COM='SOUTH CORE WITH EAST WEST REFLECTORS'
FILL 23 48 23 END FILL
ARA=22 NUX=2 NUY=1 NUZ=1
COM='SOUTH CORE WITH END REFLECTOR'
FILL 49 33 END FILL
ARA=23 NUX=1 NUY=1 NUZ=2
COM='COMBINATION OF CORE WITH TOP REFLECTOR'
FILL 50 27 END FILL
ARA=24 NUX=2 NUY=1 NUZ=1
COM='SOUTH CORE WITH FACEPLATE'
FILL 51 52 END FILL
ARA=25 NUX=3 NUY=1 NUZ=1
COM='TOTAL'
FILL 43 54 53 END FILL
END ARRAY
READ PLOT TTL='XZ SLICE OF RFP3 SHOWING MATERIAL REGIONS'
XUL=-1 YUL=64.05 ZUL=135
XLR=136 YLR=64.05 ZLR=-2
UAX=1 WDN=-1 NAX=130 NCH='0123456'END
TTL='YZ SLICE OF NORTH CORE FIRST ROW'
XUL=48 YUL=-2 ZUL=136
XLR=48 YLR=136 ZLR=-2
VAX=1 WDN=-1 NAX=130 NCH='0123456'END
TTL='YZ SLICE OF NORTH CORE SECOND ROW'
XUL=28 YUL=-2 ZUL=136
XLR=28 YLR=136 ZLR=-2
VAX=1 WDN=-1 NAX=130 NCH='0123456'END
TTL='YZ SLICE OF SOUTH CORE SECOND ROW'

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Table A.3 (continued)

XUL=80 YUL=-2 ZUL=136
 XLR=80 YLR=136 ZLR=-2
 VAX=1 WDN=-1 NAX=130 NCH='0123456'
 END PLOT
 END DATA
 END

CAR13
 =CSAS25
 ROCKY FLATS CRITICALS NUREG/CR-1653 EXPERIMENT C (27 GROUP)
 ' 80 FUEL CANS 0.929 CM MODERATOR GEE.HU125.DATA(UND2)
 27GROUPNDF4 LATTICECELL
 U308 1 5.4078E-1 293.0 92234 0.03 92235 4.46 92236 0.08 92238 95.43 END
 H2O 1 1.5627E-1 END
 ARBM-BAGGIE 1.0 3 0 0 0 1001 14.01 6012 84.9 8016 1.20 1 1.9134E-2
 END
 ARBM-AL1100 1.0 3 0 0 1 13027 99.18 26000 0.5 29000 0.2 2 9.5390E-1
 END
 ARBM-TAPE(VINYL) 1.0 7 0 0 0 1001 5.92 6012 45.91 8016 10.82 17000
 25.73 20040 6.9 22000 1.6 82000 1.1 2 1.1115E-2 END
 ARBM-TAPE(MYLAR) 1.0 3 0 0 0 1001 6.83 6012 65.50 8016 27.02 2
 1.7491E-2 END
 ARBM-MODERATOR 1.185 3 0 0 0 1001 7.83 6012 59.49 8016 32.48 3 END
 ARBM-PLEX(REG) 1.0 3 0 0 0 1001 7.84 6012 59.59 8016 32.23 4
 1.1773 END
 ARBM-PLEX(PAPER) 1.0 3 0 0 0 1001 6.48 6012 42.17 8016 49.5 4
 3.7534E-3 END
 ARBM-PLEX(GLUE) 1.0 3 0 0 0 1001 11.67 6012 86.29 8016 1.20 4
 1.1648E-3 END
 ARBM-PLEX(TRIS) 1.0 8 0 0 1 1001 7.16 6012 52.03 7014 0.16 8016 29.82
 15031 1.02 17000 1.81 35079 4.260 35081 2.840 5 1.2757 END
 ARBM-PLEX(PAPER) 1.0 3 0 0 0 1001 6.48 6012 42.17 8016 49.5 5
 3.7534E-3 END
 ARBM-PLEX(GLUE) 1.0 3 0 0 0 1001 11.67 6012 86.29 8016 1.20 5
 1.1648E-3 END
 ARBM-FILLER 1.185 3 0 0 0 1001 7.83 6012 59.49 8016 32.48 6 .854 END
 ' THIS MATERIAL IS ACTUALLY MODERATOR ADJUSTED FOR THE VOLUME
 ' FRACTION OF THE VOID FILLED BETWEEN CORE AND REFLECTOR.
 END COMP
 SPHTRIANGP 19.00 18.5857 1 3 18.9579 2 END
 ROCKY FLATS CRITICALS NUREG/CR-1653 EXPERIMENT C (27 GROUP)
 ' 80 FUEL CANS 0.929 CM MODERATOR GEE.HU125.DATA(UND2)
 READ PARM RUN=YES NPG=600 FDN=YES NUB=YES PLT=NO END PARM
 READ GEOM
 UNIT 1
 COM='FUEL BOX 15.28 CM ON A SIDE WITH .15 CM WALLS .05CM STACKING VOID'
 CUBOID 1 1 6P7.49
 CUBOID 2 1 6P7.64
 CUBOID 0 1 6P7.6650
 UNIT 2
 COM='X-FACE INTERSTITIAL MODERATOR'
 CUBOID 3 1 2P0.4645 4P7.665
 UNIT 3
 COM='Y-FACE INTERSTITIAL MODERATOR'
 CUBOID 3 1 2P7.665 2P0.4645 2P7.665
 UNIT 4
 COM='Z-FACE INTERSTITIAL MODERATOR'
 CUBOID 3 1 4P7.665 2P0.4645
 UNIT 5
 COM='MORE X-FACE MODERATOR'
 CUBOID 3 1 4P0.4645 2P7.665

UNIT 6
 COM='MORE Y-FACE MODERATOR'
 CUBOID 3 1 2P7.665 4P0.4645
 UNIT 7
 COM='MORE Z-FACE MODERATOR'
 CUBOID 3 1 2P0.4645 2P7.665 2P0.4645
 UNIT 8
 COM='LAST OF INTERSTITIAL MODERATOR'
 CUBOID 3 1 6P0.4645
 UNIT 9
 COM='NORTH SPLIT TABLE CORE'
 ARRAY 1 3*0.0
 UNIT 10
 COM='SOUTH SPLIT TABLE CORE'
 ARRAY 2 3*0.0
 UNIT 11
 COM='PLEXIGLASS REFLECTOR SHEET WITHOUT TRIS, NORTH BOTTOM REFLECTOR'
 CUBOID 4 1 2P15.8000 2P38.7500 2P0.6150
 UNIT 12
 COM='PLEXIGLASS REFLECTOR SHEET WITH TRIS, NORTH BOTTOM REFLECTOR'
 CUBOID 5 1 2P15.8000 2P38.7500 2P0.6150
 UNIT 13
 COM='UPPER PORTION NORTH BOTTOM REFLECTOR WITH TRIS'
 CUBOID 5 1 2P15.8 2P38.75 2P8.24
 UNIT 14
 COM='LOWER PORTION NORTH BOTTOM REFLECTOR WITH TRIS'
 CUBOID 5 1 2P15.8 2P38.75 2P3.69
 UNIT 15
 COM='NORTH BOTTOM REFLECTOR INCLUDES REGULAR AND TRIS'
 ARRAY 3 3*0.0
 UNIT 16
 COM='PLEXIGLASS SHEET BOTTOM SOUTH REFLECTOR WITHOUT TRIS'
 CUBOID 0 1 2P5.1 2P2.55 2P0.615
 CUBOID 4 1 44.3 -5.1 2P38.75 2P0.615
 UNIT 17
 COM='PLEXIGLASS SHEET BOTTOM SOUTH REFLECTOR WITH TRIS'
 CUBOID 0 1 2P5.1 2P2.55 2P0.615
 CUBOID 5 1 44.3 -5.1 2P38.75 2P0.6150
 UNIT 18
 COM='LOWER PORTION SOUTH BOTTOM REFLECTOR WITH TRIS'
 CUBOID 0 1 2P5.1 2P2.55 2P8.855
 CUBOID 5 1 44.3 -5.1 2P38.75 2P8.855
 UNIT 19
 COM='SOUTH BOTTOM REFLECTOR WITH REGULAR AND TRIS'
 ARRAY 4 3*0.0
 UNIT 20
 COM='EAST AND WEST REFLECTORS FOR NORTH REFLECTOR WITH TRIS'
 CUBOID 5 1 2P15.8 2P12.65 2P54.2825
 UNIT 21
 COM='ARRAY FOR EAST AND WEST REFLECTORS FOR NORTH REFLECTOR'
 ARRAY 5 3*0.0
 UNIT 22
 COM='EAST AND WEST REFLECTORS FOR SOUTH REFLECTOR WITH TRIS'
 CUBOID 5 1 2P24.700 2P12.65 2P54.2825
 UNIT 23
 COM='ARRAY FOR EAST AND WEST REFLECTORS FOR SOUTH REFLECTOR'
 ARRAY 6 3*0.0
 UNIT 24
 COM='NORTH TOP REFLECTOR WITH TRIS'
 CUBOID 5 1 2P28.35 2P64.05 2P12.15
 UNIT 25
 COM='ARRAY FOR NORTH TOP REFLECTOR'
 ARRAY 7 3*0.0

Table A.3 (continued)

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UNIT 26
COM='SOUTH TOP REFLECTOR WITH TRIS'
CUBOID 0 1 2P5.1 2P2.55 2P12.15
CUBOID 5 1 69.4 -5.1 2P64.05 2P12.15
UNIT 27
COM='ARRAY FOR SOUTH TOP REFLECTOR'
ARRAY 8 3*0.0
UNIT 28
COM='NORTH END REFLECTOR 9.8CM PORTION WITHOUT TRIS'
CUBOID 4 1 2P4.9000 2P64.0500 2P54.2825
UNIT 29
COM='NORTH END REFLECTOR 5.2 CM PORTION WITH TRIS'
CUBOID 5 1 2P2.6 2P64.0500 2P54.2825
UNIT 30
COM='NORTH END REFLECTOR 10.1 CM PORTION WITHOUT TRIS'
CUBOID 4 1 2P5.05 2P64.05 2P54.2825
UNIT 31
COM='ARRAY FOR NORTH END REFLECTOR'
ARRAY 9 3*0.0
UNIT 32
COM='SOUTH END REFLECTOR'
CUBOID 5 1 2P12.55 2P64.05 2P54.2825
UNIT 33
COM='ARRAY FOR SOUTH END REFLECTOR'
ARRAY 10 3*0.0
UNIT 34
COM='12.95 THICK MODERATING PLASTIC NORTH CORE'
CUBOID 6 1 2P15.7945 2P6.4750 2P32.0535
UNIT 35
COM='2.95 THICK MODERATING PLASTIC NORTH CORE'
CUBOID 6 1 2P15.7945 2P38.5285 2P1.475
UNIT 36
ARRAY 11 3*0.0
UNIT 37
ARRAY 12 3*0.0
REPLICATE 0 1 0.0 0.011 0.443 0.0 0.1590 0.0 1
UNIT 38
COM='NORTH CORE WITH BOTTOM REFLECTOR'
ARRAY 13 3* 0.0
UNIT 39
COM='NORTH CORE WITH EAST AND WEST REFLECTOR'
ARRAY 14 3*0.0
UNIT 40
COM='NORTH CORE WITH END REFLECTOR'
ARRAY 15 3*0.0
UNIT 41
COM='NORTH SPLIT TABLE FACEPLATE'
CUBOID 3 1 2P0.6150 2P64.0500 2P66.4325
UNIT 42
COM='NORTH CORE WITH TOP REFLECTOR'
ARRAY 16 3*0.0
UNIT 43
COM='NORTH CORE WITH FACEPLATE'
ARRAY 17 3*0.0
UNIT 44
COM='12.95 CM THICK MODERATOR SOUTH CORE'
CUBOID 6 1 2P23.924 2P6.475 2P32.0535
UNIT 45
COM='2.95 THICK MODERATOR SOUTH CORE'
CUBOID 6 1 2P23.924 2P38.5285 2P1.475
UNIT 46
COM='COMBINATION OF CORE WITH 12.95 THICK MODERATOR'
ARRAY 18 3*0.0

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UNIT 47
COM='COMBINATION OF CORE WITH 2.95 THICK MODERATOR'
ARRAY 19 3*0.0
REPLICATE 0 1 1.552 0.0 0.4430 0.0 0.159 0.0 1
UNIT 48
COM='SOUTH CORE WITH EAST WEST REFLECTORS'
ARRAY 20 3*0.0
UNIT 49
COM='SOUTH CORE WITH EAST WEST REFLECTORS'
ARRAY 21 3*0.0
UNIT 50
COM='SOUTH CORE END REFLECTOR'
ARRAY 22 3*0.0
UNIT 51
COM='FACEPLATE FOR SOUTH SPLIT TABLE'
CUBOID 3 1 2P0.4620 2P64.0500 2P66.4325
UNIT 52
COM='SOUTH CORE WITH TOP REFLECTOR'
ARRAY 23 3*0.0
UNIT 53
COM='SOUTH CORE WITH FACEPLATE'
ARRAY 24 3*0.0
UNIT 54
COM='AIR GAP'
CUBOID 0 1 2P0.7805 2P64.0500 2P66.4325
GLOBAL
UNIT 55
COM='TOTAL'
ARRAY 25 3*0.0
UNIT 56
COM='NORTH BOTTOM MODERATOR'
CUBOID 6 1 2P15.8000 2P38.7500 2P8.1295
UNIT 57
COM='BOTTOM SOUTH MODERATOR'
CUBOID 6 1 2P24.700 2P38.75 2P8.1295
UNIT 58
COM='SOUTH REAR MODERATOR'
CUBOID 3 1
END GEOMETRY
READ ARRAY
ARA=1 NUX=3 NUY=7 NUZ=7
COM='NORTH SPLIT TABLE CORE'
FILL 1 2 1 3 5 3 2Q6 1 2 1
      4 7 4 6 8 6 2Q6 4 7 4
      2Q42
      1 2 1 3 5 3 2Q6 1 2 1 END FILL
ARA=2 NUX=5 NUY=7 NUZ=7
COM='SOUTH SPLIT TABLE CORE'
FILL 1 2 1 2 1 3 5 3 5 3 2Q10 1 2 1 2 1
      4 7 4 7 4 6 8 6 8 6 2Q10 4 7 4 7 4
      2Q70
      1 2 1 2 1 3 5 3 5 3 2Q10 1 2 1 2 1 END FILL
ARA=3 NUX=1 NUY=1 NUZ=4
COM='NORTH BOTTOM MODERATOR AND REFLECTOR'
FILL 14 11 13 56 END FILL
ARA=4 NUX=1 NUY=1 NUZ=8
COM='SOUTH BOTTOM MODERATOR AND REFLECTOR'
FILL 18 16 17 16 16 17 17 57 END FILL
ARA=5 NUX=1 NUY=1 NUZ=1
COM='EAST AND WEST WALLS OF NORTH REFLECTOR'
FILL 20 END FILL
ARA=6 NUX=1 NUY=1 NUZ=1
COM='EAST AND WEST WALLS OF SOUTH REFLECTOR'
FILL 22 END FILL

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Table A.3 (continued)

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ARA=7  NUX=1  NUY=1  NUZ=1
COM='ARRAY FOR NORTH TOP REFLECTOR'
FILL 24  END FILL
ARA=8  NUX=1  NUY=1  NUZ=1
COM='ARRAY FOR SOUTH TOP REFLECTOR'
FILL 26  END FILL
ARA=9  NUX=3  NUY=1  NUZ=1
COM='ARRAY FOR NORTH END REFLECTOR'
FILL 28 29 30  END FILL
ARA=10 NUX=1  NUY=1  NUZ=1
COM='ARRAY FOR SOUTH END REFLECTOR'
FILL 32  END FILL
ARA=11 NUX=1  NUY=2  NUZ=1
COM='COMBINARION OF CORE WITH 12.95CM THICK MODERATOR'
FILL 9 34  END FILL
ARA=12 NUX=1  NUY=1  NUZ=2
COM='COMBINATION OF PREVIOUS ARRAY WITH 2.95CM THICK MODERATOR'
FILL 36 35  END FILL
ARA=13 NUX=1  NUY=1  NUZ=2
COM='COMBINATION OF NORTH CORE WITH BOTTOM REFLECTOR'
FILL 15 37  END FILL
ARA=14 NUX=1  NUY=3  NUZ=1
COM='NORTH CORE WITH SIDE REFLECTORS'
FILL 21 38 21  END FILL
ARA=15 NUX=2  NUY=1  NUZ=1
COM='NORTH CORE WITH END REFLECTOR'
FILL 31 39  END FILL
ARA=16 NUX=1  NUY=1  NUZ=2
COM='NORTH CORE WITH TOP REFLECTOR'
FILL 40 25  END FILL
ARA=17 NUX=2  NUY=1  NUZ=1
COM='NORTH CORE WITH FACEPLATE'
FILL 42 41  END FILL
ARA=18 NUX=1  NUY=2  NUZ=1
COM='COMBINATION OF S. CORE WITH 12.95 CM THICK MODERATOR'
FILL 10 44  END FILL
ARA=19 NUX=1  NUY=1  NUZ=2
COM='COMBINATION OF CORE WITH 2.95 CM THICK MODERATOR'
FILL 46 45  END FILL
ARA=20 NUX=1  NUY=1  NUZ=2
COM='SOUTH CORE WITH BOTTOM REFLECTOR'
FILL 19 47  END FILL
ARA=21 NUX=1  NUY=3  NUZ=1
COM='SOUTH CORE WITH EAST WEST REFLECTORS'
FILL 23 48 23  END FILL
ARA=22 NUX=2  NUY=1  NUZ=1
COM='SOUTH CORE WITH END REFLECTOR'
FILL 49 33  END FILL
ARA=23 NUX=1  NUY=1  NUZ=2
COM='COMBINATION OF CORE WITH TOP REFLECTOR'
FILL 50 27  END FILL
ARA=24 NUX=2  NUY=1  NUZ=1
COM='SOUTH CORE WITH FACEPLATE'
FILL 51 52  END FILL
ARA=25 NUX=3  NUY=1  NUZ=1
COM='TOTAL'
FILL 43 54 53  END FILL
END ARRAY
READ PLOT TTL='XZ SLICE OF RFP3 SHOWING MATERIAL REGIONS'
XUL=-1  YUL=64.05  ZUL=135
XLR=136 YLR=64.05  ZLR=-2
UAX=1  WDN=-1  NAX=130  NCH='0123456'END
TTL='YZ SLICE OF NORTH CORE SECOND ROW'
XUL=28  YUL=-2  ZUL=136

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XLR=28  YLR=136  ZLR=-2
VAX=1  WDN=-1  NAX=130  NCH='0123456'END
TTL='YZ SLICE OF SOUTH CORE SECOND ROW'
XUL=80  YUL=-2  ZUL=136
XLR=80  YLR=136  ZLR=-2
VAX=1  WDN=-1  NAX=130  NCH='0123456'
END PLOT
END DATA
END

CAR14
=CSAS25
ROCKY FLATS CRITICALS NUREG/CR-1653 EXPERIMENT NUMBER ? (27 GROUP MODEL)
' FUEL CUBE 15.28 CM, U(4.46)308 @ H/U=1.25, HI CONC. SOLUTION DRIVEN
27GROUPNDF4  INFHOMMEDIUM
U308 1 5.4078E-1 293.0 92234 0.03 92235 4.46 92236 0.08 92238 95.43 END
H2O 1 1.5627E-1 END
ARBM-BAGGIE 1.0 3 0 0 0 1001 14.01 6012 84.9 8016 1.20 1 1.9134E-2
END
ARBM-AL1100 1.0 3 0 0 1 13027 99.18 26000 0.5 29000 0.2 2 9.5390E-1
END
ARBM-TAPE(VINYL) 1.0 7 0 0 0 1001 5.92 6012 45.91 8016 10.82 17000
25.73 20040 6.9 22000 1.6 82000 1.1 2 1.1115E-2 END
ARBM-TAPE(MYLAR) 1.0 3 0 0 0 1001 6.83 6012 65.50 8016 27.02 2
1.7491E-2 END
ARBM-MODERATOR 1.185 3 0 0 0 1001 7.83 6012 59.49 8016 32.48 3 END
ARBM-FLEX(REG) 1.0 3 0 0 0 1001 7.84 6012 59.59 8016 32.23 4
1.1773 END
ARBM-FLEX(PAPER) 1.0 3 0 0 0 1001 6.48 6012 42.17 8016 49.5 4
3.7534E-3 END
ARBM-FLEX(GLUE) 1.0 3 0 0 0 1001 11.67 6012 86.29 8016 1.20 4
1.1648E-3 END
ARBM-FLEX(TRIS) 1.0 8 0 0 1 1001 7.16 6012 52.03 7014 0.16 8016 29.82
15031 1.02 17000 1.81 35079 4.260 35081 2.840 5 1.2757 END
ARBM-FLEX(PAPER) 1.0 3 0 0 0 1001 6.48 6012 42.17 8016 49.5 5
3.7534E-3 END
ARBM-FLEX(GLUE) 1.0 3 0 0 0 1001 11.67 6012 86.29 8016 1.20 5
1.1648E-3 END
ARBM-FILLER 1.185 3 0 0 0 1001 7.83 6012 59.49 8016 32.48 6 0.7 END
' THIS MATERIAL IS ACTUALLY MODERATOR ADJUSTED FOR THE VOLUME
' FRACTION OF THE VOID FILLED BETWEEN CORE AND REFLECTOR.
ARBM-AL1100 1.0 3 0 0 1 13027 99.18 26000 0.5 29000 0.2 7 2.715 END
SOLNUO2(NO3)2 8 351.18 0.549 1.0 293.0 92234 1.022 92235 93.172
92236 0.434 92238 5.372 END
SS304 9 1.0 END
END COMP
ROCKY FLATS CRITICALS NUREG/CR-1653 EXPERIMENT NUMBER ? (27 GROUP MODEL)
' FUEL CUBE 15.28 CM, U(4.46)308 @ H/U=1.25, HI CONC. SOLUTION DRIVEN
READ PARM NPG=600 NUB=YES FDN=YES PLT=NO END PARM
READ GEOM
UNIT 1
COM='FUEL BOX WITH VOID AND PART OF AL BOX'
CUBOID 0 1 9.80 0.0 3.75 0.0 14.98 0.0
CUBOID 2 1 9.95 0.0 3.90 -0.15 14.98 0.0
CUBOID 1 1 14.98 0.0 9.365 -5.615 14.98 0.0
UNIT 2
COM='FRONT OF FUEL BOX'
CUBOID 2 1 0.15 0.0 5.615 0.0 14.98 0.0
CUBOID 0 1 0.15 0.0 9.365 0.0 14.98 0.0
CUBOID 2 1 0.15 0.0 14.98 0.0 14.98 0.0

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Table A.3 (continued)

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UNIT 3
COM='REAR OF FUEL BOX'
CUBOID 2 1 0.15 0.0 14.98 0.0 14.98 0.0
UNIT 4
COM='ARRAY TO ASSEMBLE PART OF BOX'
ARRAY 26 3*0
UNIT 5
COM='TOP AND BOTTOM OF BOX'
CUBOID 0 1 9.80 0.0 3.750 0.0 0.15 0.0
CUBOID 2 1 15.28 0.0 9.365 -5.615 0.15 0.0
GLOBAL
UNIT 6
COM='ARRAY TO ASSEMBLE TOP AND BOTTOM'
ARRAY 27 3*0
CUBOID 2 1 15.28 0.0 15.13 -0.15 15.28 0.0
CUBOID 0 1 15.305 -0.025 15.155 -0.175 15.305 -0.025
UNIT 7
COM='FUEL BOX 15.28 CM ON A SIDE WITH .15 CM WALLS .05CM STACKING VOID'
CUBOID 1 1 6P7.49
CUBOID 2 1 6P7.64
CUBOID 0 1 6P7.6650
UNIT 34
COM='ALUMINUM WEIGHT DISTRIBUTION PLATE FOR SPECIAL BOX'
CUBOID 0 1 9.80 0.0 3.750 0.0 0.16 0.0
CUBOID 7 1 15.33 0.0 9.54 -5.79 0.16 0.0
UNIT 35
COM='ALUMINUM WEIGHT DISTRIBUTION PLATE FOR BOXES'
CUBOID 7 1 4P7.665 0.16 0.0
UNIT 9
COM='NORTH SPLIT TABLE CORE'
ARRAY 1 3*0.0
CUBOID 0 1 30.66 -0.94 77.5 0.0 83.475 0.0
UNIT 10
COM='SOUTH SPLIT TABLE CORE'
ARRAY 2 3*0.0
CUBOID 0 1 49.4 0.0 77.5 0.0 83.475 0.0
UNIT 11
COM='PLEXIGLASS REFLECTOR SHEET WITHOUT TRIS, NORTH BOTTOM REFLECTOR'
CUBOID 4 1 2P15.8000 2P38.7500 2P0.6150
UNIT 12
COM='PLEXIGLASS REFLECTOR SHEET WITH TRIS, NORTH BOTTOM REFLECTOR'
CUBOID 5 1 2P15.8000 2P38.7500 2P0.6150
UNIT 13
COM='UPPER PORTION NORTH BOTTOM REFLECTOR WITH TRIS'
CUBOID 5 1 2P15.8 2P38.75 2P8.24
UNIT 14
COM='LOWER PORTION NORTH BOTTOM REFLECTOR WITH TRIS'
CUBOID 5 1 2P15.8 2P38.75 2P3.69
UNIT 15
COM='NORTH BOTTOM REFLECTOR INCLUDES REGULAR AND TRIS'
ARRAY 3 3*0.0
UNIT 16
COM='PLEXIGLAS SHEET BOTTOM SOUTH REFLECTOR WITHOUT TRIS'
CUBOID 0 1 2P5.1 2P2.5 2P0.6150
CUBOID 4 1 44.3 -5.1 2P38.75 2P0.615
UNIT 17
COM='PLEXIGLAS SHEET BOTTOM SOUTH REFLECTOR WITH TRIS'
CUBOID 0 1 2P5.1 2P2.5 2P0.6150
CUBOID 5 1 44.3 -5.1 2P38.75 2P0.6150
UNIT 18
COM='LOWER PORTION SOUTH BOTTOM REFLECTOR WITH TRIS'
CUBOID 0 1 2P5.1 2P2.5 2P8.855
CUBOID 5 1 44.3 -5.1 2P38.75 2P8.855

UNIT 19
COM='SOUTH BOTTOM REFLECTOR WITH REGULAR AND TRIS'
ARRAY 4 3*0.0
UNIT 20
COM='EAST AND WEST REFLECTORS FOR NORTH REFLECTOR WITH TRIS'
CUBOID 5 1 2P15.8 2P12.65 2P54.2825
UNIT 21
COM='ARRAY FOR EAST AND WEST REFLECTORS FOR NORTH REFLECTOR'
ARRAY 5 3*0.0
UNIT 22
COM='EAST AND WEST REFLECTORS FOR SOUTH REFLECTOR WITH TRIS'
CUBOID 5 1 2P24.700 2P12.65 2P54.2825
UNIT 23
COM='ARRAY FOR EAST AND WEST REFLECTORS FOR SOUTH REFLECTOR'
ARRAY 6 3*0.0
UNIT 24
COM='NORTH TOP REFLECTOR WITH TRIS'
CUBOID 5 1 2P28.35 2P64.05 2P12.15
UNIT 25
COM='ARRAY FOR NORTH TOP REFLECTOR'
ARRAY 7 3*0.0
UNIT 26
COM='SOUTH TOP REFLECTOR WITH TRIS'
CUBOID 0 1 2P5.1 2P2.5 2P12.15
CUBOID 5 1 69.4 -5.1 2P64.05 2P12.15
UNIT 27
COM='ARRAY FOR SOUTH TOP REFLECTOR'
ARRAY 8 3*0.0
UNIT 28
COM='NORTH END REFLECTOR 9.8CM PORTION WITHOUT TRIS'
CUBOID 4 1 2P4.9000 2P64.0500 2P54.2825
UNIT 29
COM='NORTH END REFLECTOR 5.2 CM PORTION WITH TRIS'
CUBOID 5 1 2P2.6 2P64.0500 2P54.2825
UNIT 30
COM='NORTH END REFLECTOR 10.1 CM PORTION WITHOUT TRIS'
CUBOID 4 1 2P5.05 2P64.05 2P54.2825
UNIT 31
COM='ARRAY FOR NORTH END REFLECTOR'
ARRAY 9 3*0.0
UNIT 32
COM='SOUTH END REFLECTOR'
CUBOID 5 1 2P12.55 2P64.05 2P54.2825
UNIT 33
COM='ARRAY FOR SOUTH END REFLECTOR'
ARRAY 10 3*0.0
UNIT 38
COM='NORTH CORE WITH BOTTOM REFLECTOR'
ARRAY 13 3* 0.0
UNIT 39
COM='NORTH CORE WITH EAST AND WEST REFLECTOR'
ARRAY 14 3*0.0
UNIT 40
COM='NORTH CORE WITH END REFLECTOR'
ARRAY 15 3*0.0
UNIT 42
COM='NORTH CORE WITH TOP REFLECTOR'
ARRAY 16 3*0.0
UNIT 48
COM='SOUTH CORE WITH BOTTOM REFLECTORS'
ARRAY 20 3*0.0

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Table A.3 (continued)

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UNIT 49
COM='SOUTH CORE WITH EAST WEST REFLECTORS'
ARRAY 21 3*0.0
UNIT 50
COM='SOUTH CORE END REFLECTOR'
ARRAY 22 3*0.0
UNIT 52
COM='SOUTH CORE WITH TOP REFLECTOR'
ARRAY 23 3*0.0
UNIT 54
COM='AIR GAP'
CUBOID 0 1 0.500 0.0 64.475 -63.625 69.13 -63.735
GLOBAL
UNIT 55
COM='TOTAL'
ARRAY 25 3*0.0
UNIT 56
COM='COMBINATION OF TWO REGULAR FUEL BOXES'
ARRAY 28 3*0.0
UNIT 57
COM='COMBINATION OF REGULAR FUEL BOX AND SPECIAL FUEL BOX'
ARRAY 29 3*0.0
UNIT 58
COM='COMBINATION OF TWO REGULAR WEIGHT DISTRIBUTION PLATES'
ARRAY 30 3*0.0
UNIT 59
COM='COMBINATION OF REGULAR AND SPECIAL WEIGHT DISTRIBUTION PLATES'
ARRAY 31 3*0.0
UNIT 60
COM='NORTH CORE SOLUTION DRIVER'
CUBOID 8 1 2P7.5 2P14.9 1.763 -7.5
CUBOID 0 1 2P7.5 2P14.9 2P7.5
CUBOID 9 1 2P7.65 2P15.05 2P7.65
CUBOID 0 1 2P7.665 2P15.33 2P7.665
UNIT 61
COM='SOUTH CORE SOLUTION DRIVER'
CUBOID 8 1 2P7.5 2P14.9 1.695 -7.5
CUBOID 0 1 2P7.5 2P14.9 2P7.5
CUBOID 9 1 2P7.65 2P15.05 2P7.65
CUBOID 0 1 2P7.665 2P15.33 2P7.665
END GEOMETRY
READ ARRAY
ARA=1 NUX=2 NUY=4 NUZ=9
COM='NORTH SPLIT TABLE CORE'
FILL 2R7 2R56 4R7
      2R35 2R58 4R35
      2R7 2R56 4R7
      2R35 2R58 4R35
      2R7 56 60 4R7
      2R35 2R58 4R35
      2R7 2R56 4R7
      2R35 2R58 4R35
      2R7 2R56 4R7
END FILL
ARA=2 NUX=3 NUY=4 NUZ=9
COM='SOUTH SPLIT TABLE CORE'
FILL 3R7 3R56 6R7
      3R35 3R58 6R35
      3R7 3R56 6R7
      3R35 3R58 6R35
      3R7 61 56 56 6R7
      3R35 3R58 6R35
      3R7 57 56 56 6R7
      3R35 59 58 58 6R35
      3R7 57 56 56 6R7

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END FILL
ARA=3 NUX=1 NUY=1 NUZ=3
COM='NORTH BOTTOM REFLECTOR'
FILL 14 11 13 END FILL
ARA=4 NUX=1 NUY=1 NUZ=7
COM='SOUTH BOTTOM REFLECTOR'
FILL 18 16 17 16 16 17 17 END FILL
ARA=5 NUX=1 NUY=1 NUZ=1
COM='EAST AND WEST WALLS OF NORTH REFLECTOR'
FILL 20 END FILL
ARA=6 NUX=1 NUY=1 NUZ=1
COM='EAST AND WEST WALLS OF SOUTH REFLECTOR'
FILL 22 END FILL
ARA=7 NUX=1 NUY=1 NUZ=1
COM='ARRAY FOR NORTH TOP REFLECTOR'
FILL 24 END FILL
ARA=8 NUX=1 NUY=1 NUZ=1
COM='ARRAY FOR SOUTH TOP REFLECTOR'
FILL 26 END FILL
ARA=9 NUX=3 NUY=1 NUZ=1
COM='ARRAY FOR NORTH END REFLECTOR'
FILL 28 29 30 END FILL
ARA=10 NUX=1 NUY=1 NUZ=1
COM='ARRAY FOR SOUTH END REFLECTOR'
FILL 32 END FILL
ARA=13 NUX=1 NUY=1 NUZ=2
COM='COMBINATION OF NORTH CORE WITH BOTTOM REFLECTOR'
FILL 15 9 END FILL
ARA=14 NUX=1 NUY=3 NUZ=1
COM='NORTH CORE WITH SIDE REFLECTORS'
FILL 21 38 21 END FILL
ARA=15 NUX=2 NUY=1 NUZ=1
COM='NORTH CORE WITH END REFLECTOR'
FILL 31 39 END FILL
ARA=16 NUX=1 NUY=1 NUZ=2
COM='NORTH CORE WITH TOP REFLECTOR'
FILL 40 25 END FILL
ARA=20 NUX=1 NUY=1 NUZ=2
COM='SOUTH CORE WITH BOTTOM REFLECTOR'
FILL 19 10 END FILL
ARA=21 NUX=1 NUY=3 NUZ=1
COM='SOUTH CORE WITH EAST WEST REFLECTORS'
FILL 23 48 23 END FILL
ARA=22 NUX=2 NUY=1 NUZ=1
COM='SOUTH CORE WITH END REFLECTOR'
FILL 49 33 END FILL
ARA=23 NUX=1 NUY=1 NUZ=2
COM='COMBINATION OF CORE WITH TOP REFLECTOR'
FILL 50 27 END FILL
ARA=25 NUX=3 NUY=1 NUZ=1
COM='TOTAL'
FILL 42 54 52 END FILL
ARA=26 NUX=3 NUY=1 NUZ=1
COM='ASSEMBLY OF FUEL BOX FRONT AND REAR'
FILL 2 1 3 END FILL
ARA=27 NUX=1 NUY=1 NUZ=3
COM='ASSEMBLY OF FUEL BOX TOP AND BOTTOM'
FILL 5 4 5 END FILL
ARA=28 NUX=1 NUY=2 NUZ=1
COM='COMBINATION OF TWO FUEL BOXES'
FILL 7 7 END FILL
ARA=29 NUX=1 NUY=2 NUZ=1
COM='COMBINATION OF SPECIAL AND REGULAR FUEL BOXES'
FILL 7 6 END FILL

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Table A.3 (continued)

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ARA=30 NUX=1 NUY=2 NUZ=1
COM='COMBINATION OF TWO WEIGHT DISTRIBUTION PLATES'
FILL 35 35 END FILL
ARA=31 NUX=1 NUY=2 NUZ=1
COM='COMBINATION OF SPECIAL AND REGULAR WEIGHT DISTRIBUTION PLATES'
FILL 35 34 END FILL
END ARRAY
READ PLOT TTL='YZ SLICE OF SOUTH CORE FIRST ROW'
XUL=64.319 YUL=40.000 ZUL=72.000
XLR=64.319 YLR=72.000 ZLR=56.000
VAX=1 WDN=-1 NAX=130 NCH='012345678'END
TTL='XZ SLICE OF SPHERE CUBOID'
XUL=56.0 YUL=63.625 ZUL=71.735
XLR=72.0 YLR=63.625 ZLR=55.735
UAX=1 WDN=-1 NAX=130 NCH='012345678'
END PLOT
READ START NST=1 XSM=41.37 XSP=72.894 YSM=40.63 YSP=71.29
ZSM=56.071 ZSP=71.4 END START
END DATA
END

CAR15
-CSAS25
ROCKY FLATS CRITICALS NUREG/CR-1653 EXPERIMENT NUMBER ? (27 GROUP MODEL)
' FUEL CUBE 15.28 CM, U(4.46)308 @ H/U=1.25, HI CONC. SOLUTION DRIVEN
27GROUPNDF4 INFHOMMEDIUM
U308 1 5.4078E-1 293.0 92234 0.03 92235 4.46 92236 0.08 92238 95.43 END
H2O 1 1.5627E-1 END
ARBM-BAGGIE 1.0 3 0 0 0 1001 14.01 6012 84.9 8016 1.20 1 1.9134E-2
END
ARBM-AL1100 1.0 3 0 0 1 13027 99.18 26000 0.5 29000 0.2 2 9.5390E-1
END
ARBM-TAPE(VINYL) 1.0 7 0 0 0 1001 5.92 6012 45.91 8016 10.82 17000
25.73 20040 6.9 22000 1.6 82000 1.1 2 1.1115E-2 END
ARBM-TAPE(MYLAR) 1.0 3 0 0 0 1001 6.83 6012 65.50 8016 27.02 2
1.7491E-2 END
ARBM-MODERATOR 1.185 3 0 0 0 1001 7.83 6012 59.49 8016 32.48 3 END
ARBM-PLEX(REG) 1.0 3 0 0 0 1001 7.84 6012 59.59 8016 32.23 4
1.1773 END
ARBM-PLEX(PAPER) 1.0 3 0 0 0 1001 6.48 6012 42.17 8016 49.5 4
3.7534E-3 END
ARBM-PLEX(GLUE) 1.0 3 0 0 0 1001 11.67 6012 86.29 8016 1.20 4
1.1648E-3 END
ARBM-PLEX(TRIS) 1.0 8 0 0 1 1001 7.16 6012 52.03 7014 0.16 8016 29.82
15031 1.02 17000 1.81 35079 4.260 35081 2.840 5 1.2757 END
ARBM-PLEX(PAPER) 1.0 3 0 0 0 1001 6.48 6012 42.17 8016 49.5 5
3.7534E-3 END
ARBM-PLEX(GLUE) 1.0 3 0 0 0 1001 11.67 6012 86.29 8016 1.20 5
1.1648E-3 END
ARBM-FILLER 1.185 3 0 0 0 1001 7.83 6012 59.49 8016 32.48 6 0.7 END
' THIS MATERIAL IS ACTUALLY MODERATOR ADJUSTED FOR THE VOLUME
' FRACTION OF THE VOID FILLED BETWEEN CORE AND REFLECTOR.
ARBM-AL1100 1.0 3 0 0 1 13027 99.18 26000 0.5 29000 0.2 7 2.715 END
SOLNUO2(NO3)2 8 351.18 0.549 1.0 293.0 92234 1.022 92235 93.172
92236 0.434 92238 5.372 END
SS304 9 1.0 END
END COMP
ROCKY FLATS CRITICALS NUREG/CR-1653 EXPERIMENT NUMBER ? (27 GROUP MODEL)
' FUEL CUBE 15.28 CM, U(4.46)308 @ H/U=1.25, HI CONC. SOLUTION DRIVEN
READ PARM NPG=600 NUB=YES FDN=YES PLT=NO END PARM
READ GEOM

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UNIT 1
COM='FUEL BOX WITH VOID AND PART OF AL BOX'
CUBOID 0 1 9.80 0.0 3.75 0.0 14.98 0.0
CUBOID 2 1 9.95 0.0 3.90 -0.15 14.98 0.0
CUBOID 1 1 14.98 0.0 9.365 -5.615 14.98 0.0
UNIT 2
COM='FRONT OF FUEL BOX'
CUBOID 2 1 0.15 0.0 5.615 0.0 14.98 0.0
CUBOID 0 1 0.15 0.0 9.365 0.0 14.98 0.0
CUBOID 2 1 0.15 0.0 14.98 0.0 14.98 0.0
UNIT 3
COM='REAR OF FUEL BOX'
CUBOID 2 1 0.15 0.0 14.98 0.0 14.98 0.0
UNIT 4
COM='ARRAY TO ASSEMBLE PART OF BOX'
ARRAY 26 3*0
UNIT 5
COM='TOP AND BOTTOM OF BOX'
CUBOID 0 1 9.80 0.0 3.750 0.0 0.15 0.0
CUBOID 2 1 15.28 0.0 9.365 -5.615 0.15 0.0
GLOBAL
UNIT 6
COM='ARRAY TO ASSEMBLE TOP AND BOTTOM'
ARRAY 27 3*0
CUBOID 2 1 15.28 0.0 15.13 -0.15 15.28 0.0
CUBOID 0 1 15.305 -0.025 15.155 -0.175 15.305 -0.025
UNIT 7
COM='FUEL BOX 15.28 CM ON A SIDE WITH .15 CM WALLS .05CM STACKING VOID'
CUBOID 1 1 6P7.49
CUBOID 2 1 6P7.64
CUBOID 0 1 6P7.6650
UNIT 34
COM='ALUMINUM WEIGHT DISTRIBUTION PLATE FOR SPECIAL BOX'
CUBOID 0 1 9.80 0.0 3.750 0.0 0.16 0.0
CUBOID 7 1 15.33 0.0 9.54 -5.79 0.16 0.0
UNIT 35
COM='ALUMINUM WEIGHT DISTRIBUTION PLATE FOR BOXES'
CUBOID 7 1 4P7.665 0.16 0.0
UNIT 9
COM='NORTH SPLIT TABLE CORE'
ARRAY 1 3*0.0
CUBOID 0 1 30.66 -0.94 77.5 0.0 83.475 0.0
UNIT 10
COM='SOUTH SPLIT TABLE CORE'
ARRAY 2 3*0.0
CUBOID 0 1 49.4 0.0 77.5 0.0 83.475 0.0
UNIT 11
COM='PLEXIGLASS REFLECTOR SHEET WITHOUT TRIS, NORTH BOTTOM REFLECTOR'
CUBOID 4 1 2P15.8000 2P38.7500 2P0.6150
UNIT 12
COM='PLEXIGLASS REFLECTOR SHEET WITH TRIS, NORTH BOTTOM REFLECTOR'
CUBOID 5 1 2P15.8000 2P38.7500 2P0.6150
UNIT 13
COM='UPPER PORTION NORTH BOTTOM REFLECTOR WITH TRIS'
CUBOID 5 1 2P15.8 2P38.75 2P8.24
UNIT 14
COM='LOWER PORTION NORTH BOTTOM REFLECTOR WITH TRIS'
CUBOID 5 1 2P15.8 2P38.75 2P3.69
UNIT 15
COM='NORTH BOTTOM REFLECTOR INCLUDES REGULAR AND TRIS'
ARRAY 3 3*0.0

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Table A.3 (continued)

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UNIT 16
COM='PLEXIGLAS SHEET BOTTOM SOUTH REFLECTOR WITHOUT TRIS'
CUBOID 0 1 2P5.1 2P2.5 2P0.6150
CUBOID 4 1 44.3 -5.1 2P38.75 2P0.615
UNIT 17
COM='PLEXIGLAS SHEET BOTTOM SOUTH REFLECTOR WITH TRIS'
CUBOID 0 1 2P5.1 2P2.5 2P0.6150
CUBOID 5 1 44.3 -5.1 2P38.75 2P0.6150
UNIT 18
COM='LOWER PORTION SOUTH BOTTOM REFLECTOR WITH TRIS'
CUBOID 0 1 2P5.1 2P2.5 2P8.855
CUBOID 5 1 44.3 -5.1 2P38.75 2P8.855
UNIT 19
COM='SOUTH BOTTOM REFLECTOR WITH REGULAR AND TRIS'
ARRAY 4 3*0.0
UNIT 20
COM='EAST AND WEST REFLECTORS FOR NORTH REFLECTOR WITH TRIS'
CUBOID 5 1 2P15.8 2P12.65 2P54.2825
UNIT 21
COM='ARRAY FOR EAST AND WEST REFLECTORS FOR NORTH REFLECTOR'
ARRAY 5 3*0.0
UNIT 22
COM='EAST AND WEST REFLECTORS FOR SOUTH REFLECTOR WITH TRIS'
CUBOID 5 1 2P24.700 2P12.65 2P54.2825
UNIT 23
COM='ARRAY FOR EAST AND WEST REFLECTORS FOR SOUTH REFLECTOR'
ARRAY 6 3*0.0
UNIT 24
COM='NORTH TOP REFLECTOR WITH TRIS'
CUBOID 5 1 2P28.35 2P64.05 2P12.15
UNIT 25
COM='ARRAY FOR NORTH TOP REFLECTOR'
ARRAY 7 3*0.0
UNIT 26
COM='SOUTH TOP REFLECTOR WITH TRIS'
CUBOID 0 1 2P5.1 2P2.5 2P12.15
CUBOID 5 1 69.4 -5.1 2P64.05 2P12.15
UNIT 27
COM='ARRAY FOR SOUTH TOP REFLECTOR'
ARRAY 8 3*0.0
UNIT 28
COM='NORTH END REFLECTOR 9.8CM PORTION WITHOUT TRIS'
CUBOID 4 1 2P4.9000 2P64.0500 2P54.2825
UNIT 29
COM='NORTH END REFLECTOR 5.2 CM PORTION WITH TRIS'
CUBOID 5 1 2P2.6 2P64.0500 2P54.2825
UNIT 30
COM='NORTH END REFLECTOR 10.1 CM PORTION WITHOUT TRIS'
CUBOID 4 1 2P5.05 2P64.05 2P54.2825
UNIT 31
COM='ARRAY FOR NORTH END REFLECTOR'
ARRAY 9 3*0.0
UNIT 32
COM='SOUTH END REFLECTOR'
CUBOID 5 1 2P12.55 2P64.05 2P54.2825
UNIT 33
COM='ARRAY FOR SOUTH END REFLECTOR'
ARRAY 10 3*0.0
UNIT 38
COM='NORTH CORE WITH BOTTOM REFLECTOR'
ARRAY 13 3* 0.0

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UNIT 39
COM='NORTH CORE WITH EAST AND WEST REFLECTOR'
ARRAY 14 3*0.0
UNIT 40
COM='NORTH CORE WITH END REFLECTOR'
ARRAY 15 3*0.0
UNIT 42
COM='NORTH CORE WITH TOP REFLECTOR'
ARRAY 16 3*0.0
UNIT 48
COM='SOUTH CORE WITH BOTTOM REFLECTORS'
ARRAY 20 3*0.0
UNIT 49
COM='SOUTH CORE WITH EAST WEST REFLECTORS'
ARRAY 21 3*0.0
UNIT 50
COM='SOUTH CORE END REFLECTOR'
ARRAY 22 3*0.0
UNIT 52
COM='SOUTH CORE WITH TOP REFLECTOR'
ARRAY 23 3*0.0
UNIT 54
COM='AIR GAP'
CUBOID 0 1 0.732 0.0 64.475 -63.625 69.13 -63.735
GLOBAL
UNIT 55
COM='TOTAL'
ARRAY 25 3*0.0
UNIT 56
COM='COMBINATION OF TWO REGULAR FUEL BOXES'
ARRAY 28 3*0.0
UNIT 57
COM='COMBINATION OF REGULAR FUEL BOX AND SPECIAL FUEL BOX'
ARRAY 29 3*0.0
UNIT 58
COM='COMBINATION OF TWO REGULAR WEIGHT DISTRIBUTION PLATES'
ARRAY 30 3*0.0
UNIT 59
COM='COMBINATION OF REGULAR AND SPECIAL WEIGHT DISTRIBUTION PLATES'
ARRAY 31 3*0.0
UNIT 60
COM='NORTH CORE SOLUTION DRIVER'
CUBOID 8 1 2P7.5 2P14.9 1.863 -7.5
CUBOID 0 1 2P7.5 2P14.9 2P7.5
CUBOID 9 1 2P7.65 2P15.05 2P7.65
CUBOID 0 1 2P7.665 2P15.33 2P7.665
UNIT 61
COM='SOUTH CORE SOLUTION DRIVER'
CUBOID 8 1 2P7.5 2P14.9 1.794 -7.5
CUBOID 0 1 2P7.5 2P14.9 2P7.5
CUBOID 9 1 2P7.65 2P15.05 2P7.65
CUBOID 0 1 2P7.665 2P15.33 2P7.665
END GEOMETRY
READ ARRAY
ARA=1 NUX=2 NUZ=4 NUZ=9
COM='NORTH SPLIT TABLE CORE'
FILL 2R7 2R56 4R7
2R35 2R58 4R35
2R7 2R56 4R7
2R35 2R58 4R35
2R7 56 60 4R7
2R35 2R58 4R35
2R7 2R56 4R7
2R35 2R58 4R35
2R7 2R56 4R7
END FILL

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Table A.3 (continued)

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ARA=2  NUX=3  NUY=4  NUZ=9
COM='SOUTH SPLIT TABLE CORE'
FILL  3R7  3R56  6R7
      3R35  3R58  6R35
      3R7  3R56  6R7
      3R35  3R58  6R35
      3R7  61  56  56  6R7
      3R35  3R58  6R35
      3R7  57  56  56  6R7
      3R35  59  58  58  6R35
      3R7  57  56  56  6R7
END FILL
ARA=3  NUX=1  NUY=1  NUZ=3
COM='NORTH BOTTOM REFLECTOR'
FILL  14  11  13  END FILL
ARA=4  NUX=1  NUY=1  NUZ=7
COM='SOUTH BOTTOM REFLECTOR'
FILL  18  16  17  16  17  17  END FILL
ARA=5  NUX=1  NUY=1  NUZ=1
COM='EAST AND WEST WALLS OF NORTH REFLECTOR'
FILL  20  END FILL
ARA=6  NUX=1  NUY=1  NUZ=1
COM='EAST AND WEST WALLS OF SOUTH REFLECTOR'
FILL  22  END FILL
ARA=7  NUX=1  NUY=1  NUZ=1
COM='ARRAY FOR NORTH TOP REFLECTOR'
FILL  24  END FILL
ARA=8  NUX=1  NUY=1  NUZ=1
COM='ARRAY FOR SOUTH TOP REFLECTOR'
FILL  26  END FILL
ARA=9  NUX=3  NUY=1  NUZ=1
COM='ARRAY FOR NORTH END REFLECTOR'
FILL  28  29  30  END FILL
ARA=10 NUX=1  NUY=1  NUZ=1
COM='ARRAY FOR SOUTH END REFLECTOR'
FILL  32  END FILL
ARA=13 NUX=1  NUY=1  NUZ=2
COM='COMBINATION OF NORTH CORE WITH BOTTOM REFLECTOR'
FILL  15  9  END FILL
ARA=14 NUX=1  NUY=3  NUZ=1
COM='NORTH CORE WITH SIDE REFLECTORS'
FILL  21  38  21  END FILL
ARA=15 NUX=2  NUY=1  NUZ=1
COM='NORTH CORE WITH END REFLECTOR'
FILL  31  39  END FILL
ARA=16 NUX=1  NUY=1  NUZ=2
COM='NORTH CORE WITH TOP REFLECTOR'
FILL  40  25  END FILL
ARA=20 NUX=1  NUY=1  NUZ=2
COM='SOUTH CORE WITH BOTTOM REFLECTOR'
FILL  19  10  END FILL
ARA=21 NUX=1  NUY=3  NUZ=1
COM='SOUTH CORE WITH EAST WEST REFLECTORS'
FILL  23  48  23  END FILL
ARA=22 NUX=2  NUY=1  NUZ=1
COM='SOUTH CORE WITH END REFLECTOR'
FILL  49  33  END FILL
ARA=23 NUX=1  NUY=1  NUZ=2
COM='COMBINATION OF CORE WITH TOP REFLECTOR'
FILL  50  27  END FILL
ARA=25 NUX=3  NUY=1  NUZ=1
COM='TOTAL'
FILL  42  54  52  END FILL

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ARA=26 NUX=3  NUY=1  NUZ=1
COM='ASSEMBLY OF FUEL BOX FRONT AND REAR'
FILL  2  1  3  END FILL
ARA=27 NUX=1  NUY=1  NUZ=3
COM='ASSEMBLY OF FUEL BOX TOP AND BOTTOM'
FILL  5  4  5  END FILL
ARA=28 NUX=1  NUY=2  NUZ=1
COM='COMBINATION OF TWO FUEL BOXES'
FILL  7  7  END FILL
ARA=29 NUX=1  NUY=2  NUZ=1
COM='COMBINATION OF SPECIAL AND REGULAR FUEL BOXES'
FILL  7  6  END FILL
ARA=30 NUX=1  NUY=2  NUZ=1
COM='COMBINATION OF TWO WEIGHT DISTRIBUTION PLATES'
FILL  35  35  END FILL
ARA=31 NUX=1  NUY=2  NUZ=1
COM='COMBINATION OF SPECIAL AND REGULAR WEIGHT DISTRIBUTION PLATES'
FILL  35  34  END FILL
END ARRAY
READ PLOT TTL='YZ SLICE OF SOUTH CORE FIRST ROW'
XUL=64.319 YUL=40.000 ZUL=72.000
XLR=64.319 YLR=72.000 ZLR=56.000
VAX=1 WDN=-1 NAX=130 NCH='012345678' END
TTL='XZ SLICE OF SPHERE CUBOID'
XUL=56.0 YUL=63.625 ZUL=71.735
XLR=72.0 YLR=63.625 ZLR=55.735
UAX=1 WDN=-1 NAX=130 NCH='012345678'
END PLOT
' READ START NST=1 XSM=41.37 XSP=72.894 YSM=40.63 YSP=71.29
' ZSM=56.071 ZSP=71.4 END START
READ START NST=1 END START
END DATA
END

CAR16
=CSAS25
ROCKY PLATS CRITICALS NUREG/CR-1653 EXPERIMENT NUMBER ? (27 GROUP MODEL)
' FUEL CUBE 15.28 CM, U(4.46)308 @ H/U=1.25, LOW CONC. SOLUTION DRIVEN
27GROUPNDF4 INFHOMMEDIUM
U308 1 5.4078E-1 293.0 92234 0.03 92235 4.46 92236 0.08 92238 95.43 END
H2O 1 1.5627E-1 END
ARBM-BAGGIE 1.0 3 0 0 0 1001 14.01 6012 84.9 8016 1.20 1 1.9134E-2
END
ARBM-AL1100 1.0 3 0 0 1 13027 99.18 26000 0.5 29000 0.2 2 9.5390E-1
END
ARBM-TAPE(VINYL) 1.0 7 0 0 0 1001 5.92 6012 45.91 8016 10.82 17000
25.73 20040 6.9 22000 1.6 82000 1.1 2 1.1115E-2 END
ARBM-TAPE(MYLAR) 1.0 3 0 0 0 1001 6.83 6012 65.50 8016 27.02 2
1.7491E-2 END
ARBM-MODERATOR 1.185 3 0 0 0 1001 7.83 6012 59.49 8016 32.48 3 END
ARBM-PLEX(REG) 1.0 3 0 0 0 1001 7.84 6012 59.59 8016 32.23 4
1.1773 END
ARBM-PLEX(PAPER) 1.0 3 0 0 0 1001 6.48 6012 42.17 8016 49.5 4
3.7534E-3 END
ARBM-PLEX(GLUE) 1.0 3 0 0 0 1001 11.67 6012 86.29 8016 1.20 4
1.1648E-3 END
ARBM-PLEX(TRIS) 1.0 8 0 0 1 1001 7.16 6012 52.03 7014 0.16 8016 29.82
15031 1.02 17000 1.81 35079 4.260 35081 2.840 5 1.2757 END
ARBM-PLEX(PAPER) 1.0 3 0 0 0 1001 6.48 6012 42.17 8016 49.5 5
3.7534E-3 END

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Table A.3 (continued)

ARBM-PLEX(GLUE) 1.0 3 0 0 0 1001 11.67 6012 86.29 8016 1.20 5
 1.1648E-3 END
 ARBM-FILLER 1.185 3 0 0 0 1001 7.83 6012 59.49 8016 32.48 6 0.7 END
 ' THIS MATERIAL IS ACTUALLY MODERATOR ADJUSTED FOR THE VOLUME
 ' FRACTION OF THE VOID FILLED BETWEEN CORE AND REFLECTOR.
 ARBM-AL1100 1.0 3 0 0 1 13027 99.18 26000 0.5 29000 0.2 7 2.715 END
 SOLNUO2(NO3)2 8 86.42 0.149 1.0 293.0 92234 1.022 92235 93.172
 92236 0.434 92238 5.372 END
 SS304 9 1.0 END
 END COMP
 ROCKY FLATS CRITICALS NUREG/CR-1653 EXPERIMENT NUMBER ? (27 GROUP MODEL)
 ' FUEL CUBE 15.28 CM, U(4.46)308 @ H/U=1.25, LOW CONC. SOLUTION DRIVEN
 READ PARM NPG=600 NUB=YES FDN=YES PLT=YES END PARM
 READ GEOM
 UNIT 1
 COM='FUEL BOX WITH VOID AND PART OF AL BOX'
 CUBOID 0 1 9.80 0.0 3.75 0.0 14.98 0.0
 CUBOID 2 1 9.95 0.0 3.90 -0.15 14.98 0.0
 CUBOID 1 1 14.98 0.0 9.365 -5.615 14.98 0.0
 UNIT 2
 COM='FRONT OF FUEL BOX'
 CUBOID 2 1 0.15 0.0 5.615 0.0 14.98 0.0
 CUBOID 0 1 0.15 0.0 9.365 0.0 14.98 0.0
 CUBOID 2 1 0.15 0.0 14.98 0.0 14.98 0.0
 UNIT 3
 COM='REAR OF FUEL BOX'
 CUBOID 2 1 0.15 0.0 14.98 0.0 14.98 0.0
 UNIT 4
 COM='ARRAY TO ASSEMBLE PART OF BOX'
 ARRAY 26 3*0
 UNIT 5
 COM='TOP AND BOTTOM OF BOX'
 CUBOID 0 1 9.80 0.0 3.750 0.0 0.15 0.0
 CUBOID 2 1 15.28 0.0 9.365 -5.615 0.15 0.0
 GLOBAL
 UNIT 6
 COM='ARRAY TO ASSEMBLE TOP AND BOTTOM'
 ARRAY 27 3*0
 CUBOID 2 1 15.28 0.0 15.13 -0.15 15.28 0.0
 CUBOID 0 1 15.305 -0.025 15.155 -0.175 15.305 -0.025
 UNIT 7
 COM='FUEL BOX 15.28 CM ON A SIDE WITH .15 CM WALLS .05CM STACKING VOID'
 CUBOID 1 1 6P7.49
 CUBOID 2 1 6P7.64
 CUBOID 0 1 6P7.6650
 UNIT 34
 COM='ALUMINUM WEIGHT DISTRIBUTION PLATE FOR SPECIAL BOX'
 CUBOID 0 1 9.80 0.0 3.750 0.0 0.16 0.0
 CUBOID 7 1 15.33 0.0 9.54 -5.79 0.16 0.0
 UNIT 35
 COM='ALUMINUM WEIGHT DISTRIBUTION PLATE FOR BOXES'
 CUBOID 7 1 4P7.665 0.16 0.0
 UNIT 9
 COM='NORTH SPLIT TABLE CORE'
 ARRAY 1 3*0.0
 CUBOID 0 1 30.66 -0.94 77.5 0.0 83.475 0.0
 UNIT 10
 COM='SOUTH SPLIT TABLE CORE'
 ARRAY 2 3*0.0
 CUBOID 0 1 49.4 0.0 77.5 0.0 83.475 0.0

UNIT 11
 COM='PLEXIGLASS REFLECTOR SHEET WITHOUT TRIS, NORTH BOTTOM REFLECTOR'
 CUBOID 4 1 2P15.8000 2P38.7500 2P0.6150
 UNIT 12
 COM='PLEXIGLASS REFLECTOR SHEET WITH TRIS, NORTH BOTTOM REFLECTOR'
 CUBOID 5 1 2P15.8000 2P38.7500 2P0.6150
 UNIT 13
 COM='UPPER PORTION NORTH BOTTOM REFLECTOR WITH TRIS'
 CUBOID 5 1 2P15.8 2P38.75 2P8.24
 UNIT 14
 COM='LOWER PORTION NORTH BOTTOM REFLECTOR WITH TRIS'
 CUBOID 5 1 2P15.8 2P38.75 2P3.69
 UNIT 15
 COM='NORTH BOTTOM REFLECTOR INCLUDES REGULAR AND TRIS'
 ARRAY 3 3*0.0
 UNIT 16
 COM='PLEXIGLAS SHEET BOTTOM SOUTH REFLECTOR WITHOUT TRIS'
 CUBOID 0 1 2P5.1 2P2.5 2P0.6150
 CUBOID 4 1 44.3 -5.1 2P38.75 2P0.615
 UNIT 17
 COM='PLEXIGLAS SHEET BOTTOM SOUTH REFLECTOR WITH TRIS'
 CUBOID 0 1 2P5.1 2P2.5 2P0.6150
 CUBOID 5 1 44.3 -5.1 2P38.75 2P0.6150
 UNIT 18
 COM='LOWER PORTION SOUTH BOTTOM REFLECTOR WITH TRIS'
 CUBOID 0 1 2P5.1 2P2.5 2P8.855
 CUBOID 5 1 44.3 -5.1 2P38.75 2P8.855
 UNIT 19
 COM='SOUTH BOTTOM REFLECTOR WITH REGULAR AND TRIS'
 ARRAY 4 3*0.0
 UNIT 20
 COM='EAST AND WEST REFLECTORS FOR NORTH REFLECTOR WITH TRIS'
 CUBOID 5 1 2P15.8 2P12.65 2P54.2825
 UNIT 21
 COM='ARRAY FOR EAST AND WEST REFLECTORS FOR NORTH REFLECTOR'
 ARRAY 5 3*0.0
 UNIT 22
 COM='EAST AND WEST REFLECTORS FOR SOUTH REFLECTOR WITH TRIS'
 CUBOID 5 1 2P24.700 2P12.65 2P54.2825
 UNIT 23
 COM='ARRAY FOR EAST AND WEST REFLECTORS FOR SOUTH REFLECTOR'
 ARRAY 6 3*0.0
 UNIT 24
 COM='NORTH TOP REFLECTOR WITH TRIS'
 CUBOID 5 1 2P28.35 2P64.05 2P12.15
 UNIT 25
 COM='ARRAY FOR NORTH TOP REFLECTOR'
 ARRAY 7 3*0.0
 UNIT 26
 COM='SOUTH TOP REFLECTOR WITH TRIS'
 CUBOID 0 1 2P5.1 2P2.5 2P12.15
 CUBOID 5 1 69.4 -5.1 2P64.05 2P12.15
 UNIT 27
 COM='ARRAY FOR SOUTH TOP REFLECTOR'
 ARRAY 8 3*0.0
 UNIT 28
 COM='NORTH END REFLECTOR 9.8CM PORTION WITHOUT TRIS'
 CUBOID 4 1 2P4.9000 2P64.0500 2P54.2825
 UNIT 29
 COM='NORTH END REFLECTOR 5.2 CM PORTION WITH TRIS'
 CUBOID 5 1 2P2.6 2P64.0500 2P54.2825
 UNIT 30
 COM='NORTH END REFLECTOR 10.1 CM PORTION WITHOUT TRIS'
 CUBOID 4 1 2P5.05 2P64.05 2P54.2825

Table A.3 (continued)

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UNIT 31
COM='ARRAY FOR NORTH END REFLECTOR'
ARRAY 9 3*0.0
UNIT 32
COM='SOUTH END REFLECTOR'
CUBOID 5 1 2P12.55 2P64.05 2P54.2825
UNIT 33
COM='ARRAY FOR SOUTH END REFLECTOR'
ARRAY 10 3*0.0
UNIT 38
COM='NORTH CORE WITH BOTTOM REFLECTOR'
ARRAY 13 3* 0.0
UNIT 39
COM='NORTH CORE WITH EAST AND WEST REFLECTOR'
ARRAY 14 3*0.0
UNIT 40
COM='NORTH CORE WITH END REFLECTOR'
ARRAY 15 3*0.0
UNIT 42
COM='NORTH CORE WITH TOP REFLECTOR'
ARRAY 16 3*0.0
UNIT 48
COM='SOUTH CORE WITH BOTTOM REFLECTORS'
ARRAY 20 3*0.0
UNIT 49
COM='SOUTH CORE WITH EAST WEST REFLECTORS'
ARRAY 21 3*0.0
UNIT 50
COM='SOUTH CORE END REFLECTOR'
ARRAY 22 3*0.0
UNIT 52
COM='SOUTH CORE WITH TOP REFLECTOR'
ARRAY 23 3*0.0
UNIT 54
COM='AIR GAP'
CUBOID 0 1 0.570 0.0 64.475 -63.625 69.13 -63.735
GLOBAL
UNIT 55
COM='TOTAL'
ARRAY 25 3*0.0
UNIT 56
COM='COMBINATION OF TWO REGULAR FUEL BOXES'
ARRAY 28 3*0.0
UNIT 57
COM='COMBINATION OF REGULAR FUEL BOX AND SPECIAL FUEL BOX'
ARRAY 29 3*0.0
UNIT 58
COM='COMBINATION OF TWO REGULAR WEIGHT DISTRIBUTION PLATES'
ARRAY 30 3*0.0
UNIT 59
COM='COMBINATION OF REGULAR AND SPECIAL WEIGHT DISTRIBUTION PLATES'
ARRAY 31 3*0.0
UNIT 60
COM='NORTH CORE SOLUTION DRIVER'
CUBOID 8 1 2P7.5 2P14.9 3.332 -7.5
CUBOID 0 1 2P7.5 2P14.9 2P7.5
CUBOID 9 1 2P7.65 2P15.05 2P7.65
CUBOID 0 1 2P7.665 2P15.33 2P7.665
UNIT 61
COM='SOUTH CORE SOLUTION DRIVER'
CUBOID 8 1 2P7.5 2P14.9 3.292 -7.5
CUBOID 0 1 2P7.5 2P14.9 2P7.5
CUBOID 9 1 2P7.65 2P15.05 2P7.65
CUBOID 0 1 2P7.665 2P15.33 2P7.665
END GEOMETRY

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READ ARRAY
ARA=1 NUX=2 NUY=4 NUZ=9
COM='NORTH SPLIT TABLE CORE'
FILL 2R7 2R56 4R7
      2R35 2R58 4R35
      2R7 2R56 4R7
      2R35 2R58 4R35
      2R7 56 60 4R7
      2R35 2R58 4R35
      2R7 2R56 4R7
      2R35 2R58 4R35
      2R7 2R56 4R7
END FILL
ARA=2 NUX=3 NUY=4 NUZ=9
COM='SOUTH SPLIT TABLE CORE'
FILL 3R7 3R56 6R7
      3R35 3R58 6R35
      3R7 3R56 6R7
      3R35 3R58 6R35
      3R7 61 56 56 6R7
      3R35 3R58 6R35
      3R7 57 56 56 6R7
      3R35 59 58 58 6R35
      3R7 57 56 56 6R7
END FILL
ARA=3 NUX=1 NUY=1 NUZ=3
COM='NORTH BOTTOM REFLECTOR'
FILL 14 11 13 END FILL
ARA=4 NUX=1 NUY=1 NUZ=7
COM='SOUTH BOTTOM REFLECTOR'
FILL 18 16 17 16 16 17 17 END FILL
ARA=5 NUX=1 NUY=1 NUZ=1
COM='EAST AND WEST WALLS OF NORTH REFLECTOR'
FILL 20 END FILL
ARA=6 NUX=1 NUY=1 NUZ=1
COM='EAST AND WEST WALLS OF SOUTH REFLECTOR'
FILL 22 END FILL
ARA=7 NUX=1 NUY=1 NUZ=1
COM='ARRAY FOR NORTH TOP REFLECTOR'
FILL 24 END FILL
ARA=8 NUX=1 NUY=1 NUZ=1
COM='ARRAY FOR SOUTH TOP REFLECTOR'
FILL 26 END FILL
ARA=9 NUX=3 NUY=1 NUZ=1
COM='ARRAY FOR NORTH END REFLECTOR'
FILL 28 29 30 END FILL
ARA=10 NUX=1 NUY=1 NUZ=1
COM='ARRAY FOR SOUTH END REFLECTOR'
FILL 32 END FILL
ARA=13 NUX=1 NUY=1 NUZ=2
COM='COMBINATION OF NORTH CORE WITH BOTTOM REFLECTOR'
FILL 15 9 END FILL
ARA=14 NUX=1 NUY=3 NUZ=1
COM='NORTH CORE WITH SIDE REFLECTORS'
FILL 21 38 21 END FILL
ARA=15 NUX=2 NUY=1 NUZ=1
COM='NORTH CORE WITH END REFLECTOR'
FILL 31 39 END FILL
ARA=16 NUX=1 NUY=1 NUZ=2
COM='NORTH CORE WITH TOP REFLECTOR'
FILL 40 25 END FILL
ARA=20 NUX=1 NUY=1 NUZ=2
COM='SOUTH CORE WITH BOTTOM REFLECTOR'
FILL 19 10 END FILL

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Table A.3 (continued)

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ARA-21 NUX=1 NUY=3 NUZ=1
COM='SOUTH CORE WITH EAST WEST REFLECTORS'
FILL 23 48 23 END FILL
ARA-22 NUX=2 NUY=1 NUZ=1
COM='SOUTH CORE WITH END REFLECTOR'
FILL 49 33 END FILL
ARA-23 NUX=1 NUY=1 NUZ=2
COM='COMBINATION OF CORE WITH TOP REFLECTOR'
FILL 50 27 END FILL
ARA-25 NUX=3 NUY=1 NUZ=1
COM='TOTAL'
FILL 42 54 52 END FILL
ARA-26 NUX=3 NUY=1 NUZ=1
COM='ASSEMBLY OF FUEL BOX FRONT AND REAR'
FILL 2 1 3 END FILL
ARA-27 NUX=1 NUY=1 NUZ=3
COM='ASSEMBLY OF FUEL BOX TOP AND BOTTOM'
FILL 5 4 5 END FILL
ARA-28 NUX=1 NUY=2 NUZ=1
COM='COMBINATION OF TWO FUEL BOXES'
FILL 7 7 END FILL
ARA-29 NUX=1 NUY=2 NUZ=1
COM='COMBINATION OF SPECIAL AND REGULAR FUEL BOXES'
FILL 7 6 END FILL
ARA-30 NUX=1 NUY=2 NUZ=1
COM='COMBINATION OF TWO WEIGHT DISTRIBUTION PLATES'
FILL 35 35 END FILL
ARA-31 NUX=1 NUY=2 NUZ=1
COM='COMBINATION OF SPECIAL AND REGULAR WEIGHT DISTRIBUTION PLATES'
FILL 35 34 END FILL
END ARRAY
READ PLOT TTL='YZ SLICE OF SOUTH CORE FIRST ROW'
XUL=64.319 YUL=40.000 ZUL=72.000
XLR=64.319 YLR=72.000 ZLR=56.000
VAX=1 WDN=-1 NAX=130 NCH='012345678'END
TTL='XZ SLICE OF SPHERE CUBOID'
XUL=56.0 YUL=63.625 ZUL=71.735
XLR=72.0 YLR=63.625 ZLR=55.735
UAX=1 WDN=-1 NAX=130 NCH='012345678'
END PLOT
READ START NST=1 XSM=41.37 XSP=72.894 YSM=40.63 YSP=71.29
ZSM=56.071 ZSP=71.4 END START
END DATA
END

CAR17
=CSAS25
ROCKY FLATS CRITICALS NUREG/CR-2500 EXPERIMENT F (27 GROUP)
' 48 FUEL CANS 0.929 CM MODERATOR GEE.HU203.DATA(UNDER)
27GROUPNDF4 LATTICECELL
U308 1 5.4078E-1 293.0 92234 0.03 92235 4.46 92236 0.08 92238 95.43 END
H2O 1 2.6356E-1 END
ARBM-BAGGIE 1.0 3 0 0 0 1001 14.01 6012 84.9 8016 1.20 1 1.9134E-2
END
ARBM-AL1100 1.0 3 0 0 1 13027 99.18 26000 0.5 29000 0.2 2 9.5390E-1
END
ARBM-TAPE(VINYL) 1.0 7 0 0 0 1001 5.92 6012 45.91 8016 10.82 17000
25.73 20040 6.9 22000 1.6 82000 1.1 2 1.1115E-2 END
ARBM-TAPE(MYLAR) 1.0 3 0 0 0 1001 6.83 6012 65.50 8016 27.02 2
1.7491E-2 END
ARBM-MODERATOR 1.185 3 0 0 0 1001 7.83 6012 59.49 8016 32.48 3 END
ARBM-PLEX(REG) 1.0 3 0 0 0 1001 7.84 6012 59.59 8016 32.23 4
1.1773 END
ARBM-PLEX(PAPER) 1.0 3 0 0 0 1001 6.48 6012 42.17 8016 49.5 4
3.7534E-3 END
ARBM-PLEX(GLUE) 1.0 3 0 0 0 1001 11.67 6012 86.29 8016 1.20 4
1.1648E-3 END
ARBM-PLEX(TRIS) 1.0 8 0 0 1 1001 7.16 6012 52.03 7014 0.16 8016 29.82
15031 1.02 17000 1.81 35079 4.260 35081 2.840 5 1.2757 END
ARBM-PLEX(PAPER) 1.0 3 0 0 0 1001 6.48 6012 42.17 8016 49.5 5
3.7534E-3 END
ARBM-PLEX(GLUE) 1.0 3 0 0 0 1001 11.67 6012 86.29 8016 1.20 5
1.1648E-3 END
ARBM-FILLER 1.185 3 0 0 0 1001 7.83 6012 59.49 8016 32.48 6 1.0 END
' THIS MATERIAL IS ACTUALLY MODERATOR ADJUSTED FOR THE VOLUME
' FRACTION OF THE VOID FILLED BETWEEN CORE AND REFLECTOR.
END COMP
' SPHERICAL VACUUM REFLECTED 0.0 END
' 1 9.2929 ONEEXTERMOD 3 10.0 NOEXTERMOD END ZONE
SPHTRIANGP 19.00 18.5857 1 3 18.9579 2 END
ROCKY FLATS CRITICALS NUREG/CR-2500 EXPERIMENT F (27 GROUP)
' 48 FUEL CANS 0.929 CM MODERATOR GEE.HU203.DATA(UNDER)
READ PARM RUN=YES NPG=600
PLT=NO NUB=YES PDN=YES
END PARM
READ GEOM
UNIT 1
COM='FUEL BOX 15.28 CM ON A SIDE WITH .15 CM WALLS .05CM STACKING VOID'
CUBOID 1 1 6P7.49
CUBOID 2 1 6P7.64
CUBOID 0 1 6P7.6650
UNIT 2
COM='X-FACE INTERSTITIAL MODERATOR'
CUBOID 3 1 2P0.4645 4P7.665
UNIT 3
COM='Y-FACE INTERSTITIAL MODERATOR'
CUBOID 3 1 2P7.665 2P0.4645 2P7.665
UNIT 4
COM='Z-FACE INTERSTITIAL MODERATOR'
CUBOID 3 1 4P7.665 2P0.4645
UNIT 5
COM='MORE X-FACE MODERATOR'
CUBOID 3 1 4P0.4645 2P7.665
UNIT 6
COM='MORE Y-FACE MODERATOR'
CUBOID 3 1 2P7.665 4P0.4645
UNIT 7
COM='MORE Z-FACE MODERATOR'
CUBOID 3 1 2P0.4645 2P7.665 2P0.4645

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Table A.3 (continued)

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UNIT 8
COM='LAST OF INTERSTITIAL MODERATOR'
CUBOID 3 1 6P0.4645
UNIT 9
COM='NORTH SPLIT TABLE CORE'
ARRAY 1 3*0.0
REPLICATE 0 1 0.0 0.0 0.0 0.0 17.8910 0.0 1
UNIT 10
COM='SOUTH SPLIT TABLE CORE'
ARRAY 2 3*0.0
REPLICATE 0 1 0.0 0.0 0.0 0.0 17.8910 0.0 1
UNIT 11
COM='PLEXIGLASS REFLECTOR SHEET WITHOUT TRIS, NORTH BOTTOM REFLECTOR'
CUBOID 4 1 2P15.8000 2P38.7500 2P0.6150
UNIT 12
COM='PLEXIGLASS REFLECTOR SHEET WITH TRIS, NORTH BOTTOM REFLECTOR'
CUBOID 5 1 2P15.8000 2P38.7500 2P0.6150
UNIT 13
COM='UPPER PORTION NORTH BOTTOM REFLECTOR WITH TRIS'
CUBOID 5 1 2P15.8 2P38.75 2P8.24
UNIT 14
COM='LOWER PORTION NORTH BOTTOM REFLECTOR WITH TRIS'
CUBOID 5 1 2P15.8 2P38.75 2P3.69
UNIT 15
COM='NORTH BOTTOM REFLECTOR INCLUDES REGULAR AND TRIS'
ARRAY 3 3*0.0
UNIT 16
COM='PLEXIGLAS SHEET BOTTOM SOUTH REFLECTOR WITHOUT TRIS'
CUBOID 0 1 2P5.1 2P2.55 2P0.615
CUBOID 4 1 44.3 -5.1 2P38.75 2P0.615
UNIT 17
COM='PLEXIGLAS SHEET BOTTOM SOUTH REFLECTOR WITH TRIS'
CUBOID 0 1 2P5.1 2P2.55 2P0.615
CUBOID 5 1 44.3 -5.1 2P38.75 2P0.6150
UNIT 18
COM='LOWER PORTION SOUTH BOTTOM REFLECTOR WITH TRIS'
CUBOID 0 1 2P5.1 2P2.55 2P8.855
CUBOID 5 1 44.3 -5.1 2P38.75 2P8.855
UNIT 19
COM='SOUTH BOTTOM REFLECTOR WITH REGULAR AND TRIS'
ARRAY 4 3*0.0
UNIT 20
COM='EAST AND WEST REFLECTORS FOR NORTH REFLECTOR WITH TRIS'
CUBOID 5 1 2P15.8 2P12.65 2P54.2825
UNIT 21
COM='ARRAY FOR EAST AND WEST REFLECTORS FOR NORTH REFLECTOR'
ARRAY 5 3*0.0
UNIT 22
COM='EAST AND WEST REFLECTORS FOR SOUTH REFLECTOR WITH TRIS'
CUBOID 5 1 2P24.700 2P12.65 2P54.2825
UNIT 23
COM='ARRAY FOR EAST AND WEST REFLECTORS FOR SOUTH REFLECTOR'
ARRAY 6 3*0.0
UNIT 24
COM='NORTH TOP REFLECTOR WITH TRIS'
CUBOID 5 1 2P28.35 2P64.05 2P12.15
UNIT 25
COM='ARRAY FOR NORTH TOP REFLECTOR'
ARRAY 7 3*0.0
UNIT 26
COM='SOUTH TOP REFLECTOR WITH TRIS'
CUBOID 0 1 2P5.1 2P2.55 2P12.15
CUBOID 5 1 69.4 -5.1 2P64.05 2P12.15

UNIT 27
COM='ARRAY FOR SOUTH TOP REFLECTOR'
ARRAY 8 3*0.0
UNIT 28
COM='NORTH END REFLECTOR 9.8CM PORTION WITHOUT TRIS'
CUBOID 4 1 2P4.9000 2P64.0500 2P54.2825
UNIT 29
COM='NORTH END REFLECTOR 5.2 CM PORTION WITH TRIS'
CUBOID 5 1 2P2.6 2P64.0500 2P54.2825
UNIT 30
COM='NORTH END REFLECTOR 10.1 CM PORTION WITHOUT TRIS'
CUBOID 4 1 2P5.05 2P64.05 2P54.2825
UNIT 31
COM='ARRAY FOR NORTH END REFLECTOR'
ARRAY 9 3*0.0
UNIT 32
COM='SOUTH END REFLECTOR'
CUBOID 5 1 2P12.55 2P64.05 2P54.2825
UNIT 33
COM='ARRAY FOR SOUTH END REFLECTOR'
ARRAY 10 3*0.0
UNIT 34
COM='12.95 THICK MODERATING PLASTIC NORTH CORE'
CUBOID 6 1 2P15.7945 2P6.6965 2P32.8695
UNIT 35
COM='2.95 THICK MODERATING PLASTIC NORTH CORE'
CUBOID 0 1 2P15.7945 2P38.75 2P1.5545
UNIT 36
ARRAY 11 3*0.0
UNIT 37
ARRAY 12 3*0.0
UNIT 38
COM='NORTH CORE WITH BOTTOM REFLECTOR'
ARRAY 13 3* 0.0
UNIT 39
COM='NORTH CORE WITH EAST AND WEST REFLECTOR'
ARRAY 14 3*0.0
UNIT 40
COM='NORTH CORE WITH END REFLECTOR'
ARRAY 15 3*0.0
UNIT 41
COM='NORTH SPLIT TABLE FACEPLATE FOR THIS CASE AIR GAP HALF THICK'
CUBOID 0 1 2P0.1025 2P64.0500 2P66.4325
UNIT 42
COM='NORTH CORE WITH TOP REFLECTOR'
ARRAY 16 3*0.0
UNIT 43
COM='NORTH CORE WITH FACEPLATE'
ARRAY 17 3*0.0
UNIT 44
COM='12.95 CM THICK MODERATOR SOUTH CORE'
CUBOID 6 1 2P15.7945 2P6.6965 2P32.8695
UNIT 45
COM='2.95 THICK MODERATOR SOUTH CORE'
CUBOID 0 1 2P15.7945 2P38.75 2P1.5545
UNIT 46
COM='COMBINATION OF CORE WITH 12.95 THICK MODERATOR'
ARRAY 18 3*0.0
UNIT 47
COM='COMBINATION OF CORE WITH 2.95 THICK MODERATOR'
ARRAY 19 3*0.0
UNIT 48
COM='SOUTH CORE WITH EAST WEST REFLECTORS'
ARRAY 20 3*0.0

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Table A.3 (continued)

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UNIT 49
COM='SOUTH CORE WITH EAST WEST REFLECTORS'
ARRAY 21 3*0.0
UNIT 50
COM='SOUTH CORE END REFLECTOR'
ARRAY 22 3*0.0
UNIT 51
COM='FACEPLATE FOR SOUTH SPLIT TABLE'
CUBOID 3 1 2P0.4645 2P64.0500 2P66.4325
UNIT 52
COM='SOUTH CORE WITH TOP REFLECTOR'
ARRAY 23 3*0.0
UNIT 53
COM='SOUTH CORE WITH FACEPLATE'
ARRAY 24 3*0.0
UNIT 54
COM='AIR GAP HALF THICKNESS'
CUBOID 0 1 2P0.1025 2P64.0500 2P66.4325
GLOBAL
UNIT 55
COM='TOTAL'
ARRAY 25 3*0.0
UNIT 56
COM='NORTH BOTTOM MODERATOR'
CUBOID 6 1 2P15.8000 2P38.7500 2P7.3135
UNIT 57
COM='BOTTOM SOUTH MODERATOR'
CUBOID 6 1 2P24.700 2P38.75 2P7.3135
UNIT 58
COM='REAR FILLER'
CUBOID 6 1 2P8.9055 2P38.75 2P34.424
UNIT 59
COM='COMBINATION OF SOUTH CORE WITH REAR FILLER'
ARRAY 26 3*0.0
UNIT 60
COM='NORTH CORE REAR FILLER'
CUBOID 6 1 2P0.0055 2P38.75 2P34.424
UNIT 61
COM='COMBINATION OF NORTH CORE WITH REAR FILLER'
ARRAY 27 3*0.0
END GEOMETRY
READ ARRAY
ARA=1 NUX=3 NUY=7 NUZ=5
COM='NORTH SPLIT TABLE CORE'
FILL 1 2 1 3 5 3 2Q6 1 2 1
      4 7 4 6 8 6 2Q6 4 7 4
      1Q42
      1 2 1 3 5 3 2Q6 1 2 1 END FILL
ARA=2 NUX=3 NUY=7 NUZ=5
COM='SOUTH SPLIT TABLE CORE'
FILL 1 2 1 3 5 3 2Q6 1 2 1
      4 7 4 6 8 6 2Q6 4 7 4
      1Q42
      1 2 1 3 5 3 2Q6 1 2 1 END FILL
ARA=3 NUX=1 NUY=1 NUZ=4
COM='NORTH BOTTOM MODERATOR AND REFLECTOR'
FILL 14 11 13 56 END FILL
ARA=4 NUX=1 NUY=1 NUZ=8
COM='SOUTH BOTTOM MODERATOR AND REFLECTOR'
FILL 18 16 17 16 16 17 17 57 END FILL
ARA=5 NUX=1 NUY=1 NUZ=1
COM='EAST AND WEST WALLS OF NORTH REFLECTOR'
FILL 20 END FILL
ARA=6 NUX=1 NUY=1 NUZ=1
COM='EAST AND WEST WALLS OF SOUTH REFLECTOR'
FILL 22 END FILL
ARA=7 NUX=1 NUY=1 NUZ=1
COM='ARRAY FOR NORTH TOP REFLECTOR'
FILL 24 END FILL
ARA=8 NUX=1 NUY=1 NUZ=1
COM='ARRAY FOR SOUTH TOP REFLECTOR'
FILL 26 END FILL
ARA=9 NUX=3 NUY=1 NUZ=1
COM='ARRAY FOR NORTH END REFLECTOR'
FILL 28 29 30 END FILL
ARA=10 NUX=1 NUY=1 NUZ=1
COM='ARRAY FOR SOUTH END REFLECTOR'
FILL 32 END FILL
ARA=11 NUX=1 NUY=2 NUZ=1
COM='COMBINARION OF CORE WITH 12.95CM THICK MODERATOR'
FILL 9 34 END FILL
ARA=12 NUX=1 NUY=1 NUZ=2
COM='COMBINATION OF PREVIOUS ARRAY WITH 2.95CM THICK MODERATOR'
FILL 36 35 END FILL
ARA=13 NUX=1 NUY=1 NUZ=2
COM='COMBINATION OF NORTH CORE WITH BOTTOM REFLECTOR'
FILL 15 61 END FILL
ARA=14 NUX=1 NUY=3 NUZ=1
COM='NORTH CORE WITH SIDE REFLECTORS'
FILL 21 38 21 END FILL
ARA=15 NUX=2 NUY=1 NUZ=1
COM='NORTH CORE WITH END REFLECTOR'
FILL 31 39 END FILL
ARA=16 NUX=1 NUY=1 NUZ=2
COM='NORTH CORE WITH TOP REFLECTOR'
FILL 40 25 END FILL
ARA=17 NUX=2 NUY=1 NUZ=1
COM='NORTH CORE WITH FACEPLATE'
FILL 42 41 END FILL
ARA=18 NUX=1 NUY=2 NUZ=1
COM='COMBINATION OF S. CORE WITH 12.95 CM THICK MODERATOR'
FILL 10 44 END FILL
ARA=19 NUX=1 NUY=1 NUZ=2
COM='COMBINATION OF CORE WITH 2.95 CM THICK MODERATOR'
FILL 46 45 END FILL
ARA=20 NUX=1 NUY=1 NUZ=2
COM='SOUTH CORE WITH BOTTOM REFLECTOR'
FILL 19 59 END FILL
ARA=21 NUX=1 NUY=3 NUZ=1
COM='SOUTH CORE WITH EAST WEST REFLECTORS'
FILL 23 48 23 END FILL
ARA=22 NUX=2 NUY=1 NUZ=1
COM='SOUTH CORE WITH END REFLECTOR'
FILL 49 33 END FILL
ARA=23 NUX=1 NUY=1 NUZ=2
COM='COMBINATION OF CORE WITH TOP REFLECTOR'
FILL 50 27 END FILL
ARA=24 NUX=2 NUY=1 NUZ=1
COM='SOUTH CORE WITH FACEPLATE'
FILL 51 52 END FILL
ARA=25 NUX=3 NUY=1 NUZ=1
COM='TOTAL'
FILL 43 54 53 END FILL
ARA=26 NUX=2 NUY=1 NUZ=1
COM='COMBINATION OF SOUTH CORE WITH REAR FILLER'
FILL 47 58 END FILL

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Table A.3 (continued)

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ARA=27 NUX=2 NUY=1 NUZ=1
COM='COMBINATION OF NORTH CORE WITH REAR FILLER'
FILL 37 60 END FILL
END ARRAY
READ PLOT TTL='XZ SLICE OF RFPF SHOWING MATERIAL REGIONS'
XUL=-1 YUL=64.05 ZUL=135
XLR=136 YLR=64.05 ZLR=-2
UAX=1 WDN=-1 NAX=130 NCH='0123456'END
TTL='YZ SLICE OF NORTH CORE FIRST ROW'
XUL=48 YUL=-2 ZUL=136
XLR=48 YLR=136 ZLR=-2
VAX=1 WDN=-1 NAX=130 NCH='0123456'END
TTL='YZ SLICE OF NORTH CORE SECOND ROW'
XUL=28 YUL=-2 ZUL=136
XLR=28 YLR=136 ZLR=-2
VAX=1 WDN=-1 NAX=130 NCH='0123456'END
TTL='YZ SLICE OF SOUTH CORE FIRST ROW'
XUL=62 YUL=-2 ZUL=136
XLR=62 YLR=136 ZLR=-2
VAX=1 WDN=-1 NAX=130 NCH='0123456'END
TTL='TOP VIEW OF SOURCE SLOT'
XUL=-2 YUL=136 ZUL=125
XLR=138 YLR=-2 ZLR=125
UAX=1 VDN=-1 NAX=130 NCH='0123456'END
TTL='TOP VIEW OF TOP LAYER'
XUL=-2 YUL=136 ZUL=95
XLR=138 YLR=-2 ZLR=95
UAX=1 VDN=-1 NAX=130 NCH='0123456'
END PLOT
READ START NST=1
XSP=108.0 XSM=10.0
YSP=108.0 YSM=10.0
ZSP=123.0 ZSM=44.0
END START
END DATA
END

CAR18
=CSAS25
ROCKY FLATS CRITICALS NUREG/CR-2500 EXPERIMENT G (27 GROUP)
' 30 FUEL CANS 2.44 CM MODERATOR GEE.HU203.DATA(OPTUM)
27GROUPNDF4 LATTICECELL
U308 1 5.4078E-1 293.0 92234 0.03 92235 4.46 92236 0.08 92238 95.43 END
H2O 1 2.6356E-1 END
ARBM-BAGGIE 1.0 3 0 0 0 1001 14.01 6012 84.9 8016 1.20 1 1.9134E-2
END
ARBM-AL1100 1.0 3 0 0 1 13027 99.18 26000 0.5 29000 0.2 2 9.5390E-1
END
ARBM-TAPE(VINYL) 1.0 7 0 0 0 1001 5.92 6012 45.91 8016 10.82 17000
25.73 20040 6.9 22000 1.6 82000 1.1 2 1.1115E-2 END
ARBM-TAPE(MYLAR) 1.0 3 0 0 0 1001 6.83 6012 65.50 8016 27.02 2
1.7491E-2 END
ARBM-MODERATOR 1.185 3 0 0 0 1001 7.83 6012 59.49 8016 32.48 3 END
ARBM-PLEX(REG) 1.0 3 0 0 0 1001 7.84 6012 59.59 8016 32.23 4
1.1773 END
ARBM-PLEX(PAPER) 1.0 3 0 0 0 1001 6.48 6012 42.17 8016 49.5 4
3.7534E-3 END
ARBM-PLEX(GLUE) 1.0 3 0 0 0 1001 11.67 6012 86.29 8016 1.20 4
1.1648E-3 END
ARBM-PLEX(TRIS) 1.0 8 0 0 1 1001 7.16 6012 52.03 7014 0.16 8016 29.82
15031 1.02 17000 1.81 35079 4.260 35081 2.840 5 1.2757 END
ARBM-PLEX(PAPER) 1.0 3 0 0 0 1001 6.48 6012 42.17 8016 49.5 5
3.7534E-3 END
ARBM-PLEX(GLUE) 1.0 3 0 0 0 1001 11.67 6012 86.29 8016 1.20 5
1.1648E-3 END
ARBM-FILLER 1.185 3 0 0 0 1001 7.83 6012 59.49 8016 32.48 6 1.0 END
' THIS MATERIAL IS ACTUALLY MODERATOR ADJUSTED FOR THE VOLUME
' FRACTION OF THE VOID FILLED BETWEEN CORE AND REFLECTOR.
END COMP
SPHTRIANGP 19.00 18.5857 1 3 18.9579 2 END
ROCKY FLATS CRITICALS NUREG/CR-2500 EXPERIMENT G (27 GROUP)
' 30 FUEL CANS 2.44 CM MODERATOR GEE.HU203.DATA(OPTUM)
READ PARM RUN=YES NPG=600 PDN=YES NUB=YES PLT=NO
END PARM
READ GEOM
UNIT 1
COM='FUEL BOX 15.28 CM ON A SIDE WITH .15 CM WALLS .05CM STACKING VOID'
CUBOID 1 1 6P7.49
CUBOID 2 1 6P7.64
CUBOID 0 1 6P7.6650
UNIT 2
COM='X-FACE INTERSTITIAL MODERATOR'
CUBOID 3 1 2P1.2200 4P7.665
UNIT 3
COM='Y-FACE INTERSTITIAL MODERATOR'
CUBOID 3 1 2P7.665 2P1.2200 2P7.665
UNIT 4
COM='Z-FACE INTERSTITIAL MODERATOR'
CUBOID 3 1 4P7.665 2P1.2200
UNIT 5
COM='MORE X-FACE MODERATOR'
CUBOID 3 1 4P1.2200 2P7.665
UNIT 6
COM='MORE Y-FACE MODERATOR'
CUBOID 3 1 2P7.665 4P1.2200
UNIT 7
COM='MORE Z-FACE MODERATOR'
CUBOID 3 1 2P1.2200 2P7.665 2P1.2200
UNIT 8
COM='LAST OF INTERSTITIAL MODERATOR'
CUBOID 3 1 6P1.2200

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Table A.3 (continued)

UNIT 9
COM='NORTH SPLIT TABLE CORE'
ARRAY 1 3*0.0
UNIT 10
COM='SOUTH SPLIT TABLE CORE'
ARRAY 2 3*0.0
UNIT 11
COM='PLEXIGLASS REFLECTOR SHEET WITHOUT TRIS, NORTH BOTTOM REFLECTOR'
CUBOID 4 1 2P16.5500 2P38.7500 2P0.6150
UNIT 12
COM='PLEXIGLASS REFLECTOR SHEET WITH TRIS, NORTH BOTTOM REFLECTOR'
CUBOID 5 1 2P16.5500 2P38.7500 2P0.6150
UNIT 13
COM='UPPER PORTION NORTH BOTTOM REFLECTOR WITH TRIS'
CUBOID 5 1 2P16.5500 2P38.75 2P8.24
UNIT 14
COM='LOWER PORTION NORTH BOTTOM REFLECTOR WITH TRIS'
CUBOID 5 1 2P16.5500 2P38.75 2P3.69
UNIT 15
COM='NORTH BOTTOM REFLECTOR INCLUDES REGULAR AND TRIS'
ARRAY 3 3*0.0
UNIT 16
COM='PLEXIGLAS SHEET BOTTOM SOUTH REFLECTOR WITHOUT TRIS'
CUBOID 0 1 2P5.1 2P2.55 2P0.615
CUBOID 4 1 44.3 -5.1 2P38.75 2P0.615
UNIT 17
COM='PLEXIGLAS SHEET BOTTOM SOUTH REFLECTOR WITH TRIS'
CUBOID 0 1 2P5.1 2P2.55 2P0.615
CUBOID 5 1 44.3 -5.1 2P38.75 2P0.6150
UNIT 18
COM='LOWER PORTION SOUTH BOTTOM REFLECTOR WITH TRIS'
CUBOID 0 1 2P5.1 2P2.55 2P8.855
CUBOID 5 1 44.3 -5.1 2P38.75 2P8.855
UNIT 19
COM='SOUTH BOTTOM REFLECTOR WITH REGULAR AND TRIS'
ARRAY 4 3*0.0
UNIT 20
COM='EAST AND WEST REFLECTORS FOR NORTH REFLECTOR WITH TRIS'
CUBOID 5 1 2P16.5500 2P12.65 2P52.7825
UNIT 21
COM='ARRAY FOR EAST AND WEST REFLECTORS FOR NORTH REFLECTOR'
ARRAY 5 3*0.0
UNIT 22
COM='EAST AND WEST REFLECTORS FOR SOUTH REFLECTOR WITH TRIS'
CUBOID 5 1 2P24.700 2P12.65 2P52.7825
UNIT 23
COM='ARRAY FOR EAST AND WEST REFLECTORS FOR SOUTH REFLECTOR'
ARRAY 6 3*0.0
UNIT 24
COM='NORTH TOP REFLECTOR WITH TRIS'
CUBOID 5 1 2P29.1 2P64.05 2P12.15
UNIT 25
COM='ARRAY FOR NORTH TOP REFLECTOR'
ARRAY 7 3*0.0
UNIT 26
COM='SOUTH TOP REFLECTOR WITH TRIS'
CUBOID 0 1 2P5.1 2P2.55 2P12.15
CUBOID 5 1 69.4 -5.1 2P64.05 2P12.15
UNIT 27
COM='ARRAY FOR SOUTH TOP REFLECTOR'
ARRAY 8 3*0.0
UNIT 28
COM='NORTH END REFLECTOR 9.8CM PORTION WITHOUT TRIS'
CUBOID 4 1 2P4.9000 2P64.0500 2P52.7825

UNIT 29
COM='NORTH END REFLECTOR 5.2 CM PORTION WITH TRIS'
CUBOID 5 1 2P2.6 2P64.0500 2P52.7825
UNIT 30
COM='NORTH END REFLECTOR 10.1 CM PORTION WITHOUT TRIS'
CUBOID 4 1 2P5.05 2P64.05 2P52.7825
UNIT 31
COM='ARRAY FOR NORTH END REFLECTOR'
ARRAY 9 3*0.0
UNIT 32
COM='SOUTH END REFLECTOR'
CUBOID 5 1 2P12.55 2P64.05 2P52.7825
UNIT 33
COM='ARRAY FOR SOUTH END REFLECTOR'
ARRAY 10 3*0.0
UNIT 34
COM='12.95 THICK MODERATING PLASTIC NORTH CORE'
CUBOID 0 1 2P16.5500 2P13.315 2P25.4350
UNIT 35
COM='2.95 THICK MODERATING PLASTIC NORTH CORE'
CUBOID 6 1 2P16.5500 2P38.75 2P1.7525
UNIT 36
ARRAY 11 3*0.0
UNIT 37
ARRAY 12 3*0.0
UNIT 38
COM='NORTH CORE WITH BOTTOM REFLECTOR'
ARRAY 13 3* 0.0
UNIT 39
COM='NORTH CORE WITH EAST AND WEST REFLECTOR'
ARRAY 14 3*0.0
UNIT 40
COM='NORTH CORE WITH END REFLECTOR'
ARRAY 15 3*0.0
UNIT 41
COM='NORTH SPLIT TABLE FACEPLATE'
CUBOID 3 1 2P0.61 2P64.0500 2P64.9325
UNIT 42
COM='NORTH CORE WITH TOP REFLECTOR'
ARRAY 16 3*0.0
UNIT 43
COM='NORTH CORE WITH FACEPLATE'
ARRAY 17 3*0.0
UNIT 44
COM='12.95 CM THICK MODERATOR SOUTH CORE'
CUBOID 0 1 2P16.5500 2P13.315 2P25.4350
UNIT 45
COM='2.95 THICK MODERATOR SOUTH CORE'
CUBOID 6 1 2P16.5500 2P38.75 2P1.7525
UNIT 46
COM='COMBINATION OF CORE WITH 12.95 THICK MODERATOR'
ARRAY 18 3*0.0
UNIT 47
COM='COMBINATION OF CORE WITH 2.95 THICK MODERATOR'
ARRAY 19 3*0.0
UNIT 48
COM='SOUTH CORE WITH EAST WEST REFLECTORS'
ARRAY 20 3*0.0
UNIT 49
COM='SOUTH CORE WITH EAST WEST REFLECTORS'
ARRAY 21 3*0.0
UNIT 50
COM='SOUTH CORE END REFLECTOR'
ARRAY 22 3*0.0

Table A.3 (continued)

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UNIT 51
COM='FACEPLATE FOR SOUTH SPLIT TABLE'
CUBOID 3 1 2P0.610 2P64.0500 2P64.9325
UNIT 52
COM='SOUTH CORE WITH TOP REFLECTOR'
ARRAY 23 3*0.0
UNIT 53
COM='SOUTH CORE WITH FACEPLATE'
ARRAY 24 3*0.0
UNIT 54
COM='AIR GAP'
CUBOID 0 1 2P0.2850 2P64.0500 2P64.9325
GLOBAL
UNIT 55
COM='TOTAL'
ARRAY 25 3*0.0
UNIT 56
COM='NORTH BOTTOM MODERATOR'
CUBOID 6 1 2P16.5500 2P38.7500 2P13.05
UNIT 57
COM='BOTTOM SOUTH MODERATOR'
CUBOID 6 1 2P24.700 2P38.75 2P13.05
UNIT 58
COM='REAR FILLER'
CUBOID 6 1 2P8.1500 2P38.75 2P27.1875
UNIT 59
COM='COMBINATION OF SOUTH CORE WITH REAR FILLER'
ARRAY 26 3*0.0
UNIT 60
COM='NORTH CORE REAR FILLER'
CUBOID 6 1 2P0.0 2P38.75 2P27.1875
UNIT 61
COM='COMBINATION OF NORTH CORE WITH REAR FILLER'
ARRAY 27 3*0.0
UNIT 62
COM='EMPTY FUEL LOCATION'
CUBOID 0 1 6P7.6650
UNIT 63
COM='Y-FACE MODERATOR VOID'
CUBOID 0 1 2P7.665 2P1.22 2P7.665
END GEOMETRY
READ ARRAY
ARA=1 NUX=3 NUY=5 NUZ=5
COM='NORTH SPLIT TABLE CORE'
FILL 1 2 1 3 5 3 1Q6 1 2 1
      4 7 4 6 8 6 1Q6 4 7 4
      1Q30
      62 2 1 63 5 3 1Q6 62 2 1 END FILL
ARA=2 NUX=3 NUY=5 NUZ=5
COM='SOUTH SPLIT TABLE CORE'
FILL 1 2 1 3 5 3 1Q6 1 2 1
      4 7 4 6 8 6 1Q6 4 7 4
      1Q30
      1 2 62 3 5 63 1Q6 1 2 62 END FILL
ARA=3 NUX=1 NUY=1 NUZ=4
COM='NORTH BOTTOM MODERATOR AND REFLECTOR'
FILL 14 11 13 56 END FILL
ARA=4 NUX=1 NUY=1 NUZ=8
COM='SOUTH BOTTOM MODERATOR AND REFLECTOR'
FILL 18 16 17 16 16 17 17 57 END FILL
ARA=5 NUX=1 NUY=1 NUZ=1
COM='EAST AND WEST WALLS OF NORTH REFLECTOR'
FILL 20 END FILL

ARA=6 NUX=1 NUY=1 NUZ=1
COM='EAST AND WEST WALLS OF SOUTH REFLECTOR'
FILL 22 END FILL
ARA=7 NUX=1 NUY=1 NUZ=1
COM='ARRAY FOR NORTH TOP REFLECTOR'
FILL 24 END FILL
ARA=8 NUX=1 NUY=1 NUZ=1
COM='ARRAY FOR SOUTH TOP REFLECTOR'
FILL 26 END FILL
ARA=9 NUX=3 NUY=1 NUZ=1
COM='ARRAY FOR NORTH END REFLECTOR'
FILL 28 29 30 END FILL
ARA=10 NUX=1 NUY=1 NUZ=1
COM='ARRAY FOR SOUTH END REFLECTOR'
FILL 32 END FILL
ARA=11 NUX=1 NUY=2 NUZ=1
COM='COMBINARION OF CORE WITH 12.95CM THICK MODERATOR'
FILL 9 34 END FILL
ARA=12 NUX=1 NUY=1 NUZ=2
COM='COMBINATION OF PREVIOUS ARRAY WITH 2.95CM THICK MODERATOR'
FILL 36 35 END FILL
ARA=13 NUX=1 NUY=1 NUZ=2
COM='COMBINATION OF NORTH CORE WITH BOTTOM REFLECTOR'
FILL 15 61 END FILL
ARA=14 NUX=1 NUY=3 NUZ=1
COM='NORTH CORE WITH SIDE REFLECTORS'
FILL 21 38 21 END FILL
ARA=15 NUX=2 NUY=1 NUZ=1
COM='NORTH CORE WITH END REFLECTOR'
FILL 31 39 END FILL
ARA=16 NUX=1 NUY=1 NUZ=2
COM='NORTH CORE WITH TOP REFLECTOR'
FILL 40 25 END FILL
ARA=17 NUX=2 NUY=1 NUZ=1
COM='NORTH CORE WITH FACEPLATE'
FILL 42 41 END FILL
ARA=18 NUX=1 NUY=2 NUZ=1
COM='COMBINATION OF S. CORE WITH 12.95 CM THICK MODERATOR'
FILL 10 44 END FILL
ARA=19 NUX=1 NUY=1 NUZ=2
COM='COMBINATION OF CORE WITH 2.95 CM THICK MODERATOR'
FILL 46 45 END FILL
ARA=20 NUX=1 NUY=1 NUZ=2
COM='SOUTH CORE WITH BOTTOM REFLECTOR'
FILL 19 59 END FILL
ARA=21 NUX=1 NUY=3 NUZ=1
COM='SOUTH CORE WITH EAST WEST REFLECTORS'
FILL 23 48 23 END FILL
ARA=22 NUX=2 NUY=1 NUZ=1
COM='SOUTH CORE WITH END REFLECTOR'
FILL 49 33 END FILL
ARA=23 NUX=1 NUY=1 NUZ=2
COM='COMBINATION OF CORE WITH TOP REFLECTOR'
FILL 50 27 END FILL
ARA=24 NUX=2 NUY=1 NUZ=1
COM='SOUTH CORE WITH FACEPLATE'
FILL 51 52 END FILL
ARA=25 NUX=3 NUY=1 NUZ=1
COM='TOTAL'
FILL 43 54 53 END FILL
ARA=26 NUX=2 NUY=1 NUZ=1
COM='COMBINATION OF SOUTH CORE WITH REAR FILLER'
FILL 47 58 END FILL

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Table A.3 (continued)

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ARA=27 NUX=2 NUY=1 NUZ=1
COM='COMBINATION OF NORTH CORE WITH REAR FILLER'
FILL 37 60 END FILL
END ARRAY
READ PLOT TTL='XZ SLICE OF RFPG SHOWING MATERIAL REGIONS'
XUL=-1 YUL=64.05 ZUL=135
XLR=136 YLR=64.05 ZLR=-2
UAX=1 WDN=-1 NAX=130 NCH='0123456'END
TTL='YZ SLICE OF NORTH CORE FIRST ROW'
XUL=48 YUL=-2 ZUL=136
XLR=48 YLR=136 ZLR=-2
VAX=1 WDN=-1 NAX=130 NCH='0123456'END
TTL='YZ SLICE OF NORTH CORE SECOND ROW'
XUL=28 YUL=-2 ZUL=136
XLR=28 YLR=136 ZLR=-2
VAX=1 WDN=-1 NAX=130 NCH='0123456'END
TTL='YZ SLICE OF SOUTH CORE FIRST ROW'
XUL=62 YUL=-2 ZUL=136
XLR=62 YLR=136 ZLR=-2
VAX=1 WDN=-1 NAX=130 NCH='0123456'END
TTL='TOP VIEW OF SOURCE SLOT'
XUL=-2 YUL=136 ZUL=125
XLR=138 YLR=-2 ZLR=125
UAX=1 VDN=-1 NAX=130 NCH='0123456'END
TTL='TOP VIEW OF TOP LAYER'
XUL=-2 YUL=136 ZUL=95
XLR=138 YLR=-2 ZLR=95
UAX=1 VDN=-1 NAX=130 NCH='0123456'
END PLOT
READ START NST=1
XSP=100.0 XSM=10.0
YSP=100.0 YSM=10.0
ZSP=117.0 ZSM=60.0
END DATA
END

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CAR19
=CSAS25
ROCKY PLATS CRITICALS NUREG/CR-2500 EXPERIMENT NUMBER ? (27 GROUP MODEL)
' FUEL CUBE 15.28 CM, U(4.46)308 @ H/U=2.03, HI ENRICHED SPHERE DRIVEN
27GROUPNDF4 INFHOMMEDIUM
U308 1 5.4078E-1 293.0 92234 0.03 92235 4.46 92236 0.08 92238 95.43 END
H20 1 2.6356E-1 END
ARBM-BAGGIE 1.0 3 0 0 0 1001 14.01 6012 84.9 8016 1.20 1 1.9134E-2
END
ARBM-AL1100 1.0 3 0 0 1 13027 99.18 26000 0.5 29000 0.2 2 9.5390E-1
END
ARBM-TAPE(VINYL) 1.0 7 0 0 0 1001 5.92 6012 45.91 8016 10.82 17000
25.73 20040 6.9 22000 1.6 82000 1.1 2 1.1115E-2 END
ARBM-TAPE(MYLAR) 1.0 3 0 0 0 1001 6.83 6012 65.50 8016 27.02 2
1.7491E-2 END
ARBM-MODERATOR 1.185 3 0 0 0 1001 7.83 6012 59.49 8016 32.48 3 END
ARBM-FLEX(REG) 1.0 3 0 0 0 1001 7.84 6012 59.59 8016 32.23 4
1.1773 END
ARBM-PLEX(PAPER) 1.0 3 0 0 0 1001 6.48 6012 42.17 8016 49.5 4
3.7534E-3 END
ARBM-PLEX(GLUE) 1.0 3 0 0 0 1001 11.67 6012 86.29 8016 1.20 4
1.1648E-3 END

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ARBM-PLEX(TRIS) 1.0 8 0 0 1 1001 7.16 6012 52.03 7014 0.16 8016 29.82
15031 1.02 17000 1.81 35079 4.260 35081 2.840 5 1.2757 END
ARBM-PLEX(PAPER) 1.0 3 0 0 0 1001 6.48 6012 42.17 8016 49.5 5
3.7534E-3 END
ARBM-PLEX(GLUE) 1.0 3 0 0 0 1001 11.67 6012 86.29 8016 1.20 5
1.1648E-3 END
ARBM-FILLER 1.185 3 0 0 0 1001 7.83 6012 59.49 8016 32.48 6 0.7 END
' THIS MATERIAL IS ACTUALLY MODERATOR ADJUSTED FOR THE VOLUME
' FRACTION OF THE VOID FILLED BETWEEN CORE AND REFLECTOR.
ARBM-AL1100 1.0 3 0 0 1 13027 99.18 26000 0.5 29000 0.2 7 2.715 END
URANIUM 8 0.9483 293.0 92234 1.0 92235 93.19 92236 0.4 92238 5.41 END
ARBM-PJ 0.816 2 0 0 0 1001 85.1 6012 14.9 8 0.0089 END
SS304 9 1.0 END
END COMP
ROCKY PLATS CRITICALS NUREG/CR-2500 EXPERIMENT NUMBER ? (27 GROUP MODEL)
' FUEL CUBE 15.28 CM, U(4.46)308 @ H/U=2.03, HI ENRICHED SPHERE DRIVEN
READ PARM NPG=600 NUB=YES FDN=YES PLT=NO END PARM
READ GEOM
UNIT 1
COM='FUEL BOX WITH VOID AND PART OF AL BOX'
CUBOID 0 1 9.80 0.0 3.75 0.0 14.98 0.0
CUBOID 2 1 9.95 0.0 3.90 -0.15 14.98 0.0
CUBOID 1 1 14.98 0.0 9.365 -5.615 14.98 0.0
UNIT 2
COM='FRONT OF FUEL BOX'
CUBOID 2 1 0.15 0.0 5.615 0.0 14.98 0.0
CUBOID 0 1 0.15 0.0 9.365 0.0 14.98 0.0
CUBOID 2 1 0.15 0.0 14.98 0.0 14.98 0.0
UNIT 3
COM='REAR OF FUEL BOX'
CUBOID 2 1 0.15 0.0 14.98 0.0 14.98 0.0
UNIT 4
COM='ARRAY TO ASSEMBLE PART OF BOX'
ARRAY 26 3*0
UNIT 5
COM='TOP AND BOTTOM OF BOX'
CUBOID 0 1 9.80 0.0 3.750 0.0 0.15 0.0
CUBOID 2 1 15.28 0.0 9.365 -5.615 0.15 0.0
GLOBAL
UNIT 6
COM='ARRAY TO ASSEMBLE TOP AND BOTTOM'
ARRAY 27 3*0
CUBOID 2 1 15.28 0.0 15.13 -0.15 15.28 0.0
CUBOID 0 1 15.305 -0.025 15.155 -0.175 15.305 -0.025
UNIT 7
COM='FUEL BOX 15.28 CM ON A SIDE WITH .15 CM WALLS .05CM STACKING VOID'
CUBOID 1 1 6P7.49
CUBOID 2 1 6P7.64
CUBOID 0 1 6P7.6650
UNIT 8
COM='BOX FOR DRIVER'
CYLINDER 9 1 0.3175 2P5.66
SPHERE 8 1 5.67
CUBOID 0 1 9.62 -5.71 2P7.665 7.365 -7.965
HOLE 37 0.0 0.0 -7.965
UNIT 34
COM='ALUMINUM WEIGHT DISTRIBUTION PLATE FOR SPECIAL BOX'
CUBOID 0 1 9.80 0.0 3.750 0.0 0.16 0.0
CUBOID 7 1 15.33 0.0 9.54 -5.79 0.16 0.0
UNIT 35
COM='ALUMINUM WEIGHT DISTRIBUTION PLATE FOR BOXES'
CUBOID 7 1 4P7.665 0.16 0.0

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Table A.3 (continued)

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UNIT 37
COM='DRIVER MOUNT'
CYLINDER 9 1 1.56 2.2 0.0
UNIT 9
COM='NORTH SPLIT TABLE CORE'
ARRAY 1 3*0.0
CUBOID 0 1 30.66 -0.94 77.5 0.0 83.475 0.0
UNIT 10
COM='SOUTH SPLIT TABLE CORE'
ARRAY 2 3*0.0
CUBOID 0 1 49.4 0.0 77.5 0.0 83.475 0.0
UNIT 11
COM='PLEXIGLASS REFLECTOR SHEET WITHOUT TRIS, NORTH BOTTOM REFLECTOR'
CUBOID 4 1 2P15.8000 2P38.7500 2P0.6150
UNIT 12
COM='PLEXIGLASS REFLECTOR SHEET WITH TRIS, NORTH BOTTOM REFLECTOR'
CUBOID 5 1 2P15.8000 2P38.7500 2P0.6150
UNIT 13
COM='UPPER PORTION NORTH BOTTOM REFLECTOR WITH TRIS'
CUBOID 5 1 2P15.8 2P38.75 2P8.24
UNIT 14
COM='LOWER PORTION NORTH BOTTOM REFLECTOR WITH TRIS'
CUBOID 5 1 2P15.8 2P38.75 2P3.69
UNIT 15
COM='NORTH BOTTOM REFLECTOR INCLUDES REGULAR AND TRIS'
ARRAY 3 3*0.0
UNIT 16
COM='PLEXIGLAS SHEET BOTTOM SOUTH REFLECTOR WITHOUT TRIS'
CUBOID 0 1 2P5.1 2P2.5 2P0.6150
CUBOID 4 1 44.3 -5.1 2P38.75 2P0.615
UNIT 17
COM='PLEXIGLAS SHEET BOTTOM SOUTH REFLECTOR WITH TRIS'
CUBOID 0 1 2P5.1 2P2.5 2P0.6150
CUBOID 5 1 44.3 -5.1 2P38.75 2P0.6150
UNIT 18
COM='LOWER PORTION SOUTH BOTTOM REFLECTOR WITH TRIS'
CUBOID 0 1 2P5.1 2P2.5 2P8.855
CUBOID 5 1 44.3 -5.1 2P38.75 2P8.855
UNIT 19
COM='SOUTH BOTTOM REFLECTOR WITH REGULAR AND TRIS'
ARRAY 4 3*0.0
UNIT 20
COM='EAST AND WEST REFLECTORS FOR NORTH REFLECTOR WITH TRIS'
CUBOID 5 1 2P15.8 2P12.65 2P54.2825
UNIT 21
COM='ARRAY FOR EAST AND WEST REFLECTORS FOR NORTH REFLECTOR'
ARRAY 5 3*0.0
UNIT 22
COM='EAST AND WEST REFLECTORS FOR SOUTH REFLECTOR WITH TRIS'
CUBOID 5 1 2P24.700 2P12.65 2P54.2825
UNIT 23
COM='ARRAY FOR EAST AND WEST REFLECTORS FOR SOUTH REFLECTOR'
ARRAY 6 3*0.0
UNIT 24
COM='NORTH TOP REFLECTOR WITH TRIS'
CUBOID 5 1 2P28.35 2P64.05 2P12.15
UNIT 25
COM='ARRAY FOR NORTH TOP REFLECTOR'
ARRAY 7 3*0.0
UNIT 26
COM='SOUTH TOP REFLECTOR WITH TRIS'
CUBOID 0 1 2P5.1 2P2.5 2P12.15
CUBOID 5 1 69.4 -5.1 2P64.05 2P12.15

UNIT 27
COM='ARRAY FOR SOUTH TOP REFLECTOR'
ARRAY 8 3*0.0
UNIT 28
COM='NORTH END REFLECTOR 9.8CM PORTION WITHOUT TRIS'
CUBOID 4 1 2P4.9000 2P64.0500 2P54.2825
UNIT 29
COM='NORTH END REFLECTOR 5.2 CM PORTION WITH TRIS'
CUBOID 5 1 2P2.6 2P64.0500 2P54.2825
UNIT 30
COM='NORTH END REFLECTOR 10.1 CM PORTION WITHOUT TRIS'
CUBOID 4 1 2P5.05 2P64.05 2P54.2825
UNIT 31
COM='ARRAY FOR NORTH END REFLECTOR'
ARRAY 9 3*0.0
UNIT 32
COM='SOUTH END REFLECTOR'
CUBOID 5 1 2P12.55 2P64.05 2P54.2825
UNIT 33
COM='ARRAY FOR SOUTH END REFLECTOR'
ARRAY 10 3*0.0
UNIT 38
COM='NORTH CORE WITH BOTTOM REFLECTOR'
ARRAY 13 3* 0.0
UNIT 39
COM='NORTH CORE WITH EAST AND WEST REFLECTOR'
ARRAY 14 3*0.0
UNIT 40
COM='NORTH CORE WITH END REFLECTOR'
ARRAY 15 3*0.0
UNIT 42
COM='NORTH CORE WITH TOP REFLECTOR'
ARRAY 16 3*0.0
UNIT 48
COM='SOUTH CORE WITH BOTTOM REFLECTORS'
ARRAY 20 3*0.0
UNIT 49
COM='SOUTH CORE WITH EAST WEST REFLECTORS'
ARRAY 21 3*0.0
UNIT 50
COM='SOUTH CORE END REFLECTOR'
ARRAY 22 3*0.0
UNIT 52
COM='SOUTH CORE WITH TOP REFLECTOR'
ARRAY 23 3*0.0
UNIT 54
COM='AIR GAP'
CUBOID 0 1 1.49 0.0 64.475 -63.625 69.13 -63.735
GLOBAL
UNIT 55
COM='TOTAL'
ARRAY 25 3*0.0
END GEOMETRY
READ ARRAY
ARA=1 NUX=2 NUY=5 NUZ=9
COM='NORTH SPLIT TABLE CORE'
FILL 10R7
10R35
10R7
10R35
10R7
10R35
10R7
10R35
10R7
10R35
10R7 END FILL

```

Table A.3 (continued)

```

ARA=2  NUX=3  NUY=5  NUZ=9
COM='SOUTH SPLIT TABLE CORE'
FILL  6R7 6 8R7
      6R35 34 8R35
      6R7 6 8R7
      6R35 34 8R35
      6R7 8 8R7
      6R35 34 8R35
      6R7 6 8R7
      6R35 34 8R35
      6R7 6 8R7  END FILL
ARA=3  NUX=1  NUY=1  NUZ=3
COM='NORTH BOTTOM REFLECTOR'
FILL  14 11 13  END FILL
ARA=4  NUX=1  NUY=1  NUZ=7
COM='SOUTH BOTTOM REFLECTOR'
FILL  18 16 17 16 16 17 17  END FILL
ARA=5  NUX=1  NUY=1  NUZ=1
COM='EAST AND WEST WALLS OF NORTH REFLECTOR'
FILL  20  END FILL
ARA=6  NUX=1  NUY=1  NUZ=1
COM='EAST AND WEST WALLS OF SOUTH REFLECTOR'
FILL  22  END FILL
ARA=7  NUX=1  NUY=1  NUZ=1
COM='ARRAY FOR NORTH TOP REFLECTOR'
FILL  24  END FILL
ARA=8  NUX=1  NUY=1  NUZ=1
COM='ARRAY FOR SOUTH TOP REFLECTOR'
FILL  26  END FILL
ARA=9  NUX=3  NUY=1  NUZ=1
COM='ARRAY FOR NORTH END REFLECTOR'
FILL  28 29 30  END FILL
ARA=10 NUX=1  NUY=1  NUZ=1
COM='ARRAY FOR SOUTH END REFLECTOR'
FILL  32  END FILL
ARA=13 NUX=1  NUY=1  NUZ=2
COM='COMBINATION OF NORTH CORE WITH BOTTOM REFLECTOR'
FILL  15 9  END FILL
ARA=14 NUX=1  NUY=3  NUZ=1
COM='NORTH CORE WITH SIDE REFLECTORS'
FILL  21 38 21  END FILL
ARA=15 NUX=2  NUY=1  NUZ=1
COM='NORTH CORE WITH END REFLECTOR'
FILL  31 39  END FILL
ARA=16 NUX=1  NUY=1  NUZ=2
COM='NORTH CORE WITH TOP REFLECTOR'
FILL  40 25  END FILL
ARA=20 NUX=1  NUY=1  NUZ=2
COM='SOUTH CORE WITH BOTTOM REFLECTOR'
FILL  19 10  END FILL
ARA=21 NUX=1  NUY=3  NUZ=1
COM='SOUTH CORE WITH EAST WEST REFLECTORS'
FILL  23 48 23  END FILL
ARA=22 NUX=2  NUY=1  NUZ=1
COM='SOUTH CORE WITH END REFLECTOR'
FILL  49 33  END FILL
ARA=23 NUX=1  NUY=1  NUZ=2
COM='COMBINATION OF CORE WITH TOP REFLECTOR'
FILL  50 27  END FILL
ARA=25 NUX=3  NUY=1  NUZ=1
COM='TOTAL'
FILL  42 54 52  END FILL
ARA=26 NUX=3  NUY=1  NUZ=1
COM='ASSEMBLY OF FUEL BOX FRONT AND REAR'
FILL  2 1 3  END FILL

ARA=27 NUX=1  NUY=1  NUZ=3
COM='ASSEMBLY OF FUEL BOX TOP AND BOTTOM'
FILL  5 4 5  END FILL
END ARRAY
READ PLOT TTL='YZ SLICE OF SOUTH CORE FIRST ROW'
XUL=64.319 YUL=55.625 ZUL=71.735
XLR=64.319 YLR=71.625 ZLR=55.735
VAX=1 WDN=-1 NAX=130 NCH='012345678' END
TTL='XZ SLICE OF SPHERE CUBOID'
XUL=56.0 YUL=63.625 ZUL=71.735
XLR=72.0 YLR=63.625 ZLR=55.735
UAX=1 WDN=-1 NAX=130 NCH='012345678'
END PLOT
' READ START NST=6 TFX=65 TFY=63.625 TFZ=63.735 LNU=300 END START
READ START NST=1 XSM=56.981 XSP=71.649 YSM=56.219 YSP=70.959
ZSM=56.401 ZSP=71.069 END START
END DATA
END

CAR20
=CSAS25
ROCKY FLATS CRITICALS NUREG/CR-2500 EXPERIMENT NUMBER ? (27 GROUP MODEL)
' FUEL CUBE 15.28 CM, U(4.46)308 @ H/U=2.03, HI ENRICHED SPHERE DRIVEN
27GROUPNDF4 INFHOMMEDIUM
U308 1 5.4078E-1 293.0 92234 0.03 92235 4.46 92236 0.08 92238 95.43 END
H2O 1 2.6356E-1 END
ARBM-BAGGIE 1.0 3 0 0 0 1001 14.01 6012 84.9 8016 1.20 1 1.9134E-2
END
ARBM-AL1100 1.0 3 0 0 1 13027 99.18 26000 0.5 29000 0.2 2 9.5390E-1
END
ARBM-TAPE(VINYL) 1.0 7 0 0 0 1001 5.92 6012 45.91 8016 10.82 17000
25.73 20040 6.9 22000 1.6 82000 1.1 2 1.1115E-2 END
ARBM-TAPE(MYLAR) 1.0 3 0 0 0 1001 6.83 6012 65.50 8016 27.02 2
1.7491E-2 END
ARBM-MODERATOR 1.185 3 0 0 0 1001 7.83 6012 59.49 8016 32.48 3 END
ARBM-PLEX(REG) 1.0 3 0 0 0 1001 7.84 6012 59.59 8016 32.23 4
1.1773 END
ARBM-PLEX(PAPER) 1.0 3 0 0 0 1001 6.48 6012 42.17 8016 49.5 4
3.7534E-3 END
ARBM-PLEX(GLUE) 1.0 3 0 0 0 1001 11.67 6012 86.29 8016 1.20 4
1.1648E-3 END
ARBM-PLEX(TRIS) 1.0 8 0 0 1 1001 7.16 6012 52.03 7014 0.16 8016 29.82
15031 1.02 17000 1.81 35079 4.260 35081 2.840 5 1.2757 END
ARBM-PLEX(PAPER) 1.0 3 0 0 0 1001 6.48 6012 42.17 8016 49.5 5
3.7534E-3 END
ARBM-PLEX(GLUE) 1.0 3 0 0 0 1001 11.67 6012 86.29 8016 1.20 5
1.1648E-3 END
ARBM-FILLER 1.185 3 0 0 0 1001 7.83 6012 59.49 8016 32.48 6 0.7 END
' THIS MATERIAL IS ACTUALLY MODERATOR ADJUSTED FOR THE VOLUME
' FRACTION OF THE VOID FILLED BETWEEN CORE AND REFLECTOR.
ARBM-AL1100 1.0 3 0 0 1 13027 99.18 26000 0.5 29000 0.2 7 2.715 END
URANIUM 8 0.9483 293.0 92234 1.0 92235 93.19 92236 0.4 92238 5.41 END
ARBM-PJ 0.816 2 0 0 0 1001 85.1 6012 14.9 8 0.0089 END
SS304 9 1.0 END
END COMP
ROCKY FLATS CRITICALS NUREG/CR-2500 EXPERIMENT NUMBER ? (27 GROUP MODEL)
' FUEL CUBE 15.28 CM, U(4.46)308 @ H/U=2.03, HI ENRICHED SPHERE DRIVEN
READ PARM NPG=600 NUB=YES FDN=YES PLT=NO END PARM
READ GEOM

```

Table A.3 (continued)

```

UNIT 1
COM='FUEL BOX WITH VOID AND PART OF AL BOX'
CUBOID 0 1 9.80 0.0 3.75 0.0 14.98 0.0
CUBOID 2 1 9.95 0.0 3.90 -0.15 14.98 0.0
CUBOID 1 1 14.98 0.0 9.365 -5.615 14.98 0.0
UNIT 2
COM='FRONT OF FUEL BOX'
CUBOID 2 1 0.15 0.0 5.615 0.0 14.98 0.0
CUBOID 0 1 0.15 0.0 9.365 0.0 14.98 0.0
CUBOID 2 1 0.15 0.0 14.98 0.0 14.98 0.0
UNIT 3
COM='REAR OF FUEL BOX'
CUBOID 2 1 0.15 0.0 14.98 0.0 14.98 0.0
UNIT 4
COM='ARRAY TO ASSEMBLE PART OF BOX'
ARRAY 26 3*0
UNIT 5
COM='TOP AND BOTTOM OF BOX'
CUBOID 0 1 9.80 0.0 3.750 0.0 0.15 0.0
CUBOID 2 1 15.28 0.0 9.365 -5.615 0.15 0.0
GLOBAL
UNIT 6
COM='ARRAY TO ASSEMBLE TOP AND BOTTOM'
ARRAY 27 3*0
CUBOID 2 1 15.28 0.0 15.13 -0.15 15.28 0.0
CUBOID 0 1 15.305 -0.025 15.155 -0.175 15.305 -0.025
UNIT 7
COM='FUEL BOX 15.28 CM ON A SIDE WITH .15 CM WALLS .05CM STACKING VOID'
CUBOID 1 1 6P7.49
CUBOID 2 1 6P7.64
CUBOID 0 1 6P7.6650
UNIT 8
COM='BOX FOR DRIVER'
CYLINDER 9 1 0.3175 2P2.318
SPHERE 0 1 2.34
SPHERE 8 1 5.67
HOLE 36 0.0 0.0 2.3401
HOLE 100 0.0 0.0 -2.3401
CUBOID 0 1 8.71 -6.62 2P7.665 7.365 -7.965
HOLE 37 0.0 0.0 -7.965
UNIT 34
COM='ALUMINUM WEIGHT DISTRIBUTION PLATE FOR SPECIAL BOX'
CUBOID 0 1 9.80 0.0 3.750 0.0 0.16 0.0
CUBOID 7 1 15.33 0.0 9.54 -5.79 0.16 0.0
UNIT 35
COM='ALUMINUM WEIGHT DISTRIBUTION PLATE FOR BOXES'
CUBOID 7 1 4P7.665 0.16 0.0
UNIT 36
COM='DRIVER SUPPORT'
CYLINDER 9 1 0.3175 3.32 0.0
UNIT 100
COM='DRIVER SUPPORT'
CYLINDER 9 1 0.3175 0.0 -3.32
UNIT 37
COM='DRIVER MOUNT'
CYLINDER 9 1 1.56 2.2 0.0
UNIT 9
COM='NORTH SPLIT TABLE CORE'
ARRAY 1 3*0.0
CUBOID 0 1 30.66 -0.94 77.5 0.0 83.475 0.0
UNIT 10
COM='SOUTH SPLIT TABLE CORE'
ARRAY 2 3*0.0
CUBOID 0 1 49.4 0.0 77.5 0.0 83.475 0.0

UNIT 11
COM='PLEXIGLASS REFLECTOR SHEET WITHOUT TRIS, NORTH BOTTOM REFLECTOR'
CUBOID 4 1 2P15.8000 2P38.7500 2P0.6150
UNIT 12
COM='PLEXIGLASS REFLECTOR SHEET WITH TRIS, NORTH BOTTOM REFLECTOR'
CUBOID 5 1 2P15.8000 2P38.7500 2P0.6150
UNIT 13
COM='UPPER PORTION NORTH BOTTOM REFLECTOR WITH TRIS'
CUBOID 5 1 2P15.8 2P38.75 2P8.24
UNIT 14
COM='LOWER PORTION NORTH BOTTOM REFLECTOR WITH TRIS'
CUBOID 5 1 2P15.8 2P38.75 2P3.69
UNIT 15
COM='NORTH BOTTOM REFLECTOR INCLUDES REGULAR AND TRIS'
ARRAY 3 3*0.0
UNIT 16
COM='PLEXIGLAS SHEET BOTTOM SOUTH REFLECTOR WITHOUT TRIS'
CUBOID 0 1 2P5.1 2P2.5 2P0.6150
CUBOID 4 1 44.3 -5.1 2P38.75 2P0.615
UNIT 17
COM='PLEXIGLAS SHEET BOTTOM SOUTH REFLECTOR WITH TRIS'
CUBOID 0 1 2P5.1 2P2.5 2P0.6150
CUBOID 5 1 44.3 -5.1 2P38.75 2P0.6150
UNIT 18
COM='LOWER PORTION SOUTH BOTTOM REFLECTOR WITH TRIS'
CUBOID 0 1 2P5.1 2P2.5 2P8.855
CUBOID 5 1 44.3 -5.1 2P38.75 2P8.855
UNIT 19
COM='SOUTH BOTTOM REFLECTOR WITH REGULAR AND TRIS'
ARRAY 4 3*0.0
UNIT 20
COM='EAST AND WEST REFLECTORS FOR NORTH REFLECTOR WITH TRIS'
CUBOID 5 1 2P15.8 2P12.65 2P54.2825
UNIT 21
COM='ARRAY FOR EAST AND WEST REFLECTORS FOR NORTH REFLECTOR'
ARRAY 5 3*0.0
UNIT 22
COM='EAST AND WEST REFLECTORS FOR SOUTH REFLECTOR WITH TRIS'
CUBOID 5 1 2P24.700 2P12.65 2P54.2825
UNIT 23
COM='ARRAY FOR EAST AND WEST REFLECTORS FOR SOUTH REFLECTOR'
ARRAY 6 3*0.0
UNIT 24
COM='NORTH TOP REFLECTOR WITH TRIS'
CUBOID 5 1 2P28.35 2P64.05 2P12.15
UNIT 25
COM='ARRAY FOR NORTH TOP REFLECTOR'
ARRAY 7 3*0.0
UNIT 26
COM='SOUTH TOP REFLECTOR WITH TRIS'
CUBOID 0 1 2P5.1 2P2.5 2P12.15
CUBOID 5 1 69.4 -5.1 2P64.05 2P12.15
UNIT 27
COM='ARRAY FOR SOUTH TOP REFLECTOR'
ARRAY 8 3*0.0
UNIT 28
COM='NORTH END REFLECTOR 9.8CM PORTION WITHOUT TRIS'
CUBOID 4 1 2P4.9000 2P64.0500 2P54.2825
UNIT 29
COM='NORTH END REFLECTOR 5.2 CM PORTION WITH TRIS'
CUBOID 5 1 2P2.6 2P64.0500 2P54.2825
UNIT 30
COM='NORTH END REFLECTOR 10.1 CM PORTION WITHOUT TRIS'
CUBOID 4 1 2P5.05 2P64.05 2P54.2825

```


Table A.3 (continued)

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UNIT 31
COM='ARRAY FOR NORTH END REFLECTOR'
ARRAY 9 3*0.0
UNIT 32
COM='SOUTH END REFLECTOR'
CUBOID 5 1 2P12.55 2P64.05 2P54.2825
UNIT 33
COM='ARRAY FOR SOUTH END REFLECTOR'
ARRAY 10 3*0.0
UNIT 38
COM='NORTH CORE WITH BOTTOM REFLECTOR'
ARRAY 13 3* 0.0
UNIT 39
COM='NORTH CORE WITH EAST AND WEST REFLECTOR'
ARRAY 14 3*0.0
UNIT 40
COM='NORTH CORE WITH END REFLECTOR'
ARRAY 15 3*0.0
UNIT 42
COM='NORTH CORE WITH TOP REFLECTOR'
ARRAY 16 3*0.0
UNIT 48
COM='SOUTH CORE WITH BOTTOM REFLECTORS'
ARRAY 20 3*0.0
UNIT 49
COM='SOUTH CORE WITH EAST WEST REFLECTORS'
ARRAY 21 3*0.0
UNIT 50
COM='SOUTH CORE END REFLECTOR'
ARRAY 22 3*0.0
UNIT 52
COM='SOUTH CORE WITH TOP REFLECTOR'
ARRAY 23 3*0.0
UNIT 54
COM='AIR GAP'
CUBOID 0 1 1.49 0.0 64.475 -63.625 69.13 -63.735
GLOBAL
UNIT 55
COM='TOTAL'
ARRAY 25 3*0.0
END GEOMETRY
READ ARRAY
ARA=1 NUX=2 NUY=5 NUZ=9
COM='NORTH SPLIT TABLE CORE'
FILL 10R7
      10R35
      10R7
      10R35
      10R7
      10R35
      10R7
      10R35
      10R7 END FILL
ARA=2 NUX=3 NUY=5 NUZ=9
COM='SOUTH SPLIT TABLE CORE'
FILL 6R7 6 8R7
      6R35 34 8R35
      6R7 6 8R7
      6R35 34 8R35
      6R7 8 8R7
      6R35 34 8R35
      6R7 6 8R7
      6R35 34 8R35

```

```

ARA=3 NUX=1 NUY=1 NUZ=3
COM='NORTH BOTTOM REFLECTOR'
FILL 14 11 13 END FILL
ARA=4 NUX=1 NUY=1 NUZ=7
COM='SOUTH BOTTOM REFLECTOR'
FILL 18 16 17 16 16 17 17 END FILL
ARA=5 NUX=1 NUY=1 NUZ=1
COM='EAST AND WEST WALLS OF NORTH REFLECTOR'
FILL 20 END FILL
ARA=6 NUX=1 NUY=1 NUZ=1
COM='EAST AND WEST WALLS OF SOUTH REFLECTOR'
FILL 22 END FILL
ARA=7 NUX=1 NUY=1 NUZ=1
COM='ARRAY FOR NORTH TOP REFLECTOR'
FILL 24 END FILL
ARA=8 NUX=1 NUY=1 NUZ=1
COM='ARRAY FOR SOUTH TOP REFLECTOR'
FILL 26 END FILL
ARA=9 NUX=3 NUY=1 NUZ=1
COM='ARRAY FOR NORTH END REFLECTOR'
FILL 28 29 30 END FILL
ARA=10 NUX=1 NUY=1 NUZ=1
COM='ARRAY FOR SOUTH END REFLECTOR'
FILL 32 END FILL
ARA=13 NUX=1 NUY=1 NUZ=2
COM='COMBINATION OF NORTH CORE WITH BOTTOM REFLECTOR'
FILL 15 9 END FILL
ARA=14 NUX=1 NUY=3 NUZ=1
COM='NORTH CORE WITH SIDE REFLECTORS'
FILL 21 38 21 END FILL
ARA=15 NUX=2 NUY=1 NUZ=1
COM='NORTH CORE WITH END REFLECTOR'
FILL 31 39 END FILL
ARA=16 NUX=1 NUY=1 NUZ=2
COM='NORTH CORE WITH TOP REFLECTOR'
FILL 40 25 END FILL
ARA=20 NUX=1 NUY=1 NUZ=2
COM='SOUTH CORE WITH BOTTOM REFLECTOR'
FILL 19 10 END FILL
ARA=21 NUX=1 NUY=3 NUZ=1
COM='SOUTH CORE WITH EAST WEST REFLECTORS'
FILL 23 48 23 END FILL
ARA=22 NUX=2 NUY=1 NUZ=1
COM='SOUTH CORE WITH END REFLECTOR'
FILL 49 33 END FILL
ARA=23 NUX=1 NUY=1 NUZ=2
COM='COMBINATION OF CORE WITH TOP REFLECTOR'
FILL 50 27 END FILL
ARA=25 NUX=3 NUY=1 NUZ=1
COM='TOTAL'
FILL 42 54 52 END FILL
ARA=26 NUX=3 NUY=1 NUZ=1
COM='ASSEMBLY OF FUEL BOX FRONT AND REAR'
FILL 2 1 3 END FILL
ARA=27 NUX=1 NUY=1 NUZ=3
COM='ASSEMBLY OF FUEL BOX TOP AND BOTTOM'
FILL 5 4 5 END FILL
END ARRAY

```

Table A.3 (continued)

```
READ PLOT TTL='YZ SLICE OF SOUTH CORE FIRST ROW'  
XUL=64.319 YUL=55.625 ZUL=71.735  
XLR=64.319 YLR=71.625 ZLR=55.735  
VAX=1 WDN=-1 NAX=130 NCH='012345678'END  
TTL='XZ SLICE OF SPHERE CUBOID'  
XUL=56.0 YUL=63.625 ZUL=71.735  
XLR=72.0 YLR=63.625 ZLR=55.735  
UAX=1 WDN=-1 NAX=130 NCH='012345678'  
END PLOT  
  READ START NST=6 TFX=65 TFY=63.625 TFZ=63.735 LNU=300 END START  
READ START NST=1 XSM=56.981 XSP=71.649 YSM=56.219 YSP=70.959  
  ZSM=56.401 ZSP=71.069 END START  
END DATA  
END
```

Table A.4. Table 4 input data

```

CAA03
=CSAS25
UO2(NO3)2 SOLN H/U-235=1379 BARE SPHERE CASE 3
27GROUPNDF4 MULTIREGION
U-234 1 0 5.400-7 END
U-235 1 0 4.815-5 END
U-236 1 0 1.390-7 END
U-238 1 0 2.811-6 END
H 1 0 6.640-2 END
O 1 0 3.379-2 END
N 1 0 1.753-4 END
AL 2 1 END
END COMP
SPHERICAL END
1 34.6 NOEXTERMOD 2 34.92 NOEXTERMOD END ZONE
UO2(NO3)2 SOLN H/U-235=1379 BARE SPHERE CASE 3
READ PARAM NPG=600 NUB=YES FDN=YES END PARAM
READ GEOM
SPHERE 1 1 34.6
SPHERE 2 1 34.92
END GEOM
END DATA
END

```

```

CAA04
=CSAS25
UO2F2 SOLN H/U-235=76.1 H2O REFL SPHERE CASE 4
27GROUPNDF4 MULTIREGION
U-234 1 0 8.795-6 END
U-235 1 0 8.327-4 END
U-236 1 0 4.449-6 END
U-238 1 0 4.729-5 END
H 1 0 6.337-2 END
O 1 0 3.347-2 END
F 1 0 1.786-3 END
AL 2 1 END
H2O 3 1 END
END COMP
SPHERICAL END
1 11.5 ONEXTERMOD 2 11.66 NOEXTERMOD 3 29.66 NOEXTERMOD END ZONE
UO2F2 SOLN H/U-235=76.1 H2O REFL SPHERE CASE 4
READ PARAM NPG=600 NUB=YES FDN=YES END PARAM
READ GEOM
SPHERE 1 1 11.5
SPHERE 2 1 11.66
REFLECTOR 3 2 3 6
END GEOM
READ BIAS ID=500 2 7 END BIAS
END DATA
END

```

```

CAA05
=CSAS25
UO2F2 SOLN H/U-235=126.5 H2O REFL SPHERE CASE 5
27GROUPNDF4 MULTIREGION
U-234 1 0 5.405-6 END
U-235 1 0 5.117-4 END
U-236 1 0 2.734-6 END
U-238 1 0 2.906-5 END
H 1 0 6.473-2 END
O 1 0 3.346-2 END
F 1 0 1.098-3 END
AL 2 1 END
H2O 3 1 END
END COMP
SPHERICAL END
1 11.8 ONEXTERMOD 2 11.96 NOEXTERMOD 3 29.96 NOEXTERMOD END ZONE
UO2F2 SOLN H/U-235=126.5 H2O REFL SPHERE CASE 5
READ PARAM NPG=600 NUB=YES FDN=YES END PARAM
READ GEOM
SPHERE 1 1 11.8
SPHERE 2 1 11.96
REFLECTOR 3 2 3 6
END GEOM
READ BIAS ID=500 2 7 END BIAS
END DATA
END

```

```

CAA06
=CSAS25
UO2F2 SOLN H/U-235=1270 H2O REFL SPHERE CASE 6
27GROUPNDF4 MULTIREGION
U-234 1 0 5.530-7 END
U-235 1 0 5.231-5 END
U-236 1 0 2.800-7 END
U-238 1 0 2.971-6 END
H 1 0 6.643-2 END
O 1 0 3.333-2 END
F 1 0 1.122-4 END
AL 2 1 END
H2O 3 1 END
END COMP
SPHERICAL END
1 27.9 ONEXTERMOD 2 28.10 NOEXTERMOD 3 46.10 NOEXTERMOD END ZONE
UO2F2 SOLN H/U-235=1270 H2O REFL SPHERE CASE 6
READ PARAM NPG=600 NUB=YES FDN=YES END PARAM
READ GEOM
SPHERE 1 1 27.9
SPHERE 2 1 28.1
REFLECTOR 3 2 3 6
END GEOM
READ BIAS ID=500 2 7 END BIAS
END DATA
END

```

Table A.4 (continued)

```

CAA07
=CSAS25
UO2F2 SOLN H/U-235=268.8 H2O REFL SPHERE CASE 7
27GROUPNDF4 MULTIREGION
U-235 1 0 2.438-4 300 END
U-238 1 0 1.756-5 300 END
H 1 0 6.553-2 300 END
O 1 0 3.329-2 300 END
F 1 0 5.227-4 300 END
AL 2 1 300 END
H2O 3 1 300 END
END COMP
SPHERICAL END
1 13.2 ONEXTERMOD 2 13.33 NOEXTERMOD 3 31.33 NOEXTERMOD END ZONE
UO2F2 SOLN H/U-235=268.8 H2O REFL SPHERE CASE 7
READ PARAM NPG=600 NUB=YES FDN=YES END PARAM
READ GEOM
SPHERE 1 1 13.2
SPHERE 2 1 13.33
REFLECTOR 3 2 3 6
END GEOM
READ BIAS ID=500 2 7 END BIAS
END DATA
END

CAA08
=CSAS25
UO2F2 SOLN H/U-235=515.1 H2O REFL SPHERE CASE 8
27GROUPNDF4 MULTIREGION
U-235 1 0 1.289-4 300 END
U-238 1 0 9.282-6 300 END
H 1 0 6.640-2 300 END
O 1 0 3.348-2 300 END
F 1 0 2.764-4 300 END
AL 2 1 300 END
H2O 3 1 300 END
END COMP
SPHERICAL END
1 16.0 ONEXTERMOD 2 16.13 NOEXTERMOD 3 34.13 NOEXTERMOD END ZONE
UO2F2 SOLN H/U-235=515.1 H2O REFL SPHERE CASE 8
READ PARAM NPG=600 NUB=YES FDN=YES END PARAM
READ GEOM
SPHERE 1 1 16.0
SPHERE 2 1 16.13
REFLECTOR 3 2 3 6
END GEOM
READ BIAS ID=500 2 7 END BIAS
END DATA
END

CAA09
=CSAS25
UO2F2 SOLN H/U-235=203.5 BARE SPHERE CASE 9
27GROUPNDF4 MULTIREGION
U-235 1 0 3.207-4 297 END
U-238 1 0 2.311-5 297 END
H 1 0 6.526-2 297 END
O 1 0 3.332-2 297 END
F 1 0 6.876-4 297 END
AL 2 1 297 END
END COMP

```

```

SPHERICAL END
1 16.0 NOEXTERMOD 2 16.13 NOEXTERMOD END ZONE
UO2F2 SOLN H/U-235=203.5 BARE SPHERE CASE 9
READ PARAM NPG=600 NUB=YES FDN=YES END PARAM
READ GEOM
SPHERE 1 1 16.0
SPHERE 2 1 16.13
END GEOM
END DATA
END

```

```

CAA10
=CSAS25
UO2F2 SOLN H/U-235=239.3 H2O REFL SPHERE CASE 10
27GROUPNDF4 MULTIREGION
U-235 1 0 2.735-4 359 END
U-238 1 0 1.970-5 359 END
H 1 0 6.545-2 359 END
O 1 0 3.331-2 359 END
F 1 0 5.864-4 359 END
AL 2 1 359 END
H2O 3 1 359 END
END COMP
SPHERICAL END
1 13.2 ONEXTERMOD 2 13.33 NOEXTERMOD 3 31.33 NOEXTERMOD END ZONE
UO2F2 SOLN H/U-235=239.3 H2O REFL SPHERE CASE 10
READ PARAM NPG=600 NUB=YES FDN=YES END PARAM
READ GEOM
SPHERE 1 1 13.2
SPHERE 2 1 13.33
REFLECTOR 3 2 3 6
END GEOM
READ BIAS ID=500 2 7 END BIAS
END DATA
END

```

```

CAA11
=CSAS25
UO2F2 SOLN H/U-235=468.2 H2O REFL SPHERE CASE 11
27GROUPNDF4 MULTIREGION
U-235 1 0 1.416-4 361 END
U-238 1 0 1.020-5 361 END
H 1 0 6.630-2 361 END
O 1 0 3.345-2 361 END
F 1 0 3.036-4 361 END
AL 2 1 361 END
H2O 3 1 361 END
END COMP
SPHERICAL END
1 16.0 ONEXTERMOD 2 16.13 NOEXTERMOD 3 34.13 NOEXTERMOD END ZONE
UO2F2 SOLN H/U-235=468.2 H2O REFL SPHERE CASE 11
READ PARAM NPG=600 NUB=YES FDN=YES END PARAM
READ GEOM
SPHERE 1 1 16.0
SPHERE 2 1 16.13
REFLECTOR 3 2 3 6
END GEOM
READ BIAS ID=500 2 7 END BIAS
END DATA
END

```

Table A.4 (continued)

```

CAA12
=CSAS25
ROCKY FLATS UO2(NO3)2 SOLN 142.92 G U/L
27GROUPNDF4 MULTIREGION
SOLNUO2(NO3)2 1 142.92 0.283 1 293 92234 1.022 92235 93.172 92236 .434
92238 5.372 END
AL 2 1 END
END COMP
CYLINDRICAL END
1 14 NOEXTERMOD 2 14.3 NOEXTERMOD END ZONE
ROCKY FLATS UO2(NO3)2 SOLN 28.01 CM DIAM BARE 1
READ PARAM NPG=600 NUB=YES FDN=YES END PARAM
READ GEOM
CYLINDER 1 1 14.005 33.55 0
CYLINDER 2 1 14.325 33.55 -.32
END GEOM
END DATA
END

```

```

CAA13
=CSAS25
ROCKY FLATS UO2(NO3)2 SOLN 357.71 G U/L
27GROUPNDF4 MULTIREGION
SOLNUO2(NO3)2 1 357.71 0.549 1 293 92234 1.022 92235 93.172 92236 .434
92238 5.372 END
AL 2 1 END
END COMP
CYLINDRICAL END
1 14 NOEXTERMOD 2 14.3 NOEXTERMOD END ZONE
ROCKY FLATS UO2(NO3)2 SOLN 28.01 CM DIAM BARE 2
READ PARAM NPG=600 NUB=YES FDN=YES END PARAM
READ GEOM
CYLINDER 1 1 14.005 30.91 0
CYLINDER 2 1 14.325 30.91 -.32
END GEOM
END DATA
END

```

```

CAA14
=CSAS25
ROCKY FLATS UO2(NO3)2 SOLN 54.89 G U/L
27GROUPNDF4 MULTIREGION
SOLNUO2(NO3)2 1 54.89 0.105 1 293 92234 1.022 92235 93.172 92236 .434
92238 5.372 END
AL 2 1 END
END COMP
CYLINDRICAL END
1 16.5 NOEXTERMOD 2 16.8 NOEXTERMOD END ZONE
ROCKY FLATS UO2(NO3)2 SOLN 33.01 CM DIAM BARE 3
READ PARAM NPG=600 NUB=YES FDN=YES END PARAM
READ GEOM
CYLINDER 1 1 16.505 39.48 0
CYLINDER 2 1 16.825 39.48 -.32
END GEOM
END DATA
END

```

```

CAA15
=CSAS25
ROCKY FLATS UO2(NO3)2 SOLN 137.40 G U/L
27GROUPNDF4 MULTIREGION
SOLNUO2(NO3)2 1 137.4 .287 1 293 92234 1.022 92235 93.172 92236 .434
92238 5.372 END
AL 2 1 END
END COMP
CYLINDRICAL END
1 16.5 NOEXTERMOD 2 16.8 NOEXTERMOD END ZONE
ROCKY FLATS UO2(NO3)2 SOLN 33.01 CM DIAM BARE 4
READ PARAM NPG=600 NUB=YES FDN=YES END PARAM
READ GEOM
CYLINDER 1 1 16.505 23.96 0
CYLINDER 2 1 16.825 23.96 -.32
END GEOM
END DATA
END

```

```

CAA16
=CSAS25
ROCKY FLATS UO2(NO3)2 SOLN 357.71 G U/L
27GROUPNDF4 MULTIREGION
SOLNUO2(NO3)2 1 357.71 .549 1 293 92234 1.022 92235 93.172 92236 .434
92238 5.372 END
AL 2 1 END
END COMP
CYLINDRICAL END
1 16.5 NOEXTERMOD 2 16.8 NOEXTERMOD END ZONE
ROCKY FLATS UO2(NO3)2 SOLN 33.01 CM DIAM BARE 5
READ PARAM NPG=600 NUB=YES FDN=YES END PARAM
READ GEOM
CYLINDER 1 1 16.505 22.53 0
CYLINDER 2 1 16.825 22.53 -.32
END GEOM
END DATA
END

```

```

CAA17
=CSAS25
ROCKY FLATS UO2(NO3)2 SOLN 144.38 G U/L
27GROUPNDF4 MULTIREGION
SOLNUO2(NO3)2 1 144.38 .272 1 293 92234 1.022 92235 93.172 92236 .434
92238 5.372 END
AL 2 1 END
RFCONCRETE 3 1 END
END COMP
CYLINDRICAL END
1 14 NOEXTERMOD 2 14.3 NOEXTERMOD END ZONE
ROCKY FLATS UO2(NO3)2 SOLN 28.01 CM DIAM REFL 1 CONC REFL
READ PARAM NPG=600 NUB=YES FDN=YES END PARAM
READ GEOM
CYLINDER 1 1 14.005 31.37 0
CYLINDER 2 1 14.325 31.37 -.32
CUBOID 0 1 64.6 -57.2 57.4 -64.8 80.8 -41.1
REFLECTOR 3 2 4R5.14 2R0 5
REFLECTOR 0 1 4R0 2R0.9 1
REFLECTOR 3 2 4R0 2R5.14 5
END GEOM
READ BIAS ID=301 2 6 END BIAS
END DATA
END

```

Table A.4 (continued)

```

CAA18
=CSAS25
ROCKY FLATS UO2(NO3)2 SOLN 334.77 G U/L
27GROUPNDF4 MULTIREGION
SOLNUO2(NO3)2 1 334.77 .521 1 293 92234 1.022 92235 93.172 92236 .434
92238 5.372 END
AL 2 1 END
RFCONCRETE 3 1 END
END COMP
CYLINDRICAL END
1 14 NOEXTERMOD 2 14.3 NOEXTERMOD END ZONE
ROCKY FLATS UO2(NO3)2 SOLN 28.01 CM DIAM REFL 2 CONC REFL
READ PARAM NPG=600 NUB=YES FDN=YES END PARAM
READ GEOM
CYLINDER 1 1 14.005 28.60 0
CYLINDER 2 1 14.325 28.60 -.32
CUBOID 0 1 64.6 -57.2 57.4 -64.8 80.8 -41.1
REFLECTOR 3 2 4R5.14 2R0 5
REFLECTOR 0 1 4R0 2R0.9 1
REFLECTOR 3 2 4R0 2R5.14 5
END GEOM
READ BIAS ID=301 2 6 END BIAS
END DATA
END
    
```

```

CAA19
=CSAS25
ROCKY FLATS UO2(NO3)2 SOLN 144.38 G U/L
27GROUPNDF4 MULTIREGION
SOLNUO2(NO3)2 1 144.38 .272 1 293 92234 1.022 92235 93.172 92236 .434
92238 5.372 END
AL 2 1 END
RFCONCRETE 3 1 END
END COMP
CYLINDRICAL END
1 16.5 NOEXTERMOD 2 16.8 NOEXTERMOD END ZONE
ROCKY FLATS UO2(NO3)2 SOLN 33.01 CM DIAM REFL 3 CONC REFL
READ PARAM NPG=600 NUB=YES FDN=YES END PARAM
READ GEOM
CYLINDER 1 1 16.505 22.85 0
CYLINDER 2 1 16.825 22.85 -.32
CUBOID 0 1 64.6 -57.2 57.4 -64.8 80.8 -41.1
REFLECTOR 3 2 4R5.14 2R0 5
REFLECTOR 0 1 4R0 2R0.9 1
REFLECTOR 3 2 4R0 2R5.14 5
END GEOM
READ BIAS ID=301 2 6 END BIAS
END DATA
END
    
```

```

CAA20
=CSAS25
ROCKY FLATS UO2(NO3)2 SOLN 334.77 G U/L
27GROUPNDF4 MULTIREGION
SOLNUO2(NO3)2 1 334.77 .521 1 293 92234 1.022 92235 93.172 92236 .434
92238 5.372 END
AL 2 1 END
RFCONCRETE 3 1 END
END COMP
CYLINDRICAL END
1 16.5 NOEXTERMOD 2 16.8 NOEXTERMOD END ZONE
ROCKY FLATS UO2(NO3)2 SOLN 33.01 CM DIAM REFL 4 CONC REFL
READ PARAM NPG=600 NUB=YES FDN=YES END PARAM
READ GEOM
CYLINDER 1 1 16.505 21.50 0
CYLINDER 2 1 16.825 21.50 -.32
CUBOID 0 1 64.6 -57.2 57.4 -64.8 80.8 -41.1
REFLECTOR 3 2 4R5.14 2R0 5
REFLECTOR 0 1 4R0 2R0.9 1
REFLECTOR 3 2 4R0 2R5.14 5
END GEOM
READ BIAS ID=301 2 6 END BIAS
END DATA
END
    
```

```

CAA21
=CSAS25
ROCKY FLATS UO2(NO3)2 SOLN 144.38 G U/L
27GROUPNDF4 MULTIREGION
SOLNUO2(NO3)2 1 144.38 .272 1 293 92234 1.022 92235 93.172 92236 .434
92238 5.372 END
AL 2 1 END
RFCONCRETE 3 1 END
END COMP
CYLINDRICAL END
1 14 NOEXTERMOD 2 14.3 NOEXTERMOD END ZONE
ROCKY FLATS UO2(NO3)2 SOLN 28.01 CM DIAM REFL 5 CONC REFL
READ PARAM NPG=600 NUB=YES FDN=YES END PARAM
READ GEOM
CYLINDER 1 1 14.005 24.70 0
CYLINDER 2 1 14.325 24.70 -.32
CUBOID 0 1 104.0 -17.8 16.5 -105.7 121.58 -.32
REFLECTOR 3 2 4R5.14 2R0 5
REFLECTOR 0 1 4R0 2R0.9 1
REFLECTOR 3 2 4R0 2R5.14 5
END GEOM
READ BIAS ID=301 2 6 END BIAS
END DATA
END
    
```

Table A.4 (continued)

```

CAA22
=CSAS25
ROCKY FLATS UO2(NO3)2 SOLN 334.77 G U/L
27GROUPNDF4 MULTIREGION
SOLNUO2(NO3)2 1 334.77 .521 1 293 92234 1.022 92235 93.172 92236 .434
92238 5.372 END
AL 2 1 END
RFCONCRETE 3 1 END
END COMP
CYLINDRICAL END
1 16.5 NOEXTERMOD 2 16.8 NOEXTERMOD END ZONE
ROCKY FLATS UO2(NO3)2 SOLN 33.01 CM DIAM REFL 6 CONC REFL
READ PARAM NPG=600 NUB=YES PDN=YES END PARAM
READ GEOM
CYLINDER 1 1 16.505 16.78 0
CYLINDER 2 1 16.825 16.78 -.32
CUBOID 0 1 104.55 -17.25 16.825 -105.375 121.58 -.32
REFLECTOR 3 2 4R5.14 2R0 5
REFLECTOR 0 1 4R0 2R0 9 1
REFLECTOR 3 2 4R0 2R5.14 5
END GEOM
READ BIAS ID=301 2 6 END BIAS
END DATA
END

```

```

CAA23
=CSAS25
ROCKY FLATS UO2(NO3)2 SOLN 147.66 G U/L
27GROUPNDF4 MULTIREGION
SOLNUO2(NO3)2 1 147.66 .271 1 293 92234 1.022 92235 93.172 92236 .434
92238 5.372 END
AL 2 1 END
PLEXIGLASS 3 1 END
H 4 0 5.5169-2 END
C 4 0 3.3967-2 END
O 4 0 1.4231-2 END
P 4 0 3.8500-4 END
CL 4 0 3.5610-4 END
BR-79 4 0 3.184-4 END
BR-81 4 0 3.116-4 END
END COMP
CYLINDRICAL END
1 14 NOEXTERMOD 2 14.3 NOEXTERMOD END ZONE
ROCKY FLATS UO2(NO3)2 SOLN 28.01 CM DIAM REFL 7 PLEXIGLASS REFL
READ PARAM NPG=600 NUB=YES PDN=YES END PARAM
READ GEOM
CYLINDER 1 1 14.005 31.26 0
CYLINDER 2 1 14.325 31.26 -.32
CUBOID 0 1 61.2 -61.7 60.4 -62.5 81.1 -41.8
REFLECTOR 3 2 4R2.971 2R0 7
REFLECTOR 4 2 5R0 2.971 7
REFLECTOR 4 2 4R0 2.886 0 7
END GEOM
READ BIAS ID=500 2 8 END BIAS
END DATA
END

```

```

CAA24
=CSAS25
ROCKY FLATS UO2(NO3)2 SOLN 345.33 G U/L
27GROUPNDF4 MULTIREGION
SOLNUO2(NO3)2 1 345.33 .534 1 293 92234 1.022 92235 93.172 92236 .434
92238 5.372 END
AL 2 1 END
PLEXIGLASS 3 1 END
H 4 0 5.5169-2 END
C 4 0 3.3967-2 END
O 4 0 1.4231-2 END
P 4 0 3.8500-4 END
CL 4 0 3.5610-4 END
BR-79 4 0 3.184-4 END
BR-81 4 0 3.116-4 END
END COMP
CYLINDRICAL END
1 14 NOEXTERMOD 2 14.3 NOEXTERMOD END ZONE
ROCKY FLATS UO2(NO3)2 SOLN 28.01 CM DIAM REFL 8 PLEXIGLASS REFL
READ PARAM NPG=600 NUB=YES PDN=YES END PARAM
READ GEOM
CYLINDER 1 1 14.005 28.84 0
CYLINDER 2 1 14.325 28.84 -.32
CUBOID 0 1 61.2 -61.7 60.4 -62.5 81.1 -41.8
REFLECTOR 3 2 4R2.971 2R0 7
REFLECTOR 4 2 5R0 2.971 7
REFLECTOR 4 2 4R0 2.886 0 7
END GEOM
READ BIAS ID=500 2 8 END BIAS
END DATA
END

```

```

CAA25
=CSAS25
ROCKY FLATS UO2(NO3)2 SOLN 147.66 G U/L
27GROUPNDF4 MULTIREGION
SOLNUO2(NO3)2 1 147.66 .271 1 293 92234 1.022 92235 93.172 92236 .434
92238 5.372 END
AL 2 1 END
PLEXIGLASS 3 1 END
H 4 0 5.5169-2 END
C 4 0 3.3967-2 END
O 4 0 1.4231-2 END
P 4 0 3.8500-4 END
CL 4 0 3.5610-4 END
BR-79 4 0 3.184-4 END
BR-81 4 0 3.116-4 END
END COMP
CYLINDRICAL END
1 16.5 NOEXTERMOD 2 16.8 NOEXTERMOD END ZONE
ROCKY FLATS UO2(NO3)2 SOLN 33.01 CM DIAM REFL 9 PLEXIGLASS REFL
READ PARAM NPG=600 NUB=YES PDN=YES END PARAM
READ GEOM
CYLINDER 1 1 16.505 22.78 0
CYLINDER 2 1 16.825 22.78 -.32
CUBOID 0 1 61.2 -61.7 60.4 -62.5 81.1 -41.8
REFLECTOR 3 2 4R2.971 2R0 7
REFLECTOR 4 2 5R0 2.971 7
REFLECTOR 4 2 4R0 2.886 0 7
END GEOM
READ BIAS ID=500 2 8 END BIAS
END DATA
END

```

Table A.4 (continued)

CAA26
 =CSAS25
 ROCKY FLATS UO2(NO3)2 SOLN 345.33 G U/L
 27GROUPNDF4 MULTIREGION
 SOLNUO2(NO3)2 1 345.33 .534 1 293 92234 1.022 92235 93.172 92236 .434
 92238 5.372 END
 AL 2 1 END
 PLEXIGLASS 3 1 END
 H 4 0 5.5169-2 END
 C 4 0 3.3967-2 END
 O 4 0 1.4231-2 END
 P 4 0 3.8500-4 END
 CL 4 0 3.5610-4 END
 BR-79 4 0 3.184-4 END
 BR-81 4 0 3.116-4 END
 END COMP
 CYLINDRICAL END
 1 16.5 NOEXTERMOD 2 16.8 NOEXTERMOD END ZONE
 ROCKY FLATS UO2(NO3)2 SOLN 33.01 CM DIAM REFL 10 PLEXIGLASS REFL
 READ PARAM NPG=600 NUB=YES FDN=YES END PARAM
 READ GEOM
 CYLINDER 1 1 16.505 21.67 0
 CYLINDER 2 1 16.825 21.67 -.32
 CUBOID 0 1 61.2 -61.7 60.4 -62.5 81.1 -41.8
 REFLECTOR 3 2 4R2.971 2R0 7
 REFLECTOR 4 2 5R0 2.971 7
 REFLECTOR 4 2 4R0 2.886 0 7
 END GEOM
 READ BIAS ID=500 2 8 END BIAS
 END DATA
 END

CAA27
 =CSAS25
 ROCKY FLATS UO2(NO3)2 SOLN 147.66 G U/L
 27GROUPNDF4 MULTIREGION
 SOLNUO2(NO3)2 1 147.66 .271 1 293 92234 1.022 92235 93.172 92236 .434
 92238 5.372 END
 AL 2 1 END
 PLEXIGLASS 3 1 END
 H 4 0 5.5169-2 END
 C 4 0 3.3967-2 END
 O 4 0 1.4231-2 END
 P 4 0 3.8500-4 END
 CL 4 0 3.5610-4 END
 BR-79 4 0 3.184-4 END
 BR-81 4 0 3.116-4 END
 END COMP
 CYLINDRICAL END
 1 14 NOEXTERMOD 2 14.3 NOEXTERMOD END ZONE
 ROCKY FLATS UO2(NO3)2 SOLN 28.01 CM DIAM REFL 11 PLEXIGLASS REFL
 READ PARAM NPG=600 NUB=YES FDN=YES END PARAM
 READ GEOM
 CYLINDER 1 1 14.005 25.26 0
 CYLINDER 2 1 14.325 25.26 -.32
 CUBOID 0 1 104.95 -17.95 17.52 -105.38 122.58 -.32
 REFLECTOR 3 2 4R2.971 2R0 7
 REFLECTOR 4 2 5R0 2.971 7
 REFLECTOR 4 2 4R0 2.886 0 7
 END GEOM
 READ BIAS ID=500 2 8 END BIAS
 END DATA
 END

CAA28
 =CSAS25
 ROCKY FLATS UO2(NO3)2 SOLN 345.33 G U/L
 27GROUPNDF4 MULTIREGION
 SOLNUO2(NO3)2 1 345.33 .534 1 293 92234 1.022 92235 93.172 92236 .434
 92238 5.372 END
 AL 2 1 END
 PLEXIGLASS 3 1 END
 H 4 0 5.5169-2 END
 C 4 0 3.3967-2 END
 O 4 0 1.4231-2 END
 P 4 0 3.8500-4 END
 CL 4 0 3.5610-4 END
 BR-79 4 0 3.184-4 END
 BR-81 4 0 3.116-4 END
 END COMP
 CYLINDRICAL END
 1 16.5 NOEXTERMOD 2 16.8 NOEXTERMOD END ZONE
 ROCKY FLATS UO2(NO3)2 SOLN 33.01 CM DIAM REFL 12 PLEXIGLASS REFL
 READ PARAM NPG=600 NUB=YES FDN=YES END PARAM
 READ GEOM
 CYLINDER 1 1 16.505 17.2 0
 CYLINDER 2 1 16.825 17.2 -.32
 CUBOID 0 1 105.2 -17.7 17.3 -105.6 122.58 -.32
 REFLECTOR 3 2 4R2.971 2R0 7
 REFLECTOR 4 2 5R0 2.971 7
 REFLECTOR 4 2 4R0 2.886 0 7
 END GEOM
 READ BIAS ID=500 2 8 END BIAS
 END DATA
 END

CAA29
 =CSAS25
 ROCKY FLATS UO2(NO3)2 SOLN 67.28 G U/L
 27GROUPNDF4 MULTIREGION
 SOLNUO2(NO3)2 1 67.28 .128 1 293 92234 1.022 92235 93.172 92236 .434
 92238 5.372 END
 AL 2 1 END
 RFCONCRETE 3 1 END
 END COMP
 CYLINDRICAL END
 1 10.5 NOEXTERMOD 2 10.9 NOEXTERMOD END ZONE
 ROCKY FLATS UO2(NO3)2 SOLN 21.12 CM DIAM 4X4 ARRAY CONC REFL
 READ PARAM NPG=600 NUB=YES FDN=YES END PARAM
 READ GEOM
 CYLINDER 1 1 10.56 27.15 0
 CYLINDER 2 1 10.96 27.15 -.32
 CUBOID 0 1 4P15.24 121.58 -.32
 CORE 0 1 2R-60.96 -.32
 REFLECTOR 3 2 4R5.14 2R0 5
 REFLECTOR 0 1 4R0 2R1.25 1
 REFLECTOR 3 2 4R0 2R5.14 5
 END GEOM
 READ ARRAY NUX=4 NUY=4 NUZ=1 END ARRAY
 READ BIAS ID=301 2 6 END BIAS
 END DATA
 END

Table A.4 (continued)

```

CAA30
=CSAS25
ROCKY FLATS UO2(NO3)2 SOLN 364.11 G U/L
27GROUPNDF4 MULTIREGION
SOLNUO2(NO3)2 1 364.11 .584 1 293 92234 1.022 92235 93.172 92236 .434
92238 5.372 END
AL 2 1 END
RFCONCRETE 3 1 END
END COMP
CYLINDRICAL END
1 10.5 NOEXTERMOD 2 10.9 NOEXTERMOD END ZONE
ROCKY FLATS UO2(NO3)2 SOLN 21.12 CM DIAM 4X4 ARRAY CONC REFL C2
READ PARAM NPG=600 NUB=YES FDN=YES END PARAM
READ GEOM
CYLINDER 1 1 10.56 17.13 0
CYLINDER 2 1 10.96 17.13 -.32
CUBOID 0 1 4P15.24 121.58 -.32
CORE 0 1 2R-60.96 -.32
REFLECTOR 3 2 4R5.14 2R0 5
REFLECTOR 0 1 4R0 2R1.25 1
REFLECTOR 3 2 4R0 2R5.14 5
END GEOM
READ ARRAY NUX=4 NUY=4 NUZ=1 END ARRAY
READ BIAS ID=301 2 6 END BIAS
END DATA
END
    
```

```

CAA31
=CSAS25
ROCKY FLATS UO2(NO3)2 SOLN 83.49 G U/L
27GROUPNDF4 MULTIREGION
SOLNUO2(NO3)2 1 83.49 .151 1 293 92234 1.022 92235 93.172 92236 .434
92238 5.372 END
AL 2 1 END
RFCONCRETE 3 1 END
END COMP
CYLINDRICAL END
1 8 NOEXTERMOD 2 8.3 NOEXTERMOD END ZONE
ROCKY FLATS UO2(NO3)2 SOLN 16.12 CM DIAM 4X4 ARRAY CONC REFL C3
READ PARAM NPG=600 NUB=YES FDN=YES END PARAM
READ GEOM
CYLINDER 1 1 8.06 51.21 0
CYLINDER 2 1 8.38 51.21 -.32
CUBOID 0 1 4P15.24 121.58 -.32
CORE 0 1 2R-60.96 -.32
REFLECTOR 3 2 4R5.14 2R0 5
REFLECTOR 0 1 4R0 2R1.25 1
REFLECTOR 3 2 4R0 2R5.14 5
END GEOM
READ ARRAY NUX=4 NUY=4 NUZ=1 END ARRAY
READ BIAS ID=301 2 6 END BIAS
END DATA
END
    
```

```

CAA32
=CSAS25
ROCKY FLATS UO2(NO3)2 SOLN 359.55 G U/L
27GROUPNDF4 MULTIREGION
SOLNUO2(NO3)2 1 359.55 .578 1 293 92234 1.022 92235 93.172 92236 .434
92238 5.372 END
AL 2 1 END
RFCONCRETE 3 1 END
END COMP
CYLINDRICAL END
1 8 NOEXTERMOD 2 8.3 NOEXTERMOD END ZONE
ROCKY FLATS UO2(NO3)2 SOLN 16.12 CM DIAM 4X4 ARRAY CONC REFL C4
READ PARAM NPG=600 NUB=YES FDN=YES END PARAM
READ GEOM
CYLINDER 1 1 8.06 31.82 0
CYLINDER 2 1 8.38 31.82 -.32
CUBOID 0 1 4P15.24 121.58 -.32
CORE 0 1 2R-60.96 -.32
REFLECTOR 3 2 4R5.14 2R0 5
REFLECTOR 0 1 4R0 2R1.25 1
REFLECTOR 3 2 4R0 2R5.14 5
END GEOM
READ ARRAY NUX=4 NUY=4 NUZ=1 END ARRAY
READ BIAS ID=301 2 6 END BIAS
END DATA
END
    
```

```

CAA33
=CSAS25
ROCKY FLATS UO2(NO3)2 SOLN 76.09 G U/L
27GROUPNDF4 MULTIREGION
SOLNUO2(NO3)2 1 76.09 .137 1 293 92234 1.022 92235 93.172 92236 .434
92238 5.372 END
AL 2 1 END
RFCONCRETE 3 1 END
END COMP
CYLINDRICAL END
1 10.5 NOEXTERMOD 2 10.9 NOEXTERMOD END ZONE
ROCKY FLATS UO2(NO3)2 SOLN 21.12 CM DIAM 2X2 ARRAY CONC REFL C5
READ PARAM NPG=600 NUB=YES FDN=YES END PARAM
READ GEOM
UNIT 1
CYLINDER 1 1 10.56 62.34 0
CYLINDER 2 1 10.96 62.34 -.32
CUBOID 0 1 4P15.24 121.58 -.32
UNIT 2
CUBOID 0 1 4P15.24 121.58 -.32
CORE 0 1 2R-60.96 -.32
REFLECTOR 3 2 4R5.14 2R0 5
REFLECTOR 0 1 4R0 2R1.25 1
REFLECTOR 3 2 4R0 2R5.14 5
END GEOM
READ ARRAY NUX=4 NUY=4 NUZ=1
FILL 5R2 2R1 2R2 2R1 5R2 END FILL
END ARRAY
READ BIAS ID=301 2 6 END BIAS
END DATA
END
    
```

Table A.4 (continued)

```

CAA34
=CSAS25
ROCKY FLATS UO2(NO3)2 SOLN 364.11 G U/L
27GROUPNDF4 MULTIREGION
SOLNUO2(NO3)2 1 364.11 .584 1 293 92234 1.022 92235 93.172 92236 .434
92238 5.372 END
AL 2 1 END
RFCONCRETE 3 1 END
END COMP
CYLINDRICAL END
1 10.5 NOEXTERMOD 2 10.9 NOEXTERMOD END ZONE
ROCKY FLATS UO2(NO3)2 SOLN 21.12 CM DIAM 2X2 ARRAY CONC REFL C6
READ PARAM NPG=600 NUB=YES FDN=YES END PARAM
READ GEOM
UNIT 1
CYLINDER 1 1 10.56 31.11 0
CYLINDER 2 1 10.96 31.11 -.32
CUBOID 0 1 4P15.24 121.58 -.32
UNIT 2
CUBOID 0 1 4P15.24 121.58 -.32
CORE 0 1 2R-60.96 -.32
REFLECTOR 3 2 4R5.14 2R0 5
REFLECTOR 0 1 4R0 2R1.25 1
REFLECTOR 3 2 4R0 2R5.14 5
END GEOM
READ ARRAY NUX=4 NUY=4 NUZ=1
FILL 5R2 2R1 2R2 2R1 5R2 END FILL
END ARRAY
READ BIAS ID=301 2 6 END BIAS
END DATA
END

```

```

CAA35
=CSAS25
ROCKY FLATS UO2(NO3)2 SOLN 359.55 G U/L
27GROUPNDF4 MULTIREGION
SOLNUO2(NO3)2 1 359.55 .578 1 293 92234 1.022 92235 93.172 92236 .434
92238 5.372 END
AL 2 1 END
RFCONCRETE 3 1 END
END COMP
CYLINDRICAL END
1 8 NOEXTERMOD 2 8.3 NOEXTERMOD END ZONE
ROCKY FLATS UO2(NO3)2 SOLN 16.12 CM DIAM 2X2 ARRAY CONC REFL C7
READ PARAM NPG=600 NUB=YES FDN=YES END PARAM
READ GEOM
UNIT 1
CYLINDER 1 1 8.06 104.04 0
CYLINDER 2 1 8.38 104.04 -.32
CUBOID 0 1 4P15.24 121.58 -.32
UNIT 2
CUBOID 0 1 4P15.24 121.58 -.32
CORE 0 1 2R-60.96 -.32
REFLECTOR 3 2 4R5.14 2R0 5
REFLECTOR 0 1 4R0 2R1.25 1
REFLECTOR 3 2 4R0 2R5.14 5
END GEOM
READ ARRAY NUX=4 NUY=4 NUZ=1
FILL 8R2 2R1 2R2 2R1 2R2 END FILL
END ARRAY
READ BIAS ID=301 2 6 END BIAS
END DATA
END

```

```

CAA36
=CSAS25
ROCKY FLATS UO2(NO3)2 SOLN 359.55 G U/L
27GROUPNDF4 MULTIREGION
SOLNUO2(NO3)2 1 359.55 .578 1 293 92234 1.022 92235 93.172 92236 .434
92238 5.372 END
AL 2 1 END
RFCONCRETE 3 1 END
END COMP
CYLINDRICAL END
1 8 NOEXTERMOD 2 8.3 NOEXTERMOD END ZONE
ROCKY FLATS UO2(NO3)2 SOLN 16.12 CM DIAM 2X4 ARRAY CONC REFL C8
READ PARAM NPG=600 NUB=YES FDN=YES END PARAM
READ GEOM
UNIT 1
CYLINDER 1 1 8.06 51.45 0
CYLINDER 2 1 8.38 51.45 -.32
CUBOID 0 1 4P15.24 121.58 -.32
UNIT 2
CUBOID 0 1 4P15.24 121.58 -.32
CORE 0 1 2R-60.96 -.32
REFLECTOR 3 2 4R5.14 2R0 5
REFLECTOR 0 1 4R0 2R1.25 1
REFLECTOR 3 2 4R0 2R5.14 5
END GEOM
READ ARRAY NUX=4 NUY=4 NUZ=1
FILL 2R1 2R2 3Q4 END FILL
END ARRAY
READ BIAS ID=301 2 6 END BIAS
END DATA
END

```

```

CAA37
=CSAS25
ROCKY FLATS UO2(NO3)2 SOLN 60.32 G U/L
27GROUPNDF4 MULTIREGION
SOLNUO2(NO3)2 1 60.32 .113 1 293 92234 1.022 92235 93.172 92236 .434
92238 5.372 END
AL 2 1 END
PLEXIGLASS 3 1 END
H 4 0 5.5169-2 END
C 4 0 3.3967-2 END
O 4 0 1.4231-2 END
P 4 0 3.8500-4 END
CL 4 0 3.5610-4 END
BR-79 4 0 3.184-4 END
BR-81 4 0 3.116-4 END
END COMP
CYLINDRICAL END
1 10.5 NOEXTERMOD 2 10.9 NOEXTERMOD END ZONE
ROCKY FLATS UO2(NO3)2 SOLN 21.12 CM DIAM 4X4 ARRAY PLEXIGLASS REFL P1
READ PARAM NPG=600 NUB=YES FDN=YES END PARAM
READ GEOM
CYLINDER 1 1 10.56 31.76 0
CYLINDER 2 1 10.96 31.76 -.32
CUBOID 0 1 4P15.24 122.58 -.32
CORE 0 1 2R-60.96 -.32
REFLECTOR 0 1 4R.49 2R0 1
REFLECTOR 3 2 4R2.971 2R0 7
REFLECTOR 4 2 5R0 2.971 7
REFLECTOR 4 2 4R0 2.886 0 7
END GEOM
READ ARRAY NUX=4 NUY=4 NUZ=1
END ARRAY
READ BIAS ID=500 2 8 END BIAS
END DATA
END

```

Table A.4 (continued)

```

CAA38
=CSAS25
ROCKY FLATS UO2(NO3)2 SOLN 355.94 G U/L
27GROUPNDF4 MULTIREGION
SOLNUO2(NO3)2 1 355.94 .494 1 293 92234 1.022 92235 93.172 92236 .434
92238 5.372 END
AL 2 1 END
PLEXIGLASS 3 1 END
H 4 0 5.5169-2 END
C 4 0 3.3967-2 END
O 4 0 1.4231-2 END
P 4 0 3.8500-4 END
CL 4 0 3.5610-4 END
BR-79 4 0 3.184-4 END
BR-81 4 0 3.116-4 END
END COMP
CYLINDRICAL END
1 10.5 NOEXTERMOD 2 10.9 NOEXTERMOD END ZONE
ROCKY FLATS UO2(NO3)2 SOLN 21.12 CM DIAM 4X4 ARRAY PLEXIGLASS REFL P2
READ PARAM NPG=600 NUB=YES FDN=YES END PARAM
READ GEOM
CYLINDER 1 1 10.56 18.82 0
CYLINDER 2 1 10.96 18.82 -.32
CUBOID 0 1 4P15.24 122.58 -.32
CORE 0 1 2R-60.96 -.32
REFLECTOR 0 1 4R.49 2R0 1
REFLECTOR 3 2 4R2.971 2R0 7
REFLECTOR 4 2 5R0 2.971 7
REFLECTOR 4 2 4R0 2.886 0 7
END GEOM
READ ARRAY NUX=4 NUY=4 NUZ=1
END ARRAY
READ BIAS ID=500 2 8 END BIAS
END DATA
END

```

```

CAA39
=CSAS25
ROCKY FLATS UO2(NO3)2 SOLN 60.32 G U/L
27GROUPNDF4 MULTIREGION
SOLNUO2(NO3)2 1 60.32 .113 1 293 92234 1.022 92235 93.172 92236 .434
92238 5.372 END
AL 2 1 END
PLEXIGLASS 3 1 END
H 4 0 5.5169-2 END
C 4 0 3.3967-2 END
O 4 0 1.4231-2 END
P 4 0 3.8500-4 END
CL 4 0 3.5610-4 END
BR-79 4 0 3.184-4 END
BR-81 4 0 3.116-4 END
END COMP
CYLINDRICAL END
1 8 NOEXTERMOD 2 8.3 NOEXTERMOD END ZONE
ROCKY FLATS UO2(NO3)2 SOLN 16.12 CM DIAM 4X4 ARRAY PLEXIGLASS REFL P3
READ PARAM NPG=600 NUB=YES FDN=YES END PARAM
READ GEOM
CYLINDER 1 1 8.06 78.40 0
CYLINDER 2 1 8.38 78.40 -.32
CUBOID 0 1 4P15.24 122.58 -.32
CORE 0 1 2R-60.96 -.32

```

```

REFLECTOR 0 1 4R.49 2R0 1
REFLECTOR 3 2 4R2.971 2R0 7
REFLECTOR 4 2 5R0 2.971 7
REFLECTOR 4 2 4R0 2.886 0 7
END GEOM
READ ARRAY NUX=4 NUY=4 NUZ=1
END ARRAY
READ BIAS ID=500 2 8 END BIAS
END DATA
END

```

```

CAA40
=CSAS25
ROCKY FLATS UO2(NO3)2 SOLN 355.94 G U/L
27GROUPNDF4 MULTIREGION
SOLNUO2(NO3)2 1 355.94 .494 1 293 92234 1.022 92235 93.172 92236 .434
92238 5.372 END
AL 2 1 END
PLEXIGLASS 3 1 END
H 4 0 5.5169-2 END
C 4 0 3.3967-2 END
O 4 0 1.4231-2 END
P 4 0 3.8500-4 END
CL 4 0 3.5610-4 END
BR-79 4 0 3.184-4 END
BR-81 4 0 3.116-4 END
END COMP
CYLINDRICAL END
1 8 NOEXTERMOD 2 8.3 NOEXTERMOD END ZONE
ROCKY FLATS UO2(NO3)2 SOLN 16.12 CM DIAM 4X4 ARRAY PLEXIGLASS REFL P4
READ PARAM NPG=600 NUB=YES FDN=YES END PARAM
READ GEOM
CYLINDER 1 1 8.06 35.56 0
CYLINDER 2 1 8.38 35.56 -.32
CUBOID 0 1 4P15.24 122.58 -.32
CORE 0 1 2R-60.96 -.32
REFLECTOR 0 1 4R.49 2R0 1
REFLECTOR 3 2 4R2.971 2R0 7
REFLECTOR 4 2 5R0 2.971 7
REFLECTOR 4 2 4R0 2.886 0 7
END GEOM
READ ARRAY NUX=4 NUY=4 NUZ=1
END ARRAY
READ BIAS ID=500 2 8 END BIAS
END DATA
END

```

```

CAA41
=CSAS25
ROCKY FLATS UO2(NO3)2 SOLN 60.32 G U/L
27GROUPNDF4 MULTIREGION
SOLNUO2(NO3)2 1 60.32 .113 1 293 92234 1.022 92235 93.172 92236 .434
92238 5.372 END
AL 2 1 END
PLEXIGLASS 3 1 END
H 4 0 5.5169-2 END
C 4 0 3.3967-2 END
O 4 0 1.4231-2 END
P 4 0 3.8500-4 END
CL 4 0 3.5610-4 END
BR-79 4 0 3.184-4 END
BR-81 4 0 3.116-4 END

```

Table A.4 (continued)

```

END COMP
CYLINDRICAL END
1 10.5 NOEXTERMOD 2 10.9 NOEXTERMOD END ZONE
ROCKY FLATS UO2(NO3)2 SOLN 21.12 CM DIAM 2X2 ARRAY PLEXIGLASS REFL P5
READ PARAM NPG=600 NUB=YES FDN=YES END PARAM
READ GEOM
UNIT 1
CYLINDER 1 1 10.56 102.29 0
CYLINDER 2 1 10.96 102.29 -.32
CUBOID 0 1 4P15.24 122.58 -.32
UNIT 2
CUBOID 0 1 4P15.24 122.58 -.32
CORE 0 1 2R-60.96 -.32
REFLECTOR 0 1 4R.49 2R0 1
REFLECTOR 3 2 4R2.971 2R0 7
REFLECTOR 4 2 5R0 2.971 7
REFLECTOR 4 2 4R0 2.886 0 7
END GEOM
READ ARRAY NUX=4 NUY=4 NUZ=1
FILL 5R2 2R1 2R2 2R1 5R2 END FILL
END ARRAY
READ BIAS ID=500 2 8 END BIAS
END DATA
END

```

```

CAA42
=CSAS25
ROCKY FLATS UO2(NO3)2 SOLN 355.94 G U/L
27GROUPNDF4 MULTIREGION
SOLNUO2(NO3)2 1 355.94 .494 1 293 92234 1.022 92235 93.172 92236 .434
92238 5.372 END
AL 2 1 END
PLEXIGLASS 3 1 END
H 4 0 5.5169-2 END
C 4 0 3.3967-2 END
O 4 0 1.4231-2 END
P 4 0 3.8500-4 END
CL 4 0 3.5610-4 END
BR-79 4 0 3.184-4 END
BR-81 4 0 3.116-4 END
END COMP
CYLINDRICAL END
1 10.5 NOEXTERMOD 2 10.9 NOEXTERMOD END ZONE
ROCKY FLATS UO2(NO3)2 SOLN 21.12 CM DIAM 2X2 ARRAY PLEXIGLASS REFL P6
READ PARAM NPG=600 NUB=YES FDN=YES END PARAM
READ GEOM
UNIT 1
CYLINDER 1 1 10.56 33.20 0
CYLINDER 2 1 10.96 33.20 -.32
CUBOID 0 1 4P15.24 122.58 -.32
UNIT 2
CUBOID 0 1 4P15.24 122.58 -.32
CORE 0 1 2R-60.96 -.32
REFLECTOR 0 1 4R.49 2R0 1
REFLECTOR 3 2 4R2.971 2R0 7
REFLECTOR 4 2 5R0 2.971 7
REFLECTOR 4 2 4R0 2.886 0 7
END GEOM
READ ARRAY NUX=4 NUY=4 NUZ=1
FILL 5R2 2R1 2R2 2R1 5R2 END FILL
END ARRAY

```

```

READ BIAS ID=500 2 8 END BIAS
END DATA
END

CAA43
=CSAS25
ROCKY FLATS UO2(NO3)2 SOLN 355.94 G U/L
27GROUPNDF4 MULTIREGION
SOLNUO2(NO3)2 1 355.94 .494 1 293 92234 1.022 92235 93.172 92236 .434
92238 5.372 END
AL 2 1 END
PLEXIGLASS 3 1 END
H 4 0 5.5169-2 END
C 4 0 3.3967-2 END
O 4 0 1.4231-2 END
P 4 0 3.8500-4 END
CL 4 0 3.5610-4 END
BR-79 4 0 3.184-4 END
BR-81 4 0 3.116-4 END
END COMP
CYLINDRICAL END
1 8 NOEXTERMOD 2 8.3 NOEXTERMOD END ZONE
ROCKY FLATS UO2(NO3)2 SOLN 16.12 CM DIAM 3X2 ARRAY PLEXIGLASS REFL P7
READ PARAM NPG=600 NUB=YES FDN=YES END PARAM
READ GEOM
UNIT 1
CYLINDER 1 1 8.06 89.78 0
CYLINDER 2 1 8.38 89.78 -.32
CUBOID 0 1 4P15.24 122.58 -.32
UNIT 2
CUBOID 0 1 4P15.24 122.58 -.32
CORE 0 1 2R-60.96 -.32
REFLECTOR 0 1 4R.49 2R0 1
REFLECTOR 3 2 4R2.971 2R0 7
REFLECTOR 4 2 5R0 2.971 7
REFLECTOR 4 2 4R0 2.886 0 7
END GEOM
READ ARRAY NUX=4 NUY=4 NUZ=1
FILL 4R2 3R1 2 3R1 5R2 END FILL
END ARRAY
READ BIAS ID=500 2 8 END BIAS
END DATA
END

```

Table A.5. Table 5 input data

```
CAS01
=CSAS25
KENO-5 VALIDATION CASE A-1
27GROUPNDF4 MULTIREGION
URANIUM 1 .9837 293 92235 93.8 92238 6.2 END
END COMP
SPHERICAL END
1 8.73136 NOEXTERMOD END ZONE
KENO-5 VALIDATION CASE A-1
READ PARAM NPG=600 FDN=YES NUB=YES END PARAM
READ GEOM
SPHERE 1 1 8.73136
END GEOM
END DATA
END
```

```
CAS02
=CSAS25
KENO-5 VALIDATION CASE A-10
27GROUPNDF4 MULTIREGION
URANIUM 1 .9866 293 92235 97.67 92238 2.33 END
H2O 2 END
PLEXIGLASS 3 END
END COMP
SPHERICAL END
1 6.55 ONEEXTERMOD 2 12.7 NOEXTERMOD END ZONE
KENO-5 VALIDATION CASE A-10
READ PARAM TME=60 NPG=600 FDN=YES NUB=YES END PARAM
READ GEOM
BOX TYPE 1
SPHERE 1 1 6.5537
CUBOID 2 1 12.7 -12.7 12.7 -12.7 6.5537 -6.5537
BOX TYPE 2
CYLINDER 2 1 4.1275 1.27 -1.27
CYLINDER 3 1 12.7 1.27 -1.27
CUBOID 2 1 12.7 -12.7 12.7 -12.7 1.27 -1.27
CORE 0 1 -12.7 -12.7 -7.8237
CYLINDER 2 1 30.48 24.3337 -39.5737
END GEOM
READ ARRAY NUX=1 NUY=1 NUZ=2 LOOP
1 1 1 1 1 1 1 2 2 1
2 1 1 1 1 1 1 1 1
END ARRAY
END DATA
END
```

```
CAS03
=CSAS25
KENO-5 VALIDATION CASE A11
27GROUPNDF4 MULTIREGION
SOLNUO2(NO3)2 1 346.73 .542 1 293 92235 93.172 92238 6.828 END
SS304 2 END
END COMP
CYLINDRICAL END
1 13.96 ONEEXTERMOD 2 14.28 ONEEXTERMOD END ZONE
KENO-5 VALIDATION CASE A11
READ PARAM NPG=600 FDN=YES NUB=YES END PARAM
READ GEOM
CYLINDER 1 1 13.96 14.465 -14.465
CYLINDER 0 1 13.96 27.135 -14.465
CYLINDER 2 1 14.28 27.135 -15.105
END GEOM
END DATA
END
```

```
CAS04
=CSAS25
KENO-5 VALIDATION CASE A-2
27GROUPNDF4 MULTIREGION
ARMUMMO 17.08 2 1 0 1 92000 90 42000 10 1 1 293 92235 93.2 92238 6.8 END
END COMP
CYLINDRICAL END
1 7.62 NOEXTERMOD END ZONE
KENO-5 VALIDATION CASE A-2
READ PARAM NPG=600 FDN=YES NUB=YES END PARAM
READ GEOM
CYLINDER 0 1 2.54 9.87 -9.87
CYLINDER 1 1 10.16 9.87 -9.87
CUBE 0 1 10.16 -10.16
END GEOM
END DATA
END
```

```
CAS05
=CSAS25
KENO-5 VALIDATION CASE A-3
27GROUPNDF4 MULTIREGION
SOLNUO2F2 1 19.992 0 1 293 92235 93.2 92238 6.8 END
AL 2 END
END COMP
SPHERICAL END
1 34.6 ONEEXTERMOD 2 34.92 NOEXTERMOD END ZONE
KENO-5 VALIDATION CASE A-3
READ PARAM NPG=600 FDN=YES NUB=YES END PARAM
READ GEOM
SPHERE 1 1 34.6
SPHERE 2 1 34.92
CUBE 0 1 35.0 -35.0
END GEOM
END DATA
END
```

```
CAS06
=CSAS25
KENO-5 VALIDATION CASE A-4
27GROUPNDF4 MULTIREGION
SOLNUO2(NO3)2 1 20.15 .139 1 293 92235 93.18 92238 6.82 END
AL 2 END
END COMP
SPHERICAL END
1 34.6 ONEEXTERMOD 2 34.92 NOEXTERMOD END ZONE
KENO-5 VALIDATION CASE A-4
READ PARAM NPG=600 FDN=YES NUB=YES END PARAM
READ GEOM
SPHERE 1 1 34.6
SPHERE 2 1 34.92
CUBE 0 1 35.0 -35.0
END GEOM
END DATA
END
```

Table A.5 (continued)

```
CAS07
=CSAS25
KENO-5 VALIDATION CASE A-5
27GROUPNDF4 MULTIREGION
URANIUM 1 .9848 283 92235 93.5 92238 6.5 END
H2O 2 END
END COMP
SPHERICAL END
1 12.7 ONEEXTERMOD 2 31. NOEXTERMOD END ZONE
KENO-5 VALIDATION CASE A-5
READ PARAM TME=60 NPG=600 FDN=YES NUB=YES END PARAM
READ GEOM
HEMISPHERE 2 1 12.7
HEMISPHERE 1 1 15.24
CUBOID 2 1 31.00 -31.00 31.00 -31.00 31.00 -16.
END GEOM
END DATA
END
```

```
CAS08
=CSAS25
KENO-5 VALIDATION CASE A-6
27GROUPNDF4 MULTIREGION
C 1 .7522 END
URANIUM 2 .9848 293 92235 93.2 92238 6.8 END
END COMP
CYLINDRICAL END
1 8.89 NOEXTERMOD 2 13.97 TWOEXTERMOD 1 31.75 NOEXTERMOD END ZONE
KENO-5 VALIDATION CASE A-6
READ PARAM NPG=600 FDN=YES NUB=YES END PARAM
READ GEOM
CYLINDER 1 1 8.89 3.425 -3.425
CYLINDER 2 1 11.43 3.425 -3.425
CYLINDER 1 1 11.43 3.495 -3.425
CYLINDER 2 1 13.97 3.495 -3.425
CYLINDER 1 1 31.75 21.275 -21.205
CUBE 0 1 32.0 -32.0
END GEOM
END DATA
END
```

```
CAS09
=CSAS25
KENO-5 VALIDATION CASE A-7
27GROUPNDF4 MULTIREGION
URANIUM 1 .9848 293 92235 94 92238 6 END
URANIUM 2 END
END COMP
SLAB END
1 7.62 NOEXTERMOD 2 52.02 NOEXTERMOD END ZONE
KENO-5 VALIDATION CASE A-7
READ PARAM NPG=600 FDN=YES NUB=YES END PARAM
READ GEOM
CUBOID 1 1 3.81 -3.81 4.445 -4.445 7.62 -7.62
CUBOID 2 1 26.01 -26.01 26.645 -26.645 29.82 -29.82
CUBE 0 1 30.0 -30.0
END GEOM
END DATA
END
```

```
CAS10
=CSAS25
KENO-5 VALIDATION CASE A-8
27GROUPNDF4 MULTIREGION
ARBMOIL .88 3 0 0 0 6012 86.82 1001 13.16 16032 .02 1 END
URANIUM 2 .9528 293 92235 93.1 92238 6.9 END
ARBMPJEL .024 2 0 0 0 6012 85 1001 15 2 END
END COMP
SPHERICAL END
1 6.679 NOEXTERMOD 2 25.5 TWOEXTERMOD 1 40.5 NOEXTERMOD END ZONE
KENO-5 VALIDATION CASE A-8
READ PARAM TME=60 NPG=600 FDN=YES NUB=YES END PARAM
READ GEOM
HEMISPHERE 1 1 6.679
HEMISPHERE 2 1 10.5254
SPHERE 1 1 40.5254
CUBE 0 1 42.0 -42.0
END GEOM
END DATA
END
```

```
CAS11
=CSAS25
KENO-5 VALIDATION CASE A-9
27GROUPNDF4 MULTIREGION
ARBMOIL .88 3 0 0 0 6012 86.82 1001 13.16 16032 .02 1 END
URANIUM 2 .9528 293 92235 93.1 92238 6.9 END
ARBMPJEL .024 2 0 0 0 6012 85 1001 15 2 END
CARBONSTEEL 3 END
END COMP
SPHERICAL END
2 8.2 ONEEXTERMOD 1 40.5 NOEXTERMOD END ZONE
KENO-5 VALIDATION CASE A-9
READ PARAM
TME=60 NPG=600 FDN=YES NUB=YES END PARAM
READ GEOM
HEMISPHERE 3 1 6.012
HEMISPHERE 2 1 10.488
SPHERE 1 1 40.488
CUBE 0 1 41.0 -41.0
END GEOM
END DATA
END
```

```
CAS12
=CSAS25
KENO-5 VALIDATION CASE B-1
27GROUPNDF4 MULTIREGION
URANIUM 1 .9848 293 92235 93.2 92238 6.8 END
END COMP
CYLINDRICAL END
1 8.89 NOEXTERMOD END ZONE
KENO-5 VALIDATION CASE B-1
READ PARAM NPG=600 FDN=YES NUB=YES END PARAM
READ GEOM
CYLINDER 1 1 8.89 10.1092 0. ORIGIN -5.08 0.
CYLINDER 0 1 13.97 10.1092 0.
CYLINDER 1 1 19.05 10.1092 0.
END GEOM
END DATA
END
```

Table A.5 (continued)

```

CAS13
=CSAS25
KENO-5 VALIDATION CASE B-10
27GROUPNDF4 MULTIREGION
SOLNUO2(NO3)2 1 63.3 0 1 293 92235 92.6 92238 7.4 END
PLEXIGLASS 2 1 END
END COMP
CYLINDRICAL END
1 9.52 ONEEXTERMOD 2 10.16 NOEXTERMOD END ZONE
KENO-5 VALIDATION CASE B-10
READ PARAM NPG=600 FDN=YES NUB=YES END PARAM
READ GEOM
BOX TYPE 1
CYLINDER 1 1 9.52 8.7804 -8.7804
CYLINDER 0 1 9.52 8.9895 -8.7804
CYLINDER 2 1 10.16 9.6295 -9.4204
CUBOID 0 1 11.282 -11.282 11.282 -11.282 10.7179 -11.7179
END GEOM
READ ARRAY NUX=3 NUY=3 NUZ=3 END ARRAY
READ START NST=1 END START
END DATA
END

```

```

CAS14
=CSAS25
KENO-5 VALIDATION CASE B-11
27GROUPNDF4 MULTIREGION
SOLNUO2(NO3)2 1 505 0 1 293 92235 93.2 92238 6.8 END
PLEXIGLASS 2 1 END
SS304 3 END
END COMP
CYLINDRICAL END
1 6.8 NOEXTERMOD 2 7.08 NOEXTERMOD END ZONE
KENO-5 VALIDATION CASE B-11
READ PARAM NPG=600 FDN=YES NUB=YES END PARAM
READ GEOM
BOX TYPE 1
CYLINDER 1 1 6.8 1.76 -1.76
CYLINDER 3 1 7.08 1.76 -2.04
CUBOID 1 1 15.0875 -15.0875 15.0875 -15.0875 1.76 -2.04
BOX TYPE 2
CYLINDER 1 1 6.8 30.5 -30.5
CYLINDER 0 1 6.8 96.7 -30.5
CYLINDER 3 1 7.08 96.7 -30.5
CUBOID 0 1 15.0875 -15.0875 15.0875 -15.0875 125.7 -30.5
CORE 0 1 -60.35 -60.35 -80.0
REFLECTOR 3 1 5Z .635 1
CUBOID 2 1 70.55 -70.55 70.55 -70.55 90.2 -90.835
CUBE 0 1 95.0 -95.0
END GEOM
READ ARRAY NUX=4 NUY=4 NUZ=2 LOOP
1 1 4 1 1 4 1 1 1 1 2 1 4 1 1 4 1 2 2 1
END LOOP END ARRAY
END DATA
END

```

```

CAS15
=CSAS25
KENO-5 VALIDATION CASE B-12
27GROUPNDF4 MULTIREGION
URANIUM 1 .9829 293 92235 93.2 92238 6.8 END
C 2 .8296 END
POLYETHYLENE 3 1 END
END COMP
CYLINDRICAL END
1 5.747 ONEEXTERMOD 2 10.92 NOEXTERMOD END ZONE
KENO-5 VALIDATION CASE B-12
READ PARAM TME=60 NPG=600 FDN=YES NUB=YES END PARAM
READ GEOM
BOX TYPE 1
CYLINDER 1 1 5.747 3.9699 -4.1071
CYLINDER 0 1 5.777 4.1071 -4.1071
CUBOID 2 1 10.9195 -10.9195 10.9195 -10.9195 7.8755 -7.8755
CUBOID 0 1 15.047 -15.047 15.047 -15.047 12.0035 -12.0035
CORE 0 1 -30.094 -30.094 -24.007
CUBOID 3 1 45.344 -45.344 45.344 -45.344 39.247 -39.247
CUBE 0 1 46.0 -46.0
END GEOM
READ ARRAY NUX=2 NUY=2 NUZ=2 END ARRAY
END DATA
END

```

```

CAS16
=CSAS25
KENO-5 VALIDATION CASE B-13
27GROUPNDF4 MULTIREGION
SOLNUO2(NO3)2 1 415 0 1 293 92235 92.6 92238 7.4 END
PLEXIGLASS 2 1 END
END COMP
CYLINDRICAL END
1 9.52 ONEEXTERMOD 2 10.16 NOEXTERMOD END ZONE
KENO-5 VALIDATION CASE B-13
READ PARAM NPG=600 FDN=YES NUB=YES END PARAM
READ GEOM
CYLINDER 1 1 9.52 8.7804 -8.7804
CYLINDER 0 1 9.52 8.9896 -8.7804
CYLINDER 2 1 10.16 9.6296 -9.4204
CUBOID 0 1 15.495 -15.495 15.495 -15.495 14.9646 -14.7554
END GEOM
READ ARRAY NUX=4 NUY=4 NUZ=4 END ARRAY
END DATA
END

```

Table A.5 (continued)

```

CAS17
=CSAS25
KENO-5 VALIDATION CASE B-14
27GROUPNDF4 MULTIREGION
SOLNUO2(NO3)2 1 415 0 1 293 92235 92.6 92238 7.4 END
PLEXIGLASS 2 1 END
PARAFFIN 3 END
END COMP
CYLINDRICAL END
1 9.52 ONEEXTERMOD 2 10.16 NOEXTERMOD END ZONE
KENO-5 VALIDATION CASE B-14
READ PARAM TME=60 NPG=600 FDN=YES NUB=YES END PARAM
READ GEOM
CYLINDER 1 1 9.52 8.7804 -8.7804
CYLINDER 0 1 9.52 8.9896 -8.7804
CYLINDER 2 1 10.16 9.6296 -9.4204
CUBOID 0 1 18.425 -18.425 18.425 -18.425 17.8946 -17.6854
CORE 0 1 -55.275 -55.275 -53.37
CUBOID 3 1 70.515 -70.515 70.515 -70.515 68.61 -68.61
END GEOM
READ ARRAY NUX=3 NUY=3 NUZ=3 END ARRAY
END DATA
END

CAS18
=CSAS25
KENO-5 VALIDATION CASE B-15
27GROUPNDF4 MULTIREGION
SOLNUO2(NO3)2 1 415 0 1 293 92235 92.6 92238 7.4 END
PLEXIGLASS 2 1 END
END COMP
CYLINDRICAL END
1 9.52 ONEEXTERMOD 2 10.16 NOEXTERMOD END ZONE
KENO-5 VALIDATION CASE B-15
READ PARAM TME=60 NPG=600 FDN=YES NUB=YES END PARAM
READ GEOM
CYLINDER 1 1 9.52 8.7804 -8.7804
CYLINDER 0 1 9.52 8.9896 -8.7804
CYLINDER 2 1 10.16 9.6296 -9.4204
CUBOID 0 1 14.54 -14.54 14.54 -14.54 14.0096 -13.8004
CORE 0 1 -43.62 -43.62 -41.715
CUBOID 2 1 44.89 -44.89 44.89 -44.89 42.985 -42.985
END GEOM
READ ARRAY NUX=3 NUY=3 NUZ=3 END ARRAY
END DATA
END

```

```

CAS19
=CSAS25
KENO-5 VALIDATION CASE B-16
27GROUPNDF4 MULTIREGION
SOLNUO2(NO3)2 1 450.8 .72 1 293 92235 93.1 92238 6.9 END
SS304 2 END
END COMP
CYLINDRICAL END
1 8.128 NOEXTERMOD 2 8.4074 NOEXTERMOD END ZONE
KENO-5 VALIDATION CASE B-16
READ PARAM NPG=600 FDN=YES NUB=YES END PARAM
READ GEOM
BOX TYPE 1
XCYLINDER 1 1 8.128 68.3006 -68.3006
XCYLINDER 2 1 8.4074 68.58 -68.58
CUBOID 0 1 68.58 -68.58 9.2075 -9.2075 14.999 -110.32
BOX TYPE 2
YCYLINDER 1 1 8.128 68.3006 -68.3006
YCYLINDER 2 1 8.4074 68.58 -68.58
CUBOID 0 1 9.2075 -9.2075 68.58 -68.58 14.999 -110.32
BOX TYPE 3
XCYLINDER 1 1 8.128 68.3006 -68.3006
XCYLINDER 2 1 8.4074 68.58 -68.58
CUBOID 0 1 68.58 -68.58 9.2075 -9.2075 125.09 -14.999
BOX TYPE 4
YCYLINDER 1 1 8.128 68.3006 -68.3006
YCYLINDER 2 1 8.4074 68.58 -68.58
CUBOID 0 1 9.2075 -9.2075 68.58 -68.58 125.09 -14.999
BOX TYPE 5
CUBOID 1 1 8.89 -8.89 8.89 -8.89 14.999 -110.00
CUBOID 2 1 9.2075 -9.2075 9.2075 -9.2075 14.999 -110.32
BOX TYPE 6
CUBOID 1 1 8.89 -8.89 8.89 -8.89 125.09 -14.999
CUBOID 2 1 9.2075 -9.2075 9.2075 -9.2075 125.09 -14.999
BOX TYPE 7
CUBOID 0 1 68.58 -68.58 68.58 -68.58 14.999 -110.32
BOX TYPE 8
CUBOID 0 1 68.58 -68.58 68.58 -68.58 125.09 -14.999
END GEOM
READ ARRAY NUX=3 NUY=3 NUZ=2 LOOP
1 1 3 2 2 2 1 1 1 1 2 2 2 1 1 3 2 1 1 1 3 1 3 2 2 2 1 2 2 1
4 2 2 1 1 3 2 2 1 1 5 2 2 1 2 2 1 1 1 1 6 2 2 1 2 2 1 2 2 1
7 1 3 2 1 3 2 1 1 1 8 1 3 2 1 3 2 2 2 1
END LOOP END ARRAY
END DATA
END

```


Table A.5 (continued)

```

CAS20
=CSAS25
KENO-5 VALIDATION CASE B-17
27GROUPNDF4 MULTIREGION
SOLNUO2(NO3)2 1 355.96 .494 1 293 92235 93.172 92238 6.828 END
ARBMAL 2.737 9 0 0 1 12000 1 13027 97.35 14028 .6 22000 .03
24000 .17 25055 .07 26000 .47 29000 .25 14028 .06 2 END
PLEXIGLASS 3 1 END
END COMP
CYLINDRICAL END
1 10.56 NOEXTERMOD 2 10.96 NOEXTERMOD END ZONE
KENO-5 VALIDATION CASE B-17
READ PARAM TME=60 NPG=600 FDN=YES NUB=YES END PARAM
READ GEOM
CYLINDER 1 1 10.56 9.41 -9.41
CYLINDER 0 1 10.56 109.69 -9.41
CYLINDER 2 1 10.96 109.69 -9.73
CUBOID 0 1 15.24 -15.24 15.24 -15.24 113.17 -9.73
CORE 0 1 -60.96 -60.96 -61.45
REFLECTOR 0 1 4R0.49 2Z 1
CUBE 3 1 82.05 -82.05
END GEOM
READ ARRAY NUX=4 NUY=4 END ARRAY
END DATA
END
    
```

```

CAS21
=CSAS25
KENO-5 VALIDATION CASE B-18
27GROUPNDF4 MULTIREGION
SOLNUO2(NO3)2 1 364.11 .584 1 293 92235 93.172 92238 6.828 END
ARBMAL 2.737 9 0 0 1 12000 1 13027 97.35 14028 .6 22000 .03
24000 .17 25055 .07 26000 .47 29000 .25 14028 .06 2 END
ARBMCONC 2.321 13 0 0 1 1001 .75 6012 5.55 7014 .01 8016 49.29
11023 .42 12000 1.48 13027 2.06 14028 15.7 16032 .17 19039 .75 20040 22.95
22000 .05 26000 .82 3 END
END COMP
CYLINDRICAL END
1 10.56 NOEXTERMOD 2 10.96 NOEXTERMOD END ZONE
KENO-5 VALIDATION CASE B-18
READ PARAM TME=60 NPG=600 FDN=YES NUB=YES END PARAM
READ GEOM
BOX TYPE 1
CYLINDER 1 1 10.56 8.565 -8.565
CYLINDER 0 1 10.56 110.535 -8.565
CYLINDER 2 1 10.96 110.535 -8.885
CUBOID 0 1 15.25 -15.15 15.25 -15.25 115.515 -8.885
BOX TYPE 2
CYLINDER 1 1 10.56 8.565 -8.565
CYLINDER 0 1 10.56 110.535 -8.565
CYLINDER 2 1 10.96 110.535 -8.885
CUBOID 0 1 15.15 -15.25 15.25 -15.25 115.515 -8.885
BOX TYPE 3
CYLINDER 1 1 10.56 8.565 -8.565
CYLINDER 0 1 10.56 110.535 -8.565
CYLINDER 2 1 10.96 110.535 -8.885
CUBOID 0 1 15.25 -15.25 15.25 -15.25 115.515 -8.885
CORE 0 1 -60.9 -61.0 -62.2
REFLECTOR 0 1 2Z 2R.1 2Z 1
CUBOID 3 1 86.6 -86.6 86.8 -86.8 87.9 -87.9
END GEOM
    
```

```

READ ARRAY NUX=4 NUY=4 LOOP
1 1 1 1 1 4 1 1 1 1 2 4 4 1 1 4 1 1 1 1 3 2 3 1 1 4 1 1 1 1
END LOOP END ARRAY
END DATA
END
    
```

```

CAS22
=CSAS25
KENO-5 VALIDATION CASE B-2
27GROUPNDF4 MULTIREGION
URANIUM 1 .9848 293 92235 93.2 92238 6.8 END
END COMP
CYLINDRICAL END
1 8.89 NOEXTERMOD END ZONE
KENO-5 VALIDATION CASE B-2
READ PARAM NPG=600 FDN=YES NUB=YES END PARAM
READ GEOM
CUBOID 1 1 0.3434 -12.4434 6.35 -6.35 6.49 -6.49
CYLINDER 0 1 13.97 6.49 -6.49
CYLINDER 1 1 19.05 6.49 -6.49
CUBE 0 1 20.0 -20.0
END GEOM
END DATA
END
    
```

```

CAS23
=CSAS25
KENO-5 VALIDATION CASE B-3
27GROUPNDF4 MULTIREGION
URANIUM 1 .98231 293 92235 93.2 92238 6.8 END
END COMP
CYLINDRICAL END
1 4.55 NOEXTERMOD END ZONE
KENO-5 VALIDATION CASE B-3
READ PARAM PLT=NO NPG=600 FDN=YES NUB=YES END PARAM
READ GEOM
UNIT 1
CUBOID 1 1 2P6.3515 1.2685 -3.8115 13.377 13.058
CUBOID 0 1 2P6.3515 6.3515 -3.8115 13.377 13.058
CUBOID 1 1 2P6.3515 6.3515 -3.8115 13.377 11.155
CUBOID 0 1 4P6.3515 13.377 11.155
CUBOID 1 1 4P6.3515 13.377 0.
UNIT 2
CYLINDER 1 1 4.5555 12.918 0.
UNIT 3
CYLINDER 1 1 5.761 13.475 0.
UNIT 4
CYLINDER 1 1 4.5525 12.969 0.
UNIT 5
ARRAY 1 -4.573 -4.573 0.
UNIT 6
CYLINDER 1 1 4.5545 12.974 0.
UNIT 7
CYLINDER 1 1 5.7495 13.475 0.
UNIT 8
CYLINDER 1 1 4.5565 12.954 0.
UNIT 9
COM='CENTERPIECE'
ARRAY 2 -6.35 -6.35 0.
UNIT 10
COM='BOTTOM OF UNIT 5'
CUBOID 1 1 2P3.81 8.13 -4.573 8.91 0
CUBOID 0 1 2P4.573 8.13 -4.573 8.91 0.
    
```

Table A.5 (continued)

```

UNIT 11
COM='TOP OF UNIT 5'
CYLINDER 1 1 4.573 4.319 0.
CUBOID 0 1 2P4.573 8.13 -4.573 4.319 0.
UNIT 12
COM='BOTTOM OF CENTERPIECE'
CYLINDER 1 1 5.757 2.690 0. ORIGIN -.593 -.593
CUBOID 0 1 4P6.35 2.690 0.
UNIT 13
COM='MIDDLE OF CENTERPIECE'
CUBOID 1 1 4P6.35 5.718 0.
UNIT 14
COM='TOP OF CENTERPIECE'
HEMISPHERE 1 1 6.082 ORIGIN -.268 .268 0.
CUBOID 0 1 4P6.35 6.082 0.
GLOBAL
UNIT 15
CUBOID 0 1 4P25.0 15.0 -2.0
HOLE 1 0.0 -17.306 0.15
HOLE 2 -12.051 -9.247 0.111
HOLE 3 -16.196 1.845 0.174
HOLE 4 -9.394 10.999 0.156
HOLE 5 0.0 15.400 0.29
HOLE 6 9.727 10.803 0.134
HOLE 7 16.224 1.419 0.140
HOLE 8 11.931 -9.322 0.087
HOLE 9 0.0 0.0 -1.755
END GEOM
READ ARRAY
ARA=1 NUX=1 NUY=1 NUZ=2 FILL 10 11 END FILL
ARA=2 NUX=1 NUY=1 NUZ=3 FILL 12 13 14 END FILL
END ARRAY
READ PLOT TTL='GROTESQUE' PIC=MIX
XUL=-25 YUL=25 ZUL=0.5 XLR=25 YLR=-25 ZLR=.5
UAX=1 VDN=-1 NAX=130 END
XUL=-25 YUL=25 ZUL=2 XLR=25 YLR=-25 ZLR=2 END
XUL=-25 YUL=25 ZUL=9.5 XLR=25 YLR=-25 ZLR=9.5 END
XUL=-.593 YUL=-25 ZUL=15 XLR=-.593 YLR=25 ZLR=-2
UAX=0 VAX=1 VDN=0 WDN=-1 NAX=130 END
END PLOT
END DATA
END

```

```

CAS24
=CSAS25
KENO-5 VALIDATION CASE B-4
27GROUPNDF4 MULTIREGION
URANIUM 1 .9848 293 92235 93.2 92238 6.8 END
SS304 2 END
INCONEL 3 END
END COMP
CYLINDRICAL END
2 .254 NOEXTERMOD 1 5.74 NOEXTERMOD END ZONE
KENO-5 VALIDATION CASE B-4
READ PARAM NPG=600 PDN=YES NUB=YES PLT=NO END PARAM
READ GEOM
UNIT 1
COM='SS RODS IN FUEL'
CYLINDER 2 1 .254 2P2.691
UNIT 2
COM='SS ROD & INCONEL SLEEVE'
CYLINDER 2 1 .254 2P.987
CYLINDER 3 1 .381 2P.987
UNIT 3
COM='A6 CYLINDER & SUPPORT RODS'
CYLINDER 1 1 5.7405 2P2.691
HOLE 1 -4.2735 2R0
HOLE 1 4.2735 2R0
CUBOID 0 1 4P7.7165 2P4.667
HOLE 2 -4.2735 0 -3.679
HOLE 2 -4.2735 0 3.679
HOLE 2 4.2735 0 -3.679
HOLE 2 4.2735 0 3.679
END GEOM
READ ARRAY
NUX=4 NUY=4 NUZ=4 FILL P3 END FILL
END ARRAY
READ PLOT TTL='A6 UNIT WITH SUPPORTS' PLT=NO
XUL=0 YUL=7.7165 ZUL=9.334 XLR=15.433 YLR=7.7165 ZLR=0
UAX=1 WDN=-1 NAX=125 END PLOT
END DATA
END

CAS25
=CSAS25
KENO-5 VALIDATION CASE B-5
27GROUPNDF4 MULTIREGION
URANIUM 1 .9809 293 92235 93.2 92238 6.8 END
END COMP
CYLINDRICAL END
1 4.56 NOEXTERMOD END ZONE
KENO-5 VALIDATION CASE B-5
READ PARAM NPG=600 PDN=YES NUB=YES END PARAM
READ GEOM
BOX TYPE 1
CYLINDER 1 1 4.558 2.16 -2.16
CYLINDER 0 1 5.747 2.16 -2.16
CYLINDER 1 1 5.747 4.851 -4.851
CUBOID 0 1 5.8554 -5.8554 5.8554 -5.8554 4.9771 -4.9771
END GEOM
READ ARRAY NUX=2 NUY=2 NUZ=2 END ARRAY
END DATA
END

```

Table A.5 (continued)

```

CAS26
=CSAS25
KENO-5 VALIDATION CASE B-6
27GROUPNDF4 MULTIREGION
URANIUM 1 .9809 293 92235 93.2 92238 6.8 END
PARAFFIN 2 END
END COMP
CYLINDRICAL END
1 4.56 NOEXTERMOD END ZONE
KENO-5 VALIDATION CASE B-6
READ PARAM TME=60 NPG=600 FDN=YES NUB=YES END PARAM
READ GEOM
BOX TYPE 1
CYLINDER 1 1 4.558 8.641 -8.641
CUBOID 0 1 9.7212 -9.7212 9.7212 -9.7212 13.8041 -13.8041
CORE 0 1 -19.4424 -19.4424 -27.6082
REFLECTOR 2 1 6R15.2 1
END GEOM
READ ARRAY NUX=2 NUY=2 NUZ=2 END ARRAY
END DATA
END
    
```

```

CAS27
=CSAS25
KENO-5 VALIDATION CASE B-7
27GROUPNDF4 MULTIREGION
URANIUM 1 .9848 293 92235 93.2 92238 6.8 END
PARAFFIN 2 END
END COMP
CYLINDRICAL END
1 4.558 NOEXTERMOD END ZONE
KENO-5 VALIDATION CASE B-7
READ PARAM TME=60 NPG=600 FDN=YES NUB=YES END PARAM
READ GEOM
BOX TYPE 1
CYLINDER 1 1 4.558 2.160 -2.160
CYLINDER 0 1 5.747 2.160 -2.160
CYLINDER 1 1 5.747 4.851 -4.851
CUBOID 0 1 9.2083 -9.2083 9.2083 -9.2083 8.2875 -8.2875
CORE 0 1 -18.4166 -18.4166 -16.575
REFLECTOR 2 1 6R15.2 1
END GEOM
READ ARRAY NUX=2 NUY=2 NUZ=2 END ARRAY
END DATA
END
    
```

```

CAS28
=CSAS25
KENO-5 VALIDATION CASE B-8
27GROUPNDF4 MULTIREGION
URANIUM 1 .9848 293 92235 93.2 92238 6.8 END
PLEXIGLASS 2 1 END
END COMP
CYLINDRICAL END
1 5.753 NOEXTERMOD END ZONE
KENO-5 VALIDATION CASE B-8
READ PARAM NPG=600 FDN=YES NUB=YES END PARAM
READ GEOM
BOX TYPE 1
CYLINDER 1 1 5.753 5.3825 -5.3825
CUBOID 0 1 7.68 -7.68 7.68 -7.68 7.33 -7.33
CUBOID 2 1 8.95 -8.95 8.95 -8.95 8.6 -8.6
CUBOID 0 1 9.0599 -9.0599 9.0599 -9.0599 8.6975 -8.6975
END GEOM
READ ARRAY NUX=2 NUY=2 NUZ=2 END ARRAY
END DATA
END
    
```

```

CAS29
=CSAS25
KENO-5 VALIDATION CASE B-9
27GROUPNDF4 MULTIREGION
SOLNUO2(NO3)2 1 415 0 1 293 92235 92.6 92238 7.4 END
PLEXIGLASS 2 1 END
END COMP
CYLINDRICAL END
1 9.52 ONEEXTERMOD 2 10.16 NOEXTERMOD END ZONE
KENO-5 VALIDATION CASE B-9
READ PARAM NPG=600 FDN=YES NUB=YES END PARAM
READ GEOM
BOX TYPE 1
CYLINDER 1 1 9.52 8.7804 -8.7804
CYLINDER 0 1 9.52 8.9896 -8.7804
CYLINDER 2 1 10.16 9.6296 -9.4204
CUBOID 0 1 13.4 -13.4 13.4 -13.4 12.8696 -12.6604
END GEOM
READ ARRAY NUX=3 NUY=3 NUZ=3 END ARRAY
END DATA
END
    
```

Table A.5 (continued)

```

CAS30
=CSAS25
93.2% UO2F2 H/U-235=337
27GROUPNDF4 MULTIREGION
SOLNUO2F2 1 81.845 0 1 293 92235 93.2
92238 6.8 END
AL 2 1 END
CARBONSTEEL 3 1 END
PLEXIGLASS 4 1 END
ARBMWOOD .640525 3 0 0 0 6012 44.435 1001 6.2639 8016 49.301 5 END
REG-CONCRETE 6 END
END COMP
SLAB END
1 3.81 NOEXTERMOD 2 4.12 NOEXTERMOD END ZONE
93.2% UO2F2 3 IN AL SLAB 3X1X1 ARRAY 0 IN SEP ROOM
READ PARAM NPG=600 FDN=YES NUB=YES END PARAM
READ GEOM
CUBOID 1 1 2P3.81 2P60.325 25.50 0
REFLECTOR 2 1 4R.318 0 .318 1
CUBOID 0 1 2P4.128 2P65. 150. -1.
CORE 0 1 -12.384 -65. -1.
CYLINDER 0 1 142.8 212. -60.
CYLINDER 3 1 144.8 212. -62.
CUBOID 0 1 275.5 -638.9 475. -744.2 588. -62.
REFLECTOR 4 1 5R0 .32 1
REFLECTOR 5 1 5R0 1.27 1
REFLECTOR 3 1 5R0 .64 1
REFLECTOR 0 1 5R0 365 1
REFLECTOR 6 2 6R3 10
REFLECTOR 6 12 0 3 4R0 10
END GEOM
READ BIAS ID=301 2 21 END BIAS
READ ARRAY NUX=3 NUY=1 NUZ=1 END ARRAY
END DATA
END
    
```

```

CAS31
=CSAS25
93.2% UO2F2 H/U-235=337
27GROUPNDF4 MULTIREGION
SOLNUO2F2 1 81.845 0 1 293 92235 93.2
92238 6.8 END
AL 2 1 END
H2O 3 1 END
END COMP
SLAB END
1 3.81 ONEXTERMOD 2 4.12 NOEXTERMOD 3 22.12 NOEXTERMOD END ZONE
93.2% UO2F2 3 IN AL SLAB 3X1X1 ARRAY 0 IN SEP H2O REFL
READ PARAM NPG=600 FDN=YES NUB=YES END PARAM
READ GEOM
CUBOID 1 1 2P3.81 2P60.325 17.32 0
REFLECTOR 2 1 4R.318 0 .318 1
CUBOID 0 1 2P4.128 2P60.643 17.32 -.318
CORE 0 1 3R0
REFLECTOR 3 2 4R3 0 3 6
END GEOM
READ ARRAY NUX=3 NUY=1 NUZ=1 END ARRAY
READ BIAS ID=500 2 7 END BIAS
END DATA
END
    
```

```

CAS32
=CSAS25
93.2% UO2F2 H/U-235=337
27GROUPNDF4 MULTIREGION
SOLNUO2F2 1 81.845 0 1 293 92235 93.2
92238 6.8 END
AL 2 1 END
CARBONSTEEL 3 1 END
PLEXIGLASS 4 1 END
ARBMWOOD .640525 3 0 0 0 6012 44.435 1001 6.2639 8016 49.301 5 END
REG-CONCRETE 6 END
END COMP
SLAB END
1 3.81 NOEXTERMOD 2 4.12 NOEXTERMOD END ZONE
93.2% UO2F2 3 IN AL SLAB 3X1X1 ARRAY 1 IN SEP ROOM
READ PARAM NPG=600 FDN=YES NUB=YES END PARAM
READ GEOM
CUBOID 1 1 2P3.81 2P60.325 34.44 0
REFLECTOR 2 1 4R.318 0 .318 1
CUBOID 0 1 2P5.398 2P65. 150. -1.
CORE 0 1 -16.194 -65. -1.
CYLINDER 0 1 142.8 212. -60.
CYLINDER 3 1 144.8 212. -62.
CUBOID 0 1 275.5 -638.9 475. -744.2 588. -62.
REFLECTOR 4 1 5R0 .32 1
REFLECTOR 5 1 5R0 1.27 1
REFLECTOR 3 1 5R0 .64 1
REFLECTOR 0 1 5R0 365 1
REFLECTOR 6 2 6R3 10
REFLECTOR 6 12 0 3 4R0 10
END GEOM
READ BIAS ID=301 2 21 END BIAS
READ ARRAY NUX=3 NUY=1 NUZ=1 END ARRAY
END DATA
END
    
```

```

CAS33
=CSAS25
93.2% UO2F2 H/U-235=337
27GROUPNDF4 MULTIREGION
SOLNUO2F2 1 81.845 0 1 293 92235 93.2
92238 6.8 END
AL 2 1 END
H2O 3 1 END
END COMP
SLAB END
1 3.81 ONEXTERMOD 2 4.12 NOEXTERMOD 3 22.12 NOEXTERMOD END ZONE
93.2% UO2F2 3 IN AL SLAB 3X1X1 ARRAY 1 IN SEP H2O REFL
READ PARAM NPG=600 FDN=YES NUB=YES END PARAM
READ GEOM
UNIT 1
CUBOID 1 1 2P3.81 2P60.325 19.13 0
REFLECTOR 2 1 4R.318 0 .318 1
CUBOID 0 1 2P4.128 2P60.643 19.13 -.318
UNIT 2
CUBOID 3 1 2.54 0 2P60.643 19.13 -.318
CORE 0 1 3R0
REFLECTOR 3 2 4R3 0 3 6
END GEOM
READ ARRAY NUX=5 NUY=1 NUZ=1 FILL 1 2 1 2 1 END FILL END ARRAY
READ BIAS ID=500 2 7 END BIAS
END DATA
END
    
```

Table A.5 (continued)

```

CAS34
=CSAS25
93.2% UO2F2 H/U-235=337
27GROUPNDF4 MULTIREGION
SOLNUO2F2 1 81.845 0 1 293 92235 93.2
92238 6.8 END
AL 2 1 END
CARBONSTEEL 3 1 END
PLEXIGLASS 4 1 END
ARBMWOOD .640525 3 0 0 0 6012 44.435 1001 6.2639 8016 49.301 5 END
REG-CONCRETE 6 END
END COMP
SLAB END
1 3.81 NOEXTERMOD 2 4.12 NOEXTERMOD END ZONE
93.2% UO2F2 3 IN AL SLAB 3X1X1 ARRAY 3 IN SEP ROOM
READ PARAM NPG=600 PDN=YES NUB=YES END PARAM
READ GEOM
CUBOID 1 1 2P3.81 2P60.325 58.78 0
REFLECTOR 2 1 4R.318 0 .318 1
CUBOID 0 1 2P7.938 2P65. 150. -1.
CORE 0 1 -23.814 -65. -1.
CYLINDER 0 1 142.8 212. -60.
CYLINDER 3 1 144.8 212. -62.
CUBOID 0 1 275.5 -638.9 475. -744.2 588. -62.
REFLECTOR 4 1 5R0 .32 1
REFLECTOR 5 1 5R0 1.27 1
REFLECTOR 3 1 5R0 .64 1
REFLECTOR 0 1 5R0 365 1
REFLECTOR 6 2 6R3 10
REFLECTOR 6 12 0 3 4R0 10
END GEOM
READ BIAS ID=301 2 21 END BIAS
READ ARRAY NUX=3 NUY=1 NUZ=1 END ARRAY
END DATA
END
    
```

```

CAS35
=CSAS25
93.2% UO2F2 H/U-235=337
27GROUPNDF4 MULTIREGION
SOLNUO2F2 1 81.845 0 1 293 92235 93.2
92238 6.8 END
AL 2 1 END
H2O 3 1 END
END COMP
SLAB END
1 3.81 ONEXTERMOD 2 4.12 NOEXTERMOD 3 22.12 NOEXTERMOD END ZONE
93.2% UO2F2 3 IN AL SLAB 3X1X1 ARRAY 3 IN SEP H2O REFL
READ PARAM NPG=600 PDN=YES NUB=YES END PARAM
READ GEOM
UNIT 1
CUBOID 1 1 2P3.81 2P60.325 32.92 0
REFLECTOR 2 1 4R.318 0 .318 1
CUBOID 0 1 2P4.128 2P60.643 32.92 -.318
UNIT 2
CUBOID 3 1 7.62 0 2P60.643 32.92 -.318
CORE 0 1 3R0
REFLECTOR 3 2 4R3 0 3 6
END GEOM
READ ARRAY NUX=5 NUY=1 NUZ=1 FILL 1 2 1 2 1 END FILL END ARRAY
READ BIAS ID=500 2 7 END BIAS
END DATA
END
    
```

```

CAS36
=CSAS25
93.2% UO2F2 H/U-235=337
27GROUPNDF4 MULTIREGION
SOLNUO2F2 1 81.845 0 1 293 92235 93.2
92238 6.8 END
AL 2 1 END
CARBONSTEEL 3 1 END
PLEXIGLASS 4 1 END
ARBMWOOD .640525 3 0 0 0 6012 44.435 1001 6.2639 8016 49.301 5 END
REG-CONCRETE 6 END
END COMP
SLAB END
1 3.81 NOEXTERMOD 2 4.12 NOEXTERMOD END ZONE
93.2% UO2F2 3 IN AL SLAB 3X1X1 ARRAY 4.5 IN SEP ROOM
READ PARAM NPG=600 PDN=YES NUB=YES END PARAM
READ GEOM
CUBOID 1 1 2P3.81 2P60.325 85.52 0
REFLECTOR 2 1 4R.318 0 .318 1
CUBOID 0 1 2P9.843 2P65. 150. -1.
CORE 0 1 -29.529 -65. -1.
CYLINDER 0 1 142.8 212. -60.
CYLINDER 3 1 144.8 212. -62.
CUBOID 0 1 275.5 -638.9 475. -744.2 588. -62.
REFLECTOR 4 1 5R0 .32 1
REFLECTOR 5 1 5R0 1.27 1
REFLECTOR 3 1 5R0 .64 1
REFLECTOR 0 1 5R0 365 1
REFLECTOR 6 2 6R3 10
REFLECTOR 6 12 0 3 4R0 10
END GEOM
READ BIAS ID=301 2 21 END BIAS
READ ARRAY NUX=3 NUY=1 NUZ=1 END ARRAY
END DATA
END
    
```

```

CAS37
=CSAS25
93.2% UO2F2 H/U-235=337
27GROUPNDF4 MULTIREGION
SOLNUO2F2 1 81.845 0 1 293 92235 93.2
92238 6.8 END
AL 2 1 END
H2O 3 1 END
END COMP
SLAB END
1 3.81 ONEXTERMOD 2 4.12 NOEXTERMOD 3 22.12 NOEXTERMOD END ZONE
93.2% UO2F2 3 IN AL SLAB 3X1X1 ARRAY 4.5 IN SEP H2O REFL
READ PARAM NPG=600 PDN=YES NUB=YES END PARAM
READ GEOM
UNIT 1
CUBOID 1 1 2P3.81 2P60.325 61.06 0
REFLECTOR 2 1 4R.318 0 .318 1
CUBOID 0 1 2P4.128 2P60.643 61.06 -.318
UNIT 2
CUBOID 3 1 11.43 0 2P60.643 61.06 -.318
CORE 0 1 3R0
REFLECTOR 3 2 4R3 0 3 6
END GEOM
READ ARRAY NUX=5 NUY=1 NUZ=1 FILL 1 2 1 2 1 END FILL END ARRAY
READ BIAS ID=500 2 7 END BIAS
END DATA
END
    
```

Table A.5 (continued)

```

CAS38
=CSAS25
93.2% UO2F2 H/U-235=337
27GROUPNDF4 MULTIREGION
SOLNUO2F2 1 81.845 0 1 293 92235 93.2
92238 6.8 END
AL 2 1 END
CARBONSTEEL 3 1 END
PLEXIGLASS 4 1 END
ARBMWOOD .640525 3 0 0 0 6012 44.435 1001 6.2639 8016 49.301 5 END
REG-CONCRETE 6 END
END COMP
SLAB END
1 3.81 NOEXTERMOD 2 4.12 NOEXTERMOD END ZONE
93.2% UO2F2 3 IN AL SLAB 3X1X1 ARRAY 5.5 IN SEP ROOM
READ PARAM NPG=600 FDN=YES NUB=YES END PARAM
READ GEOM
CUBOID 1 1 2P3.81 2P60.325 107.37 0
REFLECTOR 2 1 4R.318 0 .318 1
CUBOID 0 1 2P11.113 2P65. 150. -1.
CORE 0 1 -33.339 -65. -1.
CYLINDER 0 1 142.8 212. -60.
CYLINDER 3 1 144.8 212. -62.
CUBOID 0 1 275.5 -638.9 475. -744.2 588. -62.
REFLECTOR 4 1 5R0 .32 1
REFLECTOR 5 1 5R0 1.27 1
REFLECTOR 3 1 5R0 .64 1
REFLECTOR 0 1 5R0 365 1
REFLECTOR 6 2 6R3 10
REFLECTOR 6 12 0 3 4R0 10
END GEOM
READ BIAS ID=301 2 21 END BIAS
READ ARRAY NUX=3 NUY=1 NUZ=1 END ARRAY
END DATA
END

```

```

CAS39
=CSAS25
93.2% UO2F2 H/U-235=337
27GROUPNDF4 MULTIREGION
SOLNUO2F2 1 81.845 0 1 293 92235 93.2
92238 6.8 END
AL 2 1 END
H2O 3 1 END
END COMP
SLAB END
1 3.81 NOEXTERMOD 2 4.12 NOEXTERMOD 3 22.12 NOEXTERMOD END ZONE
93.2% UO2F2 3 IN AL SLAB 3X1X1 ARRAY 5.5 IN SEP H2O REFL
READ PARAM NPG=600 FDN=YES NUB=YES END PARAM
READ GEOM
UNIT 1
CUBOID 1 1 2P3.81 2P60.325 111.68 0
REFLECTOR 2 1 4R.318 0 .318 1
CUBOID 0 1 2P4.128 2P60.643 111.68 -.318
UNIT 2
CUBOID 3 1 13.97 0 2P60.643 111.68 -.318
CORE 0 1 3R0
REFLECTOR 3 2 4R3 0 3 6
END GEOM
READ ARRAY NUX=5 NUY=1 NUZ=1 FILL 1 2 1 2 1 END FILL END ARRAY
READ BIAS ID=500 2 7 END BIAS
END DATA
END

```

```

CAS40
=CSAS25
93.2% UO2F2 H/U-235=337
27GROUPNDF4 MULTIREGION
SOLNUO2F2 1 81.845 0 1 293 92235 93.2
92238 6.8 END
AL 2 1 END
CARBONSTEEL 3 1 END
PLEXIGLASS 4 1 END
ARBMWOOD .640525 3 0 0 0 6012 44.435 1001 6.2639 8016 49.301 5 END
REG-CONCRETE 6 END
END COMP
SLAB END
1 3.81 NOEXTERMOD 2 4.12 NOEXTERMOD END ZONE
93.2% UO2F2 3 IN AL SLAB 3X1X1 ARRAY 6 IN SEP ROOM
READ PARAM NPG=600 FDN=YES NUB=YES END PARAM
READ GEOM
CUBOID 1 1 2P3.81 2P60.325 120.4 0
REFLECTOR 2 1 4R.318 0 .318 1
CUBOID 0 1 2P11.748 2P65. 150. -1.
CORE 0 1 -35.244 -65. -1.
CYLINDER 0 1 142.8 212. -60.
CYLINDER 3 1 144.8 212. -62.
CUBOID 0 1 275.5 -638.9 475. -744.2 588. -62.
REFLECTOR 4 1 5R0 .32 1
REFLECTOR 5 1 5R0 1.27 1
REFLECTOR 3 1 5R0 .64 1
REFLECTOR 0 1 5R0 365 1
REFLECTOR 6 2 6R3 10
REFLECTOR 6 12 0 3 4R0 10
END GEOM
READ BIAS ID=301 2 21 END BIAS
READ ARRAY NUX=3 NUY=1 NUZ=1 END ARRAY
END DATA
END

```

```

CAS41
=CSAS25
93.2% UO2F2 H/U-235=337
27GROUPNDF4 MULTIREGION
SOLNUO2F2 1 81.845 0 1 293 92235 93.2
92238 6.8 END
AL 2 1 END
END COMP
SLAB END
1 3.81 NOEXTERMOD 2 4.12 NOEXTERMOD END ZONE
93.2% UO2F2 3, 6 IN AL SLABS 2X1X1 ARRAY 15 IN SEP
READ PARAM NPG=600 FDN=YES NUB=YES END PARAM
READ GEOM
UNIT 1
CUBOID 1 1 2P3.81 2P60.325 65.81 0
REFLECTOR 2 1 4R.318 0 .318 1
CUBOID 0 1 2P4.128 2P65. 150. -1.
UNIT 2
CUBOID 1 1 2P7.417 2P60.325 65.81 0
REFLECTOR 2 1 4R.318 0 .318 1
CUBOID 0 1 2P7.735 2P65. 150. -1.
UNIT 3
CUBOID 0 1 38.1 0 2P65. 150. -1.
END GEOM
READ ARRAY NUX=3 NUY=1 NUZ=1 FILL 2 3 1 END FILL END ARRAY
END DATA
END

```

Table A.5 (continued)

```

CAS42
=CSAS25
93.2% UO2F2 H/U-235=337
27GROUPNDF4 MULTIREGION
SOLNUO2F2 1 81.845 0 1 293 92235 93.2
92238 6.8 END
AL 2 1 END
END COMP
SLAB END
1 3.81 NOEXTERMOD 2 4.12 NOEXTERMOD END ZONE
93.2% UO2F2 3, 6 IN AL SLABS 2X1X1 ARRAY 2 IN SEP
READ PARAM NPG=600 FDN=YES NUB=YES END PARAM
READ GEOM
UNIT 1
CUBOID 1 1 2P3.81 2P60.325 32.39 0
REFLECTOR 2 1 4R.318 0 .318 1
CUBOID 0 1 2P4.128 2P65. 150. -1.
UNIT 2
CUBOID 1 1 2P7.417 2P60.325 32.39 0
REFLECTOR 2 1 4R.318 0 .318 1
CUBOID 0 1 2P7.735 2P65. 150. -1.
UNIT 3
CUBOID 0 1 5.08 0 2P65. 150. -1.
END GEOM
READ ARRAY NUX=3 NUY=1 NUZ=1 FILL 2 3 1 END FILL END ARRAY
END DATA
END
    
```

```

CAS43
=CSAS25
93.2% UO2F2 H/U-235=337
27GROUPNDF4 MULTIREGION
SOLNUO2F2 1 81.845 0 1 293 92235 93.2
92238 6.8 END
AL 2 1 END
END COMP
SLAB END
1 3.81 NOEXTERMOD 2 4.12 NOEXTERMOD END ZONE
93.2% UO2F2 3, 6 IN AL SLABS 2X1X1 ARRAY 30 IN SEP
READ PARAM NPG=600 FDN=YES NUB=YES END PARAM
READ GEOM
UNIT 1
CUBOID 1 1 2P3.81 2P60.325 92.48 0
REFLECTOR 2 1 4R.318 0 .318 1
CUBOID 0 1 2P4.128 2P65. 150. -1.
UNIT 2
CUBOID 1 1 2P7.417 2P60.325 92.48 0
REFLECTOR 2 1 4R.318 0 .318 1
CUBOID 0 1 2P7.735 2P65. 150. -1.
UNIT 3
CUBOID 0 1 76.2 0 2P65. 150. -1.
END GEOM
READ ARRAY NUX=3 NUY=1 NUZ=1 FILL 2 3 1 END FILL END ARRAY
END DATA
END
    
```

```

CAS44
=CSAS25
93.2% UO2F2 H/U-235=337
27GROUPNDF4 MULTIREGION
SOLNUO2F2 1 81.845 0 1 293 92235 93.2
92238 6.8 END
AL 2 1 END
END COMP
SLAB END
1 3.81 NOEXTERMOD 2 4.12 NOEXTERMOD END ZONE
93.2% UO2F2 3, 6 IN AL SLABS 2X1X1 ARRAY 48 IN SEP
READ PARAM NPG=600 FDN=YES NUB=YES END PARAM
READ GEOM
UNIT 1
CUBOID 1 1 2P3.81 2P60.325 113.84 0
REFLECTOR 2 1 4R.318 0 .318 1
CUBOID 0 1 2P4.128 2P65. 150. -1.
UNIT 2
CUBOID 1 1 2P7.417 2P60.325 113.84 0
REFLECTOR 2 1 4R.318 0 .318 1
CUBOID 0 1 2P7.735 2P65. 150. -1.
UNIT 3
CUBOID 0 1 121.92 0 2P65. 150. -1.
END GEOM
READ ARRAY NUX=3 NUY=1 NUZ=1 FILL 2 3 1 END FILL END ARRAY
END DATA
END
    
```

```

CAS45
=CSAS25
93.2% UO2F2 H/U-235=337
27GROUPNDF4 MULTIREGION
SOLNUO2F2 1 81.845 0 1 293 92235 93.2
92238 6.8 END
AL 2 1 END
END COMP
SLAB END
1 3.81 NOEXTERMOD 2 4.12 NOEXTERMOD END ZONE
93.2% UO2F2 3, 6, 3 IN AL SLABS 3X1X1 ARRAY 0 IN SEP
READ PARAM NPG=600 FDN=YES NUB=YES END PARAM
READ GEOM
UNIT 1
CUBOID 1 1 2P3.81 2P60.325 19.63 0
REFLECTOR 2 1 4R.318 0 .318 1
CUBOID 0 1 2P4.128 2P65. 150. -1.
UNIT 2
CUBOID 1 1 2P7.417 2P60.325 19.63 0
REFLECTOR 2 1 4R.318 0 .318 1
CUBOID 0 1 2P7.735 2P65. 150. -1.
END GEOM
READ ARRAY NUX=3 NUY=1 NUZ=1 FILL 1 2 1 END FILL END ARRAY
END DATA
END
    
```

Table A.5 (continued)

```

CAS46
=CSAS25
93.2% UO2F2 H/U-235=337
27GROUPNDF4 MULTIREGION
SOLNUO2F2 1 81.845 0 1 293 92235 93.2
92238 6.8 END
AL 2 1 END
END COMP
SLAB END
1 3.81 NOEXTERMOD 2 4.12 NOEXTERMOD END ZONE
93.2% UO2F2 3, 6, 3 IN AL SLABS 3X1X1 ARRAY 10 IN SEP
READ PARAM NPG=600 FDN=YES NUB=YES END PARAM
READ GEOM
UNIT 1
CUBOID 1 1 2P3.81 2P60.325 44.25 0
REFLECTOR 2 1 4R.318 0 .318 1
CUBOID 0 1 2P4.128 2P65. 150. -1.
UNIT 2
CUBOID 1 1 2P7.417 2P60.325 44.25 0
REFLECTOR 2 1 4R.318 0 .318 1
CUBOID 0 1 2P7.735 2P65. 150. -1.
UNIT 3
CUBOID 0 1 25.4 0 2P65. 150. -1.
END GEOM
READ ARRAY NUX=5 NUY=1 NUZ=1 FILL 1 3 2 3 1 END FILL END ARRAY
END DATA
END
    
```

```

CAS47
=CSAS25
93.2% UO2F2 H/U-235=337
27GROUPNDF4 MULTIREGION
SOLNUO2F2 1 81.845 0 1 293 92235 93.2
92238 6.8 END
AL 2 1 END
END COMP
SLAB END
1 3.81 NOEXTERMOD 2 4.12 NOEXTERMOD END ZONE
93.2% UO2F2 3, 6, 3 IN AL SLABS 3X1X1 ARRAY 20 IN SEP
READ PARAM NPG=600 FDN=YES NUB=YES END PARAM
READ GEOM
UNIT 1
CUBOID 1 1 2P3.81 2P60.325 62.56 0
REFLECTOR 2 1 4R.318 0 .318 1
CUBOID 0 1 2P4.128 2P65. 150. -1.
UNIT 2
CUBOID 1 1 2P7.417 2P60.325 62.56 0
REFLECTOR 2 1 4R.318 0 .318 1
CUBOID 0 1 2P7.735 2P65. 150. -1.
UNIT 3
CUBOID 0 1 50.8 0 2P65. 150. -1.
END GEOM
READ ARRAY NUX=5 NUY=1 NUZ=1 FILL 1 3 2 3 1 END FILL END ARRAY
END DATA
END
    
```

```

CAS48
=CSAS25
93.2% UO2F2 H/U-235=337
27GROUPNDF4 MULTIREGION
SOLNUO2F2 1 81.845 0 1 293 92235 93.2
92238 6.8 END
AL 2 1 END
END COMP
SLAB END
1 3.81 NOEXTERMOD 2 4.12 NOEXTERMOD END ZONE
93.2% UO2F2 3, 6, 3 IN AL SLABS 3X1X1 ARRAY 32 IN SEP
READ PARAM NPG=600 FDN=YES NUB=YES END PARAM
READ GEOM
UNIT 1
CUBOID 1 1 2P3.81 2P60.325 81.56 0
REFLECTOR 2 1 4R.318 0 .318 1
CUBOID 0 1 2P4.128 2P65. 150. -1.
UNIT 2
CUBOID 1 1 2P7.417 2P60.325 81.56 0
REFLECTOR 2 1 4R.318 0 .318 1
CUBOID 0 1 2P7.735 2P65. 150. -1.
UNIT 3
CUBOID 0 1 81.28 0 2P65. 150. -1.
END GEOM
READ ARRAY NUX=5 NUY=1 NUZ=1 FILL 1 3 2 3 1 END FILL END ARRAY
END DATA
END
    
```

```

CAS49
=CSAS25
93.2% UO2F2 H/U-235=337
27GROUPNDF4 MULTIREGION
SOLNUO2F2 1 81.845 0 1 293 92235 93.2
92238 6.8 END
AL 2 1 END
END COMP
SLAB END
1 7.62 NOEXTERMOD 2 7.94 NOEXTERMOD END ZONE
93.2% UO2F2 6 & 3 IN AL SLABS 2X1X1 ARRAY 12 IN SEP
READ PARAM NPG=600 FDN=YES NUB=YES END PARAM
READ GEOM
UNIT 1
CUBOID 1 1 2P3.81 2P60.325 58.19 0
REFLECTOR 2 1 4R.318 0 .318 1
CUBOID 0 1 2P4.128 2P65. 150. -1.
UNIT 2
CUBOID 2 1 2P.318 2P60.325 58.19 0
CUBOID 1 1 2P7.938 2P60.325 58.19 0
REFLECTOR 2 1 4R.318 0 .318 1
CUBOID 0 1 2P8.574 2P65. 150. -1.
UNIT 3
CUBOID 0 1 30.48 0 2P65. 150. -1.
END GEOM
READ ARRAY NUX=3 NUY=1 NUZ=1 FILL 2 3 1 END FILL END ARRAY
END DATA
END
    
```


Table A.5 (continued)

```

CAS50
=CSAS25
93.2% UO2F2 H/U-235=337
27GROUPNDF4 MULTIREGION
SOLNUO2F2 1 81.845 0 1 293 92235 93.2
92238 6.8 END
AL 2 1 END
END COMP
SLAB END
1 7.62 NOEXTERMOD 2 7.94 NOEXTERMOD END ZONE
93.2% UO2F2 6 & 3 IN AL SLABS 2X1X1 ARRAY 18 IN SEP
READ PARAM NPG=600 FDN=YES NUB=YES END PARAM
READ GEOM
UNIT 1
CUBOID 1 1 2P3.81 2P60.325 68.3 0
REFLECTOR 2 1 4R.318 0 .318 1
CUBOID 0 1 2P4.128 2P65. 150. -1.
UNIT 2
CUBOID 2 1 2P.318 2P60.325 68.3 0
CUBOID 1 1 2P7.938 2P60.325 68.3 0
REFLECTOR 2 1 4R.318 0 .318 1
CUBOID 0 1 2P8.574 2P65. 150. -1.
UNIT 3
CUBOID 0 1 45.72 0 2P65. 150. -1.
END GEOM
READ ARRAY NUX=3 NUY=1 NUZ=1 FILL 2 3 1 END FILL END ARRAY
END DATA
END

```

```

CAS51
=CSAS25
93.2% UO2F2 H/U-235=337
27GROUPNDF4 MULTIREGION
SOLNUO2F2 1 81.845 0 1 293 92235 93.2
92238 6.8 END
AL 2 1 END
END COMP
SLAB END
1 7.62 NOEXTERMOD 2 7.94 NOEXTERMOD END ZONE
93.2% UO2F2 6 & 3 IN AL SLABS 2X1X1 ARRAY 30 IN SEP
READ PARAM NPG=600 FDN=YES NUB=YES END PARAM
READ GEOM
UNIT 1
CUBOID 1 1 2P3.81 2P60.325 83.11 0
REFLECTOR 2 1 4R.318 0 .318 1
CUBOID 0 1 2P4.128 2P65. 150. -1.
UNIT 2
CUBOID 2 1 2P.318 2P60.325 83.11 0
CUBOID 1 1 2P7.938 2P60.325 83.11 0
REFLECTOR 2 1 4R.318 0 .318 1
CUBOID 0 1 2P8.574 2P65. 150. -1.
UNIT 3
CUBOID 0 1 76.2 0 2P65. 150. -1.
END GEOM
READ ARRAY NUX=3 NUY=1 NUZ=1 FILL 2 3 1 END FILL END ARRAY
END DATA
END

```

```

CAS52
=CSAS25
93.2% UO2F2 H/U-235=337
27GROUPNDF4 MULTIREGION
SOLNUO2F2 1 81.845 0 1 293 92235 93.2
92238 6.8 END
AL 2 1 END
END COMP
SLAB END
1 7.62 NOEXTERMOD 2 7.94 NOEXTERMOD END ZONE
93.2% UO2F2 6 & 3 IN AL SLABS 2X1X1 ARRAY 6 IN SEP
READ PARAM NPG=600 FDN=YES NUB=YES END PARAM
READ GEOM
UNIT 1
CUBOID 1 1 2P3.81 2P60.325 45.03 0
REFLECTOR 2 1 4R.318 0 .318 1
CUBOID 0 1 2P4.128 2P65. 150. -1.
UNIT 2
CUBOID 2 1 2P.318 2P60.325 45.03 0
CUBOID 1 1 2P7.938 2P60.325 45.03 0
REFLECTOR 2 1 4R.318 0 .318 1
CUBOID 0 1 2P8.574 2P65. 150. -1.
UNIT 3
CUBOID 0 1 15.24 0 2P65. 150. -1.
END GEOM
READ ARRAY NUX=3 NUY=1 NUZ=1 FILL 2 3 1 END FILL END ARRAY
END DATA
END

```

```

CAS53
=CSAS25
93.2% UO2F2 H/U-235=337
27GROUPNDF4 MULTIREGION
SOLNUO2F2 1 81.845 0 1 293 92235 93.2
92238 6.8 END
AL 2 1 END
END COMP
SLAB END
1 7.62 NOEXTERMOD 2 7.94 NOEXTERMOD END ZONE
93.2% UO2F2 6 IN AL SLAB 2X1X1 ARRAY 15 IN SEP
READ PARAM NPG=600 FDN=YES NUB=YES END PARAM
READ GEOM
UNIT 1
CUBOID 1 1 2P7.417 2P60.325 44.88 0
REFLECTOR 2 1 4R.318 0 .318 1
CUBOID 0 1 2P26.784 2P65. 150. -1.
UNIT 2
CUBOID 2 1 2P.318 2P60.325 44.88 0
CUBOID 1 1 2P7.938 2P60.325 44.88 0
REFLECTOR 2 1 4R.318 0 .318 1
CUBOID 0 1 2P27.305 2P65. 150. -1.
END GEOM
READ ARRAY NUX=2 NUY=1 NUZ=1 FILL 1 2 END FILL END ARRAY
END DATA
END

```

Table A.5 (continued)

```

CAS54
=CSAS25
93.2% UO2F2 H/U-235=337
27GROUPNDF4 MULTIREGION
SOLNUO2F2 1 81.845 0 1 293 92235 93.2
92238 6.8 END
AL 2 1 END
END COMP
SLAB END
1 7.62 NOEXTERMOD 2 7.94 NOEXTERMOD END ZONE
93.2% UO2F2 6 IN AL SLAB 2X1X1 ARRAY 2 IN SEP
READ PARAM NPG=600 FDN=YES NUB=YES END PARAM
READ GEOM
UNIT 1
CUBOID 1 1 2P7.417 2P60.325 25.43 0
REFLECTOR 2 1 4R.318 0 .318 1
CUBOID 0 1 2P10.274 2P65. 150. -1.
UNIT 2
CUBOUD 2 1 2P.318 2P60.325 25.43 0
CUBOID 1 1 2P7.938 2P60.325 25.43 0
REFLECTOR 2 1 4R.318 0 .318 1
CUBOID 0 1 2P10.795 2P65. 150. -1.
END GEOM
READ ARRAY NUX=2 NUY=1 NUZ=1 FILL 1 2 END FILL END ARRAY
END DATA
END
    
```

```

CAS55
=CSAS25
93.2% UO2F2 H/U-235=337
27GROUPNDF4 MULTIREGION
SOLNUO2F2 1 81.845 0 1 293 92235 93.2
92238 6.8 END
AL 2 1 END
END COMP
SLAB END
1 7.62 NOEXTERMOD 2 7.94 NOEXTERMOD END ZONE
93.2% UO2F2 6 IN AL SLAB 2X1X1 ARRAY 20 IN SEP
READ PARAM NPG=600 FDN=YES NUB=YES END PARAM
READ GEOM
UNIT 1
CUBOID 1 1 2P7.417 2P60.325 50.27 0
REFLECTOR 2 1 4R.318 0 .318 1
CUBOID 0 1 2P33.134 2P65. 150. -1.
UNIT 2
CUBOUD 2 1 2P.318 2P60.325 50.27 0
CUBOID 1 1 2P7.938 2P60.325 50.27 0
REFLECTOR 2 1 4R.318 0 .318 1
CUBOID 0 1 2P33.655 2P65. 150. -1.
END GEOM
READ ARRAY NUX=2 NUY=1 NUZ=1 FILL 1 2 END FILL END ARRAY
END DATA
END
    
```

```

CAS56
=CSAS25
93.2% UO2F2 H/U-235=337
27GROUPNDF4 MULTIREGION
SOLNUO2F2 1 81.845 0 1 293 92235 93.2
92238 6.8 END
AL 2 1 END
END COMP
SLAB END
1 7.62 NOEXTERMOD 2 7.94 NOEXTERMOD END ZONE
93.2% UO2F2 6 IN AL SLAB 2X1X1 ARRAY 30 IN SEP
READ PARAM NPG=600 FDN=YES NUB=YES END PARAM
READ GEOM
UNIT 1
CUBOID 1 1 2P7.417 2P60.325 59.72 0
REFLECTOR 2 1 4R.318 0 .318 1
CUBOID 0 1 2P45.834 2P65. 150. -1.
UNIT 2
CUBOUD 2 1 2P.318 2P60.325 59.72 0
CUBOID 1 1 2P7.938 2P60.325 59.72 0
REFLECTOR 2 1 4R.318 0 .318 1
CUBOID 0 1 2P46.355 2P65. 150. -1.
END GEOM
READ ARRAY NUX=2 NUY=1 NUZ=1 FILL 1 2 END FILL END ARRAY
END DATA
END
    
```

```

CAS57
=CSAS25
93.2% UO2F2 H/U-235=337
27GROUPNDF4 MULTIREGION
SOLNUO2F2 1 81.845 0 1 293 92235 93.2
92238 6.8 END
AL 2 1 END
END COMP
SLAB END
1 7.62 NOEXTERMOD 2 7.94 NOEXTERMOD END ZONE
93.2% UO2F2 6 IN AL SLAB 2X1X1 ARRAY 48 IN SEP
READ PARAM NPG=600 FDN=YES NUB=YES END PARAM
READ GEOM
UNIT 1
CUBOID 1 1 2P7.417 2P60.325 73.23 0
REFLECTOR 2 1 4R.318 0 .318 1
CUBOID 0 1 2P68.694 2P65. 150. -1.
UNIT 2
CUBOUD 2 1 2P.318 2P60.325 73.23 0
CUBOID 1 1 2P7.938 2P60.325 73.23 0
REFLECTOR 2 1 4R.318 0 .318 1
CUBOID 0 1 2P69.215 2P65. 150. -1.
END GEOM
READ ARRAY NUX=2 NUY=1 NUZ=1 FILL 1 2 END FILL END ARRAY
END DATA
END
    
```

Table A.5 (continued)

```

CAS58
=CSAS25
93.2% UO2F2 H/U-235=337
27GROUPNDF4 MULTIREGION
SOLNUO2F2 1 81.845 0 1 293 92235 93.2
92238 6.8 END
AL 2 1 END
END COMP
SLAB END
1 7.62 NOEXTERMOD 2 7.94 NOEXTERMOD END ZONE
93.2% UO2F2 6 IN AL SLAB 2X1X1 ARRAY 6 IN SEP
READ PARAM NPG=600 FDN=YES NUB=YES END PARAM
READ GEOM
UNIT 1
CUBOID 1 1 2P7.417 2P60.325 32.79 0
REFLECTOR 2 1 4R.318 0 .318 1
CUBOID 0 1 2P15.354 2P65. 150. -1.
UNIT 2
CUBOID 2 1 2P.318 2P60.325 32.79 0
CUBOID 1 1 2P7.938 2P60.325 32.79 0
REFLECTOR 2 1 4R.318 0 .318 1
CUBOID 0 1 2P15.875 2P65. 150. -1.
END GEOM
READ ARRAY NUX=2 NUY=1 NUZ=1 FILL 1 2 END FILL END ARRAY
END DATA
END

```

```

CAS59
=CSAS25
93.2% UO2F2 H/U-235=337
27GROUPNDF4 MULTIREGION
SOLNUO2F2 1 81.845 0 1 293 92235 93.2
92238 6.8 END
AL 2 1 END
END COMP
SLAB END
1 7.62 NOEXTERMOD 2 7.94 NOEXTERMOD END ZONE
93.2% UO2F2 6 IN AL SLAB 2X1X1 ARRAY 66 IN SEP
READ PARAM NPG=600 FDN=YES NUB=YES END PARAM
READ GEOM
UNIT 1
CUBOID 1 1 2P7.417 2P60.325 82.12 0
REFLECTOR 2 1 4R.318 0 .318 1
CUBOID 0 1 2P91.554 2P65. 150. -1.
UNIT 2
CUBOID 2 1 2P.318 2P60.325 82.12 0
CUBOID 1 1 2P7.938 2P60.325 82.12 0
REFLECTOR 2 1 4R.318 0 .318 1
CUBOID 0 1 2P92.075 2P65. 150. -1.
END GEOM
READ ARRAY NUX=2 NUY=1 NUZ=1 FILL 1 2 END FILL END ARRAY
END DATA
END

```

```

CAS60
=CSAS25
UO2(NO3)2 279 G U/L
27GROUPNDF4 MULTIREGION
SOLNUO2(NO3)2 1 279 0 1 293 92235 92.6 92238 7.4 END
FLEXIGLASS 2 1 END
ARBWOOD .640525 3 0 0 0 6012 44.435 1001 6.2639 8016 49.301 3 END
CARBONSTEEL 4 END
REG-CONCRETE 5 END
END COMP
CYLINDRICAL END
1 9.52 ONEEXTERMOD 2 10.16 NOEXTERMOD END ZONE
UO2(NO3)2 279 G U/L 3X3X3 ARRAY UNREFL. WALLS, TANK, & FLOOR
READ PARAM NPG=600 FDN=YES NUB=YES PLT=NO END PARAM
READ GEOM
UNIT 1
CYLINDER 1 1 9.52 17.5609 0.
CYLINDER 0 1 9.52 17.77 0.
CYLINDER 2 1 10.16 18.41 -.64
CUBOID 0 1 4P13.36 21.61 -3.84
UNIT 2
ARRAY 1 2R-40.08 0.
CUBOID 0 1 4P200. 250. -50.
UNIT 3
CYLINDER 0 1 142.8 224. -48.
CYLINDER 4 1 144.8 224. -50.
CUBOID 0 1 218.1 -181.9 215. -185. 250. -50.
ARRAY 2 3R0.
REFLECTOR 0 1 57.4 57. 260. 559.2 400. 0. 1
REFLECTOR 2 1 5R0 .32 1
REFLECTOR 3 1 5R0 1.27 1
REFLECTOR 4 1 5R0 .64 1
REFLECTOR 0 1 5R0 365 1
REFLECTOR 5 2 6R3 10
REFLECTOR 5 12 0 3 4R0 10
END GEOM
READ START XSM=160 XSP=240 YSM=160 YSP=240 ZSM=50 ZSP=127 END START
READ BIAS ID=301 2 21 END BIAS
READ ARRAY ARA=1 NUX=3 NUY=3 NUZ=3 FILL F1 END FILL
ARA=2 NUX=2 NUY=1 NUZ=1 FILL 2 3 END FILL END ARRAY
READ PLOT PLT=NO
XUL=113.2 YUL=286.8 ZUL=60. XLR=286.8 YLR=113.2 ZLR=60.
UAX=1 VDN=-1 NAX=125 END
XUL=437.1 YUL=329.8 ZUL=60. XLR=726.7 YLR=40.2 ZLR=60. END
END PLOT
END DATA
END

```

Table A.5 (continued)

```

CAS61
=CSAS25
UO2(NO3)2 279 G U/L
27GROUPNDF4 MULTIREGION
SOLNUO2(NO3)2 1 279 0 1 293 92235 92.6 92238 7.4 END
PLEXIGLASS 2 1 END
ARBMWOOD .640525 3 0 0 0 6012 44.435 1001 6.2639 8016 49.301 3 END
CARBONSTEEL 4 END
REG-CONCRETE 5 END
END COMP
CYLINDRICAL END
1 9.52 ONEEXTERMOD 2 10.16 NOEXTERMOD END ZONE
UO2(NO3)2 279 G U/L 2X2X2 ARRAY UNREPL. WALLS, TANK, & FLOOR
READ PARAM PLT=NO NPG=600 FDN=YES NUB=YES END PARAM
READ GEOM
UNIT 1
CYLINDER 1 1 9.52 17.5609 0.
CYLINDER 0 1 9.52 17.77 0.
CYLINDER 2 1 10.16 18.41 -.64
CUBOID 0 1 4P10.875 19.125 -1.355
UNIT 2
ARRAY 1 2R-21.75 0.
CUBOID 0 1 4P200. 250. -50.
UNIT 3
CYLINDER 0 1 142.8 224. -48.
CYLINDER 4 1 144.8 224. -50.
CUBOID 0 1 218.1 -181.9 215. -185. 250. -50.
ARRAY 2 3R0.
REFLECTOR 0 1 57.4 57. 260. 559.2 400. 0. 1
REFLECTOR 2 1 5R0 .32 1
REFLECTOR 3 1 5R0 1.27 1
REFLECTOR 4 1 5R0 .64 1
REFLECTOR 0 1 5R0 365 1
REFLECTOR 5 2 6R3 10
REFLECTOR 5 12 0 3 4R0 10
END GEOM
READ START XSM=178 XSP=222 YSM=178 YSP=222 ZSM=50 ZSP=91 END START
READ BIAS ID=301 2 21 END BIAS
READ ARRAY ARA=1 NUX=2 NUY=2 NUZ=2 FILL F1 END FILL
ARA=2 NUX=2 NUY=1 NUZ=1 FILL 2 3 END FILL END ARRAY
READ PLOT
XUL=113.2 YUL=286.8 ZUL=60. XLR=286.8 YLR=113.2 ZLR=60.
UAX=1 VDN=-1 NAX=125 END
XUL=437.1 YUL=329.8 ZUL=60. XLR=726.7 YLR=40.2 ZLR=60. END
END PLOT
END DATA
END

```

```

CAS62
=CSAS25
UO2(NO3)2 415 G U/L
27GROUPNDF4 MULTIREGION
SOLNUO2(NO3)2 1 415 0 1 293 92235 92.6 92238 7.4 END
PLEXIGLASS 2 1 END
ARBMWOOD .640525 3 0 0 0 6012 44.435 1001 6.2639 8016 49.301 3 END
CARBONSTEEL 4 END
REG-CONCRETE 5 END
END COMP
CYLINDRICAL END
1 9.52 ONEEXTERMOD 2 10.16 NOEXTERMOD END ZONE
UO2(NO3)2 415 G U/L 5X5X5 ARRAY UNREPL. WALLS, TANK, & FLOOR
READ PARAM PLT=NO NPG=600 FDN=YES NUB=YES END PARAM
READ GEOM
UNIT 1
CYLINDER 1 1 9.52 17.5609 0.
CYLINDER 0 1 9.52 17.77 0.
CYLINDER 2 1 10.16 18.41 -.64
CUBOID 0 1 4P17.36 25.61 -7.84
UNIT 2
ARRAY 1 2R-86.8 0.
CUBOID 0 1 4P200. 250. -50.
UNIT 3
CYLINDER 0 1 142.8 224. -48.
CYLINDER 4 1 144.8 224. -50.
CUBOID 0 1 218.1 -181.9 215. -185. 250. -50.
ARRAY 2 3R0.
REFLECTOR 0 1 57.4 57. 260. 559.2 400. 0. 1
REFLECTOR 2 1 5R0 .32 1
REFLECTOR 3 1 5R0 1.27 1
REFLECTOR 4 1 5R0 .64 1
REFLECTOR 0 1 5R0 365 1
REFLECTOR 5 2 6R3 10
REFLECTOR 5 12 0 3 4R0 10
END GEOM
READ START XSM=113 XSP=287 YSM=113 YSP=287 ZSM=50 ZSP=151 END START
READ BIAS ID=301 2 21 END BIAS
READ ARRAY ARA=1 NUX=5 NUY=5 NUZ=5 FILL F1 END FILL
ARA=2 NUX=2 NUY=1 NUZ=1 FILL 2 3 END FILL END ARRAY
READ PLOT
XUL=113.2 YUL=286.8 ZUL=60. XLR=286.8 YLR=113.2 ZLR=60.
UAX=1 VDN=-1 NAX=125 END
XUL=437.1 YUL=329.8 ZUL=60. XLR=726.7 YLR=40.2 ZLR=60. END
END PLOT
END DATA
END

```

Table A.5 (continued)

```

CAS63
-CSAS25
UO2(NO3)2 415 G U/L
27GROUPNDF4 MULTIREGION
SOLNUO2(NO3)2 1 415 0 1 293 92235 92.6 92238 7.4 END
PLEXIGLASS 2 1 END
ARBMWOOD .640525 3 0 0 0 6012 44.435 1001 6.2639 8016 49.301 3 END
CARBONSTEEL 4 END
REG-CONCRETE 5 END
END COMP
CYLINDRICAL END
1 9.52 ONEEXTERMOD 2 10.16 NOEXTERMOD END ZONE
UO2(NO3)2 415 G U/L 3X3X3 ARRAY UNREFL. WALLS, TANK, & FLOOR
READ PARAM PLT=NO NPG=600 PDN=YES NUB=YES END PARAM
READ GEOM
UNIT 1
CYLINDER 1 1 9.52 17.5609 0.
CYLINDER 0 1 9.52 17.77 0.
CYLINDER 2 1 10.16 18.41 -.64
CUBOID 0 1 4P13.40 21.65 -3.88
UNIT 2
ARRAY 1 2R-40.2 0.
CUBOID 0 1 4P200. 250. -50.
UNIT 3
CYLINDER 0 1 142.8 224. -48.
CYLINDER 4 1 144.8 224. -50.
CUBOID 0 1 218.1 -181.9 215. -185. 250. -50.
ARRAY 2 3R0.
REFLECTOR 0 1 57.4 57. 260. 559.2 400. 0. 1
REFLECTOR 2 1 5R0 .32 1
REFLECTOR 3 1 5R0 1.27 1
REFLECTOR 4 1 5R0 .64 1
REFLECTOR 0 1 5R0 365 1
REFLECTOR 5 2 6R3 10
REFLECTOR 5 12 0 3 4R0 10
END GEOM
READ START XSM=160 XSP=240 YSM=160 YSP=240 ZSM=50 ZSP=127 END START
READ BIAS ID=301 2 21 END BIAS
READ ARRAY ARA=1 NUX=3 NUY=3 NUZ=3 FILL F1 END FILL
ARA=2 NUX=2 NUY=1 NUZ=1 FILL 2 3 END FILL END ARRAY
READ PLOT
XUL=113.2 YUL=286.8 ZUL=60. XLR=286.8 YLR=113.2 ZLR=60.
UAX=1 VDN=-1 NAX=125 END
XUL=437.1 YUL=329.8 ZUL=60. XLR=726.7 YLR=40.2 ZLR=60. END
END PLOT
END DATA
END

```

```

CAS64
-CSAS25
UO2(NO3)2 415 G U/L
27GROUPNDF4 MULTIREGION
SOLNUO2(NO3)2 1 415 0 1 293 92235 92.6 92238 7.4 END
PLEXIGLASS 2 1 END
ARBMWOOD .640525 3 0 0 0 6012 44.435 1001 6.2639 8016 49.301 3 END
CARBONSTEEL 4 END
REG-CONCRETE 5 END
END COMP
CYLINDRICAL END
1 9.52 ONEEXTERMOD 2 10.16 NOEXTERMOD END ZONE
UO2(NO3)2 415 G U/L 4X4X4 ARRAY UNREFL. WALLS, FLOOR, & TANK
READ PARAM PLT=NO NPG=600 PDN=YES NUB=YES END PARAM
READ GEOM
UNIT 1
CYLINDER 1 1 9.52 17.5609 0.
CYLINDER 0 1 9.52 17.77 0.
CYLINDER 2 1 10.16 18.41 -.64
CUBOID 0 1 4P15.495 23.745 -5.975
UNIT 2
ARRAY 1 2R-61.98 0.
CUBOID 0 1 4P200. 250. -50.
UNIT 3
CYLINDER 0 1 142.8 224. -48.
CYLINDER 4 1 144.8 224. -50.
CUBOID 0 1 218.1 -181.9 215. -185. 250. -50.
ARRAY 2 3R0.
REFLECTOR 0 1 57.4 57. 260. 559.2 400. 0. 1
REFLECTOR 2 1 5R0 .32 1
REFLECTOR 3 1 5R0 1.27 1
REFLECTOR 4 1 5R0 .64 1
REFLECTOR 0 1 5R0 365 1
REFLECTOR 5 2 6R3 10
REFLECTOR 5 12 0 3 4R0 10
END GEOM
READ START XSM=138 XSP=262 YSM=138 YSP=262 ZSM=50 ZSP=169 END START
READ BIAS ID=301 2 21 END BIAS
READ ARRAY ARA=1 NUX=4 NUY=4 NUZ=4 FILL F1 END FILL
ARA=2 NUX=2 NUY=1 NUZ=1 FILL 2 3 END FILL END ARRAY
READ PLOT
XUL=113.2 YUL=286.8 ZUL=60. XLR=286.8 YLR=113.2 ZLR=60.
UAX=1 VDN=-1 NAX=125 END
XUL=437.1 YUL=329.8 ZUL=60. XLR=726.7 YLR=40.2 ZLR=60. END
END PLOT
END DATA
END

```

Table A.5 (continued)

```

CAS65
=CSAS25
UO2(NO3)2 415 G U/L
27GROUPNDF4 MULTIREGION
SOLNUO2(NO3)2 1 415 0 1 293 92235 92.6 92238 7.4 END
PLEXIGLASS 2 1 END
ARBMWOOD .640525 3 0 0 0 6012 44.435 1001 6.2639 8016 49.301 3 END
CARBONSTEEL 4 END
REG-CONCRETE 5 END
END COMP
CYLINDRICAL END
1 9.52 ONEEXTERMOD 2 10.16 NOEXTERMOD END ZONE
UO2(NO3)2 415 G U/L 2X2X2 ARRAY UNREPL. WALLS, FLOOR, & TANK
READ PARAM PLT=NO NPG=600 FDN=YES NUB=YES END PARAM
READ GEOM
UNIT 1
CYLINDER 1 1 9.52 17.5609 0.
CYLINDER 0 1 9.52 17.77 0.
CYLINDER 2 1 10.16 18.41 -.64
CUBOID 0 1 4P10.875 19.125 -1.355
UNIT 2
ARRAY 1 2R-21.75 0.
CUBOID 0 1 4P200. 250. -50.
UNIT 3
CYLINDER 0 1 142.8 224. -48.
CYLINDER 4 1 144.8 224. -50.
CUBOID 0 1 218.1 -181.9 215. -185. 250. -50.
ARRAY 2 3R0.
REFLECTOR 0 1 57.4 57. 260. 559.2 400. 0. 1
REFLECTOR 2 1 5R0 .32 1
REFLECTOR 3 1 5R0 1.27 1
REFLECTOR 4 1 5R0 .64 1
REFLECTOR 0 1 5R0 365 1
REFLECTOR 5 2 6R3 10
REFLECTOR 5 12 0 3 4R0 10
END GEOM
READ START XSM=178 XSP=222 YSM=178 YSP=222 ZSM=50 ZSP=91 END START
READ BIAS ID=301 2 21 END BIAS
READ ARRAY ARA=1 NUX=2 NUY=2 NUZ=2 FILL F1 END FILL
ARA=2 NUX=2 NUY=1 NUZ=1 FILL 2 3 END FILL END ARRAY
READ PLOT
XUL=113.2 YUL=286.8 ZUL=60. XLR=286.8 YLR=113.2 ZLR=60.
UAX=1 VDN=-1 MAX=125 END
XUL=437.1 YUL=329.8 ZUL=60. XLR=726.7 YLR=40.2 ZLR=60. END
END PLOT
END DATA
END

```

```

CAS66
=CSAS25
UO2(NO3)2 415 G U/L
27GROUPNDF4 MULTIREGION
SOLNUO2(NO3)2 1 415 0 1 293 92235 92.6 92238 7.4 END
PLEXIGLASS 2 1 END
PARAFFIN 3 1 END
END COMP
CYLINDRICAL END
1 9.52 ONEEXTERMOD 2 10.16 NOEXTERMOD END ZONE
UO2(NO3)2 415 G U/L 3X3X3 ARRAY 15.24 CM PAR. BOT., 1.27 CM PLEX.
READ PARAM NPG=600 FDN=YES NUB=YES END PARAM
READ GEOM
CYLINDER 1 1 9.52 17.5609 0.
CYLINDER 0 1 9.52 17.77 0.
CYLINDER 2 1 10.16 18.41 -.64
CUBOID 0 1 4P14.95 23.20 -5.43
CORE 0 1 3R0.
REFLECTOR 2 2 5R1.27 0 1
REFLECTOR 3 2 5R0 3 4
REFLECTOR 3 6 5R0 3.24 1
END GEOM
READ BIAS ID=400 2 6 END BIAS
READ ARRAY NUX=3 NUY=3 NUZ=3 END ARRAY
END DATA
END

```

```

CAS67
=CSAS25
UO2(NO3)2 415 G U/L
27GROUPNDF4 MULTIREGION
SOLNUO2(NO3)2 1 415 0 1 293 92235 92.6 92238 7.4 END
PLEXIGLASS 2 1 END
PARAFFIN 3 1 END
END COMP
CYLINDRICAL END
1 9.52 ONEEXTERMOD 2 10.16 NOEXTERMOD END ZONE
UO2(NO3)2 415 G U/L 3X3X3 ARRAY 15.24 CM PAR. BOT., 2.54 CM PLEX.
READ PARAM NPG=600 FDN=YES NUB=YES END PARAM
READ GEOM
CYLINDER 1 1 9.52 17.5609 0.
CYLINDER 0 1 9.52 17.77 0.
CYLINDER 2 1 10.16 18.41 -.64
CUBOID 0 1 4P16.13 24.38 -6.61
CORE 0 1 3R0.
REFLECTOR 2 2 5R2.54 0 1
REFLECTOR 3 2 5R0 3 4
REFLECTOR 3 6 5R0 3.24 1
END GEOM
READ BIAS ID=400 2 6 END BIAS
READ ARRAY NUX=3 NUY=3 NUZ=3 END ARRAY
END DATA
END

```

Table A.5 (continued)

```

CAS68
=CSAS25
UO2(NO3)2 415 G U/L
27GROUPNDF4 MULTIREGION
SOLNUO2(NO3)2 1 415 0 1 293 92235 92.6 92238 7.4 END
PLEXIGLASS 2 1 END
PARAFFIN 3 1 END
END COMP
CYLINDRICAL END
1 9.52 ONEEXTERMOD 2 10.16 NOEXTERMOD END ZONE
UO2(NO3)2 415 G U/L 3X3X3 ARRAY 15.24 CM PAR. BOT., 1.27 CM PAR.
READ PARAM NPG=600 FDN=YES NUB=YES END PARAM
READ GEOM
CYLINDER 1 1 9.52 17.5609 0.
CYLINDER 0 1 9.52 17.77 0.
CYLINDER 2 1 10.16 18.41 -.64
CUBOID 0 1 4P15.10 23.35 -5.58
CORE 0 1 3R0.
REFLECTOR 3 2 5R1.27 0 1
REFLECTOR 3 2 5R0 3 4
REFLECTOR 3 6 5R0 3.24 1
END GEOM
READ BIAS ID=400 2 6 END BIAS
READ ARRAY NUX=3 NUY=3 NUZ=3 END ARRAY
END DATA
END

```

```

CAS69
=CSAS25
UO2(NO3)2 415 G U/L
27GROUPNDF4 MULTIREGION
SOLNUO2(NO3)2 1 415 0 1 293 92235 92.6 92238 7.4 END
PLEXIGLASS 2 1 END
PARAFFIN 3 1 END
END COMP
CYLINDRICAL END
1 9.52 ONEEXTERMOD 2 10.16 NOEXTERMOD END ZONE
UO2(NO3)2 415 G U/L 3X3X3 ARRAY 15.24 CM PAR 5 FC, PLEX 1 FC
READ PARAM NPG=600 FDN=YES NUB=YES END PARAM
READ GEOM
CYLINDER 1 1 9.52 17.5609 0.
CYLINDER 0 1 9.52 17.77 0.
CYLINDER 2 1 10.16 18.41 -.64
CUBOID 0 1 4P18.615 26.865 -9.095
CORE 0 1 3R0.
REFLECTOR 3 2 0 5R3 4
REFLECTOR 3 6 0 5R3.24 1
REFLECTOR 2 2 3 5R0 4
REFLECTOR 2 6 3.24 5R0 1
END GEOM
READ BIAS ID=400 2 6 END BIAS
READ ARRAY NUX=3 NUY=3 NUZ=3 END ARRAY
END DATA
END

```

```

CAS70
=CSAS25
UO2(NO3)2 415 G U/L
27GROUPNDF4 MULTIREGION
SOLNUO2(NO3)2 1 415 0 1 293 92235 92.6 92238 7.4 END
PLEXIGLASS 2 1 END
PARAFFIN 3 1 END
END COMP
CYLINDRICAL END
1 9.52 ONEEXTERMOD 2 10.16 NOEXTERMOD END ZONE
UO2(NO3)2 415 G U/L 3X3X3 ARRAY 15.24 CM PAR. BOT., 3.81 CM PAR.
READ PARAM NPG=600 FDN=YES NUB=YES END PARAM
READ GEOM
CYLINDER 1 1 9.52 17.5609 0.
CYLINDER 0 1 9.52 17.77 0.
CYLINDER 2 1 10.16 18.41 -.64
CUBOID 0 1 4P17.295 25.545 -7.775
CORE 0 1 3R0.
REFLECTOR 3 2 5R3.81 0 1
REFLECTOR 3 2 5R0 3 4
REFLECTOR 3 6 5R0 3.24 1
END GEOM
READ BIAS ID=400 2 6 END BIAS
READ ARRAY NUX=3 NUY=3 NUZ=3 END ARRAY
END DATA
END

```

```

CAS71
=CSAS25
UO2(NO3)2 415 G U/L
27GROUPNDF4 MULTIREGION
SOLNUO2(NO3)2 1 415 0 1 293 92235 92.6 92238 7.4 END
PLEXIGLASS 2 1 END
PARAFFIN 3 1 END
END COMP
CYLINDRICAL END
1 9.52 ONEEXTERMOD 2 10.16 NOEXTERMOD END ZONE
UO2(NO3)2 415 G U/L 3X3X3 ARRAY 15.24 CM PAR. BOT., 7.62 CM PAR.
READ PARAM NPG=600 FDN=YES NUB=YES END PARAM
READ GEOM
CYLINDER 1 1 9.52 17.5609 0.
CYLINDER 0 1 9.52 17.77 0.
CYLINDER 2 1 10.16 18.41 -.64
CUBOID 0 1 4P18.085 26.335 -8.565
CORE 0 1 3R0.
REFLECTOR 3 2 5R3 0 2
REFLECTOR 3 4 5R1.62 0 1
REFLECTOR 3 2 5R0 3 4
REFLECTOR 3 6 5R0 3.24 1
END GEOM
READ BIAS ID=400 2 6 END BIAS
READ ARRAY NUX=3 NUY=3 NUZ=3 END ARRAY
END DATA
END

```

Table A.5 (continued)

```

CAS72
=CSAS25
UO2(NO3)2 415 G U/L
27GROUPNDF4 MULTIREGION
SOLNUO2(NO3)2 1 415 0 1 293 92235 92.6 92238 7.4 END
PLEXIGLASS 2 1 END
PARAFFIN 3 1 END
END COMP
CYLINDRICAL END
1 9.52 ONEEXTERMOD 2 10.16 NOEXTERMOD END ZONE
UO2(NO3)2 415 G U/L 3X3X3 ARRAY 1.27 CM PLEXIGLASS REFL.
READ PARAM NPG=600 FDN=YES NUB=YES END PARAM
READ GEOM
CYLINDER 1 1 9.52 17.5609 0.
CYLINDER 0 1 9.52 17.77 0.
CYLINDER 2 1 10.16 18.41 -.64
CUBOID 0 1 4P14.54 22.79 -5.02
CORE 0 1 3R0.
REFLECTOR 2 2 6R1.27 1
END GEOM
READ BIAS ID=400 2 6 END BIAS
READ ARRAY NUX=3 NUY=3 NUZ=3 END ARRAY
END DATA
END

```

```

CAS73
=CSAS25
UO2(NO3)2 415 G U/L
27GROUPNDF4 MULTIREGION
SOLNUO2(NO3)2 1 415 0 1 293 92235 92.6 92238 7.4 END
PLEXIGLASS 2 1 END
PARAFFIN 3 1 END
END COMP
CYLINDRICAL END
1 9.52 ONEEXTERMOD 2 10.16 NOEXTERMOD END ZONE
UO2(NO3)2 415 G U/L 3X3X3 ARRAY 1.27 CM PARAFFIN REFL.
READ PARAM NPG=600 FDN=YES NUB=YES END PARAM
READ GEOM
CYLINDER 1 1 9.52 17.5609 0.
CYLINDER 0 1 9.52 17.77 0.
CYLINDER 2 1 10.16 18.41 -.64
CUBOID 0 1 4P14.67 22.92 -5.15
CORE 0 1 3R0.
REFLECTOR 3 2 6R1.27 1
END GEOM
READ BIAS ID=400 2 6 END BIAS
READ ARRAY NUX=3 NUY=3 NUZ=3 END ARRAY
END DATA
END

```

```

CAS74
=CSAS25
UO2(NO3)2 415 G U/L
27GROUPNDF4 MULTIREGION
SOLNUO2(NO3)2 1 415 0 1 293 92235 92.6 92238 7.4 END
PLEXIGLASS 2 1 END
PARAFFIN 3 1 END
END COMP
CYLINDRICAL END
1 9.52 ONEEXTERMOD 2 10.16 NOEXTERMOD END ZONE
UO2(NO3)2 415 G U/L 3X3X3 ARRAY 15.24 CM PARAFFIN REFL.
READ PARAM NPG=600 FDN=YES NUB=YES END PARAM
READ GEOM
CYLINDER 1 1 9.52 17.5609 0.
CYLINDER 0 1 9.52 17.77 0.
CYLINDER 2 1 10.16 18.41 -.64
CUBOID 0 1 4P18.425 26.675 -8.905
CORE 0 1 3R0.
REFLECTOR 3 2 6R3 4
REFLECTOR 3 6 6R3.24 1
END GEOM
READ BIAS ID=400 2 6 END BIAS
READ ARRAY NUX=3 NUY=3 NUZ=3 END ARRAY
END DATA
END

```

```

CAS75
=CSAS25
UO2(NO3)2 415 G U/L
27GROUPNDF4 MULTIREGION
SOLNUO2(NO3)2 1 415 0 1 293 92235 92.6 92238 7.4 END
PLEXIGLASS 2 1 END
PARAFFIN 3 1 END
END COMP
CYLINDRICAL END
1 9.52 ONEEXTERMOD 2 10.16 NOEXTERMOD END ZONE
UO2(NO3)2 415 G U/L 3X3X3 ARRAY 3.81 CM PARAFFIN REFL.
READ PARAM NPG=600 FDN=YES NUB=YES END PARAM
READ GEOM
CYLINDER 1 1 9.52 17.5609 0.
CYLINDER 0 1 9.52 17.77 0.
CYLINDER 2 1 10.16 18.41 -.64
CUBOID 0 1 4P17.005 25.255 -7.485
CORE 0 1 3R0.
REFLECTOR 3 2 6R3.81 1
END GEOM
READ BIAS ID=400 2 6 END BIAS
READ ARRAY NUX=3 NUY=3 NUZ=3 END ARRAY
END DATA
END

```


Table A.5 (continued)

```

CAS76
=CSAS25
UO2(NO3)2 415 G U/L
27GROUPNDF4 MULTIREGION
SOLNUO2(NO3)2 1 415 0 1 293 92235 92.6 92238 7.4 END
PLEXIGLASS 2 1 END
PARAFFIN 3 1 END
END COMP
CYLINDRICAL END
1 9.52 ONEEXTERMOD 2 10.16 NOEXTERMOD END ZONE
UO2(NO3)2 415 G U/L 2X2X2 ARRAY 15.24 CM PAR. BOT., 1.27 CM PLEX.
READ PARAM NPG=600 FDN=YES NUB=YES END PARAM
READ GEOM
CYLINDER 1 1 9.52 17.5609 0.
CYLINDER 0 1 9.52 17.77 0.
CYLINDER 2 1 10.16 18.41 -.64
CUBOID 0 1 4P11.965 20.215 -2.445
CORE 0 1 3R0.
REFLECTOR 2 2 5R1.27 0 1
REFLECTOR 3 2 5R0 3 4
REFLECTOR 3 6 5R0 3.24 1
END GEOM
READ BIAS ID=400 2 6 END BIAS
READ ARRAY NUX=2 NUY=2 NUZ=2 END ARRAY
END DATA
END
    
```

```

CAS77
=CSAS25
UO2(NO3)2 415 G U/L
27GROUPNDF4 MULTIREGION
SOLNUO2(NO3)2 1 415 0 1 293 92235 92.6 92238 7.4 END
PLEXIGLASS 2 1 END
PARAFFIN 3 1 END
END COMP
CYLINDRICAL END
1 9.52 ONEEXTERMOD 2 10.16 NOEXTERMOD END ZONE
UO2(NO3)2 415 G U/L 2X2X2 ARRAY 15.24 CM PAR. BOT., 11.43 CM PLEX.
READ PARAM NPG=600 FDN=YES NUB=YES END PARAM
READ GEOM
CYLINDER 1 1 9.52 17.5609 0.
CYLINDER 0 1 9.52 17.77 0.
CYLINDER 2 1 10.16 18.41 -.64
CUBOID 0 1 4P14.925 23.175 -5.405
CORE 0 1 3R0.
REFLECTOR 2 2 5R3.0 0 3
REFLECTOR 2 5 5R2.43 0 1
REFLECTOR 3 2 5R0 3 4
REFLECTOR 3 6 5R0 3.24 1
END GEOM
READ BIAS ID=400 2 6 END BIAS
READ ARRAY NUX=2 NUY=2 NUZ=2 END ARRAY
END DATA
END
    
```

```

CAS78
=CSAS25
UO2(NO3)2 415 G U/L
27GROUPNDF4 MULTIREGION
SOLNUO2(NO3)2 1 415 0 1 293 92235 92.6 92238 7.4 END
PLEXIGLASS 2 1 END
PARAFFIN 3 1 END
END COMP
CYLINDRICAL END
1 9.52 ONEEXTERMOD 2 10.16 NOEXTERMOD END ZONE
UO2(NO3)2 415 G U/L 2X2X2 ARRAY 15.24 CM PAR. BOT., 15.24 CM PLEX.
READ PARAM NPG=600 FDN=YES NUB=YES END PARAM
READ GEOM
CYLINDER 1 1 9.52 17.5609 0.
CYLINDER 0 1 9.52 17.77 0.
CYLINDER 2 1 10.16 18.41 -.64
CUBOID 0 1 4P14.96 23.21 -5.44
CORE 0 1 3R0.
REFLECTOR 2 2 5R3.0 0 4
REFLECTOR 2 6 5R3.24 0 1
REFLECTOR 3 2 5R0 3 4
REFLECTOR 3 6 5R0 3.24 1
END GEOM
READ BIAS ID=400 2 6 END BIAS
READ ARRAY NUX=2 NUY=2 NUZ=2 END ARRAY
END DATA
END
    
```

```

CAS79
=CSAS25
UO2(NO3)2 415 G U/L
27GROUPNDF4 MULTIREGION
SOLNUO2(NO3)2 1 415 0 1 293 92235 92.6 92238 7.4 END
PLEXIGLASS 2 1 END
PARAFFIN 3 1 END
END COMP
CYLINDRICAL END
1 9.52 ONEEXTERMOD 2 10.16 NOEXTERMOD END ZONE
UO2(NO3)2 415 G U/L 2X2X2 ARRAY 15.24 CM PAR. BOT., 2.54 CM PLEX.
READ PARAM NPG=600 FDN=YES NUB=YES END PARAM
READ GEOM
CYLINDER 1 1 9.52 17.5609 0.
CYLINDER 0 1 9.52 17.77 0.
CYLINDER 2 1 10.16 18.41 -.64
CUBOID 0 1 4P12.865 21.115 -3.345
CORE 0 1 3R0.
REFLECTOR 2 2 5R2.54 0 1
REFLECTOR 3 2 5R0 3 4
REFLECTOR 3 6 5R0 3.24 1
END GEOM
READ BIAS ID=400 2 6 END BIAS
READ ARRAY NUX=2 NUY=2 NUZ=2 END ARRAY
END DATA
END
    
```

Table A.5 (continued)

```

CAS80
=CSAS25
UO2(NO3)2 415 G U/L
27GROUPNDF4 MULTIREGION
SOLNUO2(NO3)2 1 415 0 1 293 92235 92.6 92238 7.4 END
PLEXIGLASS 2 1 END
PARAFFIN 3 1 END
END COMP
CYLINDRICAL END
1 9.52 ONEEXTERMOD 2 10.16 NOEXTERMOD END ZONE
UO2(NO3)2 415 G U/L 2X2X2 ARRAY 15.24 CM PAR. BOT., 4.45 CM PLEX.
READ PARAM NPG=600 FDN=YES NUB=YES END PARAM
READ GEOM
CYLINDER 1 1 9.52 17.5609 0.
CYLINDER 0 1 9.52 17.77 0.
CYLINDER 2 1 10.16 18.41 -.64
CUBOID 0 1 4P13.855 22.105 -4.335
CORE 0 1 3R0.
REFLECTOR 2 2 5R3.0 0 1
REFLECTOR 2 3 5R1.45 0 1
REFLECTOR 3 2 5R0 3 4
REFLECTOR 3 6 5R0 3.24 1
END GEOM
READ BIAS ID=400 2 6 END BIAS
READ ARRAY NUX=2 NUY=2 NUZ=2 END ARRAY
END DATA
END
    
```

```

CAS81
=CSAS25
UO2(NO3)2 415 G U/L
27GROUPNDF4 MULTIREGION
SOLNUO2(NO3)2 1 415 0 1 293 92235 92.6 92238 7.4 END
PLEXIGLASS 2 1 END
PARAFFIN 3 1 END
END COMP
CYLINDRICAL END
1 9.52 ONEEXTERMOD 2 10.16 NOEXTERMOD END ZONE
UO2(NO3)2 415 G U/L 2X2X2 ARRAY 15.24 CM PAR. BOT., 6.35 CM PLEX.
READ PARAM NPG=600 FDN=YES NUB=YES END PARAM
READ GEOM
CYLINDER 1 1 9.52 17.5609 0.
CYLINDER 0 1 9.52 17.77 0.
CYLINDER 2 1 10.16 18.41 -.64
CUBOID 0 1 4P14.48 22.73 -4.96
CORE 0 1 3R0.
REFLECTOR 2 2 5R3.0 0 1
REFLECTOR 2 3 5R3.35 0 1
REFLECTOR 3 2 5R0 3 4
REFLECTOR 3 6 5R0 3.24 1
END GEOM
READ BIAS ID=400 2 6 END BIAS
READ ARRAY NUX=2 NUY=2 NUZ=2 END ARRAY
END DATA
END
    
```

```

CAS82
=CSAS25
UO2(NO3)2 415 G U/L
27GROUPNDF4 MULTIREGION
SOLNUO2(NO3)2 1 415 0 1 293 92235 92.6 92238 7.4 END
PLEXIGLASS 2 1 END
PARAFFIN 3 1 END
END COMP
CYLINDRICAL END
1 9.52 ONEEXTERMOD 2 10.16 NOEXTERMOD END ZONE
UO2(NO3)2 415 G U/L 2X2X2 ARRAY 15.24 CM PAR. BOT., 1.27 CM PAR.
READ PARAM NPG=600 FDN=YES NUB=YES END PARAM
READ GEOM
CYLINDER 1 1 9.52 17.5609 0.
CYLINDER 0 1 9.52 17.77 0.
CYLINDER 2 1 10.16 18.41 -.64
CUBOID 0 1 4P12.09 20.34 -2.57
CORE 0 1 3R0.
REFLECTOR 3 2 5R1.27 0 1
REFLECTOR 3 2 5R0 3 4
REFLECTOR 3 6 5R0 3.24 1
END GEOM
READ BIAS ID=400 2 6 END BIAS
READ ARRAY NUX=2 NUY=2 NUZ=2 END ARRAY
END DATA
END
    
```

```

CAS83
=CSAS25
UO2(NO3)2 415 G U/L
27GROUPNDF4 MULTIREGION
SOLNUO2(NO3)2 1 415 0 1 293 92235 92.6 92238 7.4 END
PLEXIGLASS 2 1 END
PARAFFIN 3 1 END
END COMP
CYLINDRICAL END
1 9.52 ONEEXTERMOD 2 10.16 NOEXTERMOD END ZONE
UO2(NO3)2 415 G U/L 2X2X2 ARRAY 15.24 CM PAR. BOT., 3.81 CM PAR.
READ PARAM NPG=600 FDN=YES NUB=YES END PARAM
READ GEOM
CYLINDER 1 1 9.52 17.5609 0.
CYLINDER 0 1 9.52 17.77 0.
CYLINDER 2 1 10.16 18.41 -.64
CUBOID 0 1 4P13.79 22.04 -4.27
CORE 0 1 3R0.
REFLECTOR 3 2 5R3.81 0 1
REFLECTOR 3 2 5R0 3 4
REFLECTOR 3 6 5R0 3.24 1
END GEOM
READ BIAS ID=400 2 6 END BIAS
READ ARRAY NUX=2 NUY=2 NUZ=2 END ARRAY
END DATA
END
    
```

Table A.5 (continued)

```

CAS84
=CSAS25
UO2(NO3)2 415 G U/L
27GROUPNDF4 MULTIREGION
SOLNUO2(NO3)2 1 415 0 1 293 92235 92.6 92238 7.4 END
PLEXIGLASS 2 1 END
PARAFFIN 3 1 END
END COMP
CYLINDRICAL END
1 9.52 ONEEXTERMOD 2 10.16 NOEXTERMOD END ZONE
UO2(NO3)2 415 G U/L 2X2X2 ARRAY 15.24 CM PAR. BOT., 7.62 CM PAR.
READ PARAM NPG=600 FDN=YES NUB=YES END PARAM
READ GEOM
CYLINDER 1 1 9.52 17.5609 0.
CYLINDER 0 1 9.52 17.77 0.
CYLINDER 2 1 10.16 18.41 -.64
CUBOID 0 1 4P14.515 22.765 -4.995
CORE 0 1 3R0.
REFLECTOR 3 2 5R3 0 2
REFLECTOR 3 4 5R1.62 0 1
REFLECTOR 3 2 5R0 3 4
REFLECTOR 3 6 5R0 3.24 1
END GEOM
READ BIAS ID=400 2 6 END BIAS
READ ARRAY NUX=2 NUY=2 NUZ=2 END ARRAY
END DATA
END
    
```

```

CAS85
=CSAS25
UO2(NO3)2 415 G U/L
27GROUPNDF4 MULTIREGION
SOLNUO2(NO3)2 1 415 0 1 293 92235 92.6 92238 7.4 END
PLEXIGLASS 2 1 END
PARAFFIN 3 1 END
END COMP
CYLINDRICAL END
1 9.52 ONEEXTERMOD 2 10.16 NOEXTERMOD END ZONE
UO2(NO3)2 415 G U/L 2X2X2 ARRAY 1.27 CM PLEXIGLASS REFL.
READ PARAM NPG=600 FDN=YES NUB=YES END PARAM
READ GEOM
CYLINDER 1 1 9.52 17.5609 0.
CYLINDER 0 1 9.52 17.77 0.
CYLINDER 2 1 10.16 18.41 -.64
CUBOID 0 1 4P11.66 19.91 -2.14
CORE 0 1 3R0.
REFLECTOR 2 2 6R1.27 1
END GEOM
READ BIAS ID=400 2 6 END BIAS
READ ARRAY NUX=2 NUY=2 NUZ=2 END ARRAY
END DATA
END
    
```

```

CAS86
=CSAS25
UO2(NO3)2 415 G U/L
27GROUPNDF4 MULTIREGION
SOLNUO2(NO3)2 1 415 0 1 293 92235 92.6 92238 7.4 END
PLEXIGLASS 2 1 END
PARAFFIN 3 1 END
END COMP
CYLINDRICAL END
1 9.52 ONEEXTERMOD 2 10.16 NOEXTERMOD END ZONE
UO2(NO3)2 415 G U/L 2X2X2 ARRAY 1.27 CM PARAFFIN REFL.
READ PARAM NPG=600 FDN=YES NUB=YES END PARAM
READ GEOM
CYLINDER 1 1 9.52 17.5609 0.
CYLINDER 0 1 9.52 17.77 0.
CYLINDER 2 1 10.16 18.41 -.64
CUBOID 0 1 4P11.80 20.05 -2.28
CORE 0 1 3R0.
REFLECTOR 3 2 6R1.27 1
END GEOM
READ BIAS ID=400 2 6 END BIAS
READ ARRAY NUX=2 NUY=2 NUZ=2 END ARRAY
END DATA
END
    
```

```

CAS87
=CSAS25
UO2(NO3)2 415 G U/L
27GROUPNDF4 MULTIREGION
U-235 1 0 9.846-4 END
U-238 1 0 7.769-5 END
H 1 0 5.809-2 END
N 1 0 2.131-3 END
O 1 0 3.756-2 END
PLEXIGLASS 2 1 END
PARAFFIN 3 1 END
END COMP
CYLINDRICAL END
1 9.52 ONEEXTERMOD 2 10.16 NOEXTERMOD END ZONE
UO2(NO3)2 415 G U/L 2X2X2 ARRAY 15.24 CM PARAFFIN REFL.
READ PARAM NPG=600 FDN=YES NUB=YES END PARAM
READ GEOM
CYLINDER 1 1 9.52 17.5609 0.
CYLINDER 0 1 9.52 17.77 0.
CYLINDER 2 1 10.16 18.41 -.64
CUBOID 0 1 4P14.655 22.905 -5.135
CORE 0 1 3R0.
REFLECTOR 3 2 6R3 4
REFLECTOR 3 6 6R3.24 1
END GEOM
READ BIAS ID=400 2 6 END BIAS
READ ARRAY NUX=2 NUY=2 NUZ=2 END ARRAY
END DATA
END
    
```

Table A.5 (continued)

```

CAS88
=CSAS25
UO2(NO3)2 415 G U/L
27GROUPNDF4 MULTIREGION
SOLNUO2(NO3)2 1 415 0 1 293 92235 92.6 92238 7.4 END
PLEXIGLASS 2 1 END
PARAFFIN 3 1 END
END COMP
CYLINDRICAL END
1 9.52 ONEEXTERMOD 2 10.16 NOEXTERMOD END ZONE
UO2(NO3)2 415 G U/L 2X2X2 ARRAY 3.81 CM PARAFFIN REFL.
READ PARAM NPG=600 FDN=YES NUB=YES END PARAM
READ GEOM
CYLINDER 1 1 9.52 17.5609 0.
CYLINDER 0 1 9.52 17.77 0.
CYLINDER 2 1 10.16 18.41 -.64
CUBOID 0 1 4P13.615 21.865 -4.095
CORE 0 1 3R0.
REFLECTOR 3 2 6R3.81 1
END GEOM
READ BIAS ID=400 2 6 END BIAS
READ ARRAY NUX=2 NUY=2 NUZ=2 END ARRAY
END DATA
END

```

```

CAS89
=CSAS25
UO2(NO3)2 415 G U/L
27GROUPNDF4 MULTIREGION
SOLNUO2(NO3)2 1 415 0 1 293 92235 92.6 92238 7.4 END
PLEXIGLASS 2 1 END
PARAFFIN 3 1 END
END COMP
CYLINDRICAL END
1 9.52 ONEEXTERMOD 2 10.16 NOEXTERMOD END ZONE
UO2(NO3)2 415 G U/L 2X2X2 ARRAY 7.62 CM PARAFFIN REFL.
READ PARAM NPG=600 FDN=YES NUB=YES END PARAM
READ GEOM
CYLINDER 1 1 9.52 17.5609 0.
CYLINDER 0 1 9.52 17.77 0.
CYLINDER 2 1 10.16 18.41 -.64
CUBOID 0 1 4P14.40 22.65 -4.88
CORE 0 1 3R0.
REFLECTOR 3 2 6R3 2
REFLECTOR 3 4 6R1.62 1
END GEOM
READ BIAS ID=400 2 6 END BIAS
READ ARRAY NUX=2 NUY=2 NUZ=2 END ARRAY
END DATA
END

```

```

CAS90
=CSAS25
UO2(NO3)2 415 G U/L
27GROUPNDF4 MULTIREGION
SOLNUO2(NO3)2 1 415 0 1 293 92235 92.6 92238 7.4 END
PLEXIGLASS 2 1 END
ARBMWOOD .640525 3 0 0 0 6012 44.435 1001 6.2639 8016 49.301 3 END
CARBONSTEEL 4 END
REG-CONCRETE 5 END
SOLNUO2(NO3)2 6 279 0 1 293 92235 92.6 92238 7.4 END
END COMP
CYLINDRICAL END
1 9.52 ONEEXTERMOD 2 10.16 NOEXTERMOD END ZONE
UO2(NO3)2 415 G U/L 3X3X3 ARRAY UNREFL. 279 G U/L 5 CENT. UNITS WALLS, FLOOR, &
READ PARAM PLT=NO NPG=600 FDN=YES NUB=YES END PARAM
READ GEOM
UNIT 1
CYLINDER 1 1 9.52 17.5609 0.
CYLINDER 0 1 9.52 17.77 0.
CYLINDER 2 1 10.16 18.41 -.64
CUBOID 0 1 4P13.365 21.615 -3.845
UNIT 4
CYLINDER 6 1 9.52 17.5609 0.
CYLINDER 0 1 9.52 17.77 0.
CYLINDER 2 1 10.16 18.41 -.64
CUBOID 0 1 4P13.365 21.615 -3.845
UNIT 2
ARRAY 1 2R-40.095 0.
CUBOID 0 1 4P200. 250. -50.
UNIT 3
CYLINDER 0 1 142.8 224. -48.
CYLINDER 4 1 144.8 224. -50.
CUBOID 0 1 218.1 -181.9 215. -185. 250. -50.
ARRAY 2 3R0.
REFLECTOR 0 1 57.4 57. 260. 559.2 400. 0. 1
REFLECTOR 2 1 5R0 .32 1
REFLECTOR 3 1 5R0 1.27 1
REFLECTOR 4 1 5R0 .64 1
REFLECTOR 0 1 5R0 365 1
REFLECTOR 5 2 6R3 10
REFLECTOR 5 12 0 3 4R0 10
END GEOM
READ START XSM=138 XSP=262 YSM=138 YSP=262 ZSM=50 ZSP=169 END START
READ BIAS ID=301 2 21 END BIAS
READ ARRAY ARA=1 NUX=3 NUY=3 NUZ=3 FILL 10R1 4 1 3R4 1 4 10R1 END FILL
ARA=2 NUX=2 NUY=1 NUZ=1 FILL 2 3 END FILL END ARRAY
READ PLOT
XUL=113.2 YUL=286.8 ZUL=60. XLR=286.8 YLR=113.2 ZLR=60.
UAX=1 VDN=-1 NAX=125 END
XUL=437.1 YUL=329.8 ZUL=60. XLR=726.7 YLR=40.2 ZLR=60. END
END PLOT
END DATA
END

```

Table A.5 (continued)

```

CAS91
=CSAS25
UO2(NO3)2 63.3 G U/L
27GROUPNDF4 MULTIREGION
SOLNUO2(NO3)2 1 63.3 0 1 293 92235 92.6 92238 7.4 END
PLEXIGLASS 2 1 END
ARBMWOOD .640525 3 0 0 0 6012 44.435 1001 6.2639 8016 49.301 3 END
CARBONSTEEL 4 END
REG-CONCRETE 5 END
END COMP
CYLINDRICAL END
1 9.52 ONEEXTERMOD 2 10.16 NOEXTERMOD END ZONE
UO2(NO3)2 63.3 G U/L 3X3X3 ARRAY UNREPL. WALLS, FLOOR, & TANK
READ PARAM NPG=600 FDN=YES NUB=YES PLT=NO END PARAM
READ GEOM
UNIT 1
CYLINDER 1 1 9.52 17.5609 0.
CYLINDER 0 1 9.52 17.77 0.
CYLINDER 2 1 10.16 18.41 -.64
CUBOID 0 1 4P11.365 19.615 -1.845
UNIT 2
ARRAY 1 2R-34.095 0.
CUBOID 0 1 4P200. 250. -50.
UNIT 3
CYLINDER 0 1 142.8 224. -48.
CYLINDER 4 1 144.8 224. -50.
CUBOID 0 1 218.1 -181.9 215. -185. 250. -50.
ARRAY 2 3R0.
REFLECTOR 0 1 57.4 57. 260. 559.2 400. 0. 1
REFLECTOR 2 1 5R0 .32 1
REFLECTOR 3 1 5R0 1.27 1
REFLECTOR 4 1 5R0 .64 1
REFLECTOR 0 1 5R0 365 1
REFLECTOR 5 2 6R3 10
REFLECTOR 5 12 0 3 4R0 10
END GEOM
READ START XSM=165 XSP=234 YSM=165 YSP=234 ZSM=50 ZSP=115 END START
READ BIAS ID=301 2 21 END BIAS
READ ARRAY ARA=1 NUX=3 NUY=3 NUZ=3 FILL F1 END FILL
ARA=2 NUX=2 NUY=1 NUZ=1 FILL 2 3 END FILL END ARRAY
READ PLOT
XUL=113.2 YUL=286.8 ZUL=60. XLR=286.8 YLR=113.2 ZLR=60.
UAX=1 VDN=-1 NAX=125 END
XUL=437.1 YUL=329.8 ZUL=60. XLR=726.7 YLR=40.2 ZLR=60. END
END PLOT
END DATA
END

```

Table A.6. Table 6 input data

```

CAS01
=CSAS25
ETA EXPERIMENTS EXP # 1
27GROUPNDF4 INFHOMMEDIUM
U-233 1 0 0.0 END
U-234 1 0 0.00538-4 END
U-235 1 0 0.48006-4 END
U-236 1 0 0.00138-4 END
U-238 1 0 0.02807-4 END
N 1 0 1.869-4 END
H 1 0 0.066228 END
O 1 0 0.033736 END
B-10 1 0 0.0 END
B-11 1 0 0.0 END
TH-232 1 0 0.0 END
AL 2 1 END
SS316 3 1 END
CARBONSTEEL 4 1 END
END COMP
ETA EXPERIMENTS # 1
READ PARAM NPG=600 FDN=YES NUB=YES TME=59 END PARAM
READ GEOM
SPHERE 1 1 34.5948 SPHERE 2 1 34.9148 CUBOID 0 1 6P34.9148
END GEOM READ START NST=1 END START
END DATA
END
    
```

```

CAS02
=CSAS25
ETA EXPERIMENTS EXP # 2
27GROUPNDF4 INFHOMMEDIUM
U-233 1 0 0.0 END
U-234 1 0 0.00631-4 END
U-235 1 0 0.56206-4 END
U-236 1 0 0.00163-4 END
U-238 1 0 0.03281-4 END
N 1 0 2.129-4 END
H 1 0 0.066148 END
O 1 0 0.033800 END
B-10 1 0 0.01029-4 END
B-11 1 0 0.04166-4 END
TH-232 1 0 0.0 END
AL 2 1 END
SS316 3 1 END
CARBONSTEEL 4 1 END
END COMP
ETA EXPERIMENTS # 2
READ PARAM NPG=600 FDN=YES NUB=YES TME=59 END PARAM
READ GEOM
SPHERE 1 1 34.5948 SPHERE 2 1 34.9148 CUBOID 0 1 6P34.9148
END GEOM READ START NST=1 END START
END DATA
END
    
```

```

CAS03
=CSAS25
ETA EXPERIMENTS EXP # 3
27GROUPNDF4 INFHOMMEDIUM
U-233 1 0 0.0 END
U-234 1 0 0.00716-4 END
U-235 1 0 0.63944-4 END
U-236 1 0 0.00184-4 END
U-238 1 0 0.03734-4 END
N 1 0 2.392-4 END
H 1 0 0.066070 END
O 1 0 0.033865 END
B-10 1 0 0.02057-4 END
B-11 1 0 0.08332-4 END
TH-232 1 0 0.0 END
AL 2 1 END
SS316 3 1 END
CARBONSTEEL 4 1 END
END COMP
ETA EXPERIMENTS # 3
READ PARAM NPG=600 FDN=YES NUB=YES TME=59 END PARAM
READ GEOM
SPHERE 1 1 34.5948 SPHERE 2 1 34.9148 CUBOID 0 1 6P34.9148
END GEOM READ START NST=1 END START
END DATA
END
    
```

```

CAS04
=CSAS25
ETA EXPERIMENTS EXP # 4
27GROUPNDF4 INFHOMMEDIUM
U-233 1 0 0.0 END
U-234 1 0 0.00762-4 END
U-235 1 0 0.67959-4 END
U-236 1 0 0.00197-4 END
U-238 1 0 0.03967-4 END
N 1 0 2.548-4 END
H 1 0 0.066028 END
O 1 0 0.034028 END
B-10 1 0 0.02532-4 END
B-11 1 0 0.10255-4 END
TH-232 1 0 0.0 END
AL 2 1 END
SS316 3 1 END
CARBONSTEEL 4 1 END
END COMP
ETA EXPERIMENTS # 4
READ PARAM NPG=600 FDN=YES NUB=YES TME=59 END PARAM
READ GEOM
SPHERE 1 1 34.5948 SPHERE 2 1 34.9148 CUBOID 0 1 6P34.9148
END GEOM READ START NST=1 END START
END DATA
END
    
```

Table A.6 (continued)

```

CAS05
=CSAS25
ETA EXPERIMENTS EXP # 5
27GROUPNDF4 INFHOMMEDIUM
U-233 1 0 0.43284-4 END
U-234 1 0 0.00716-4 END
U-235 1 0 0.00018-4 END
U-236 1 0 0.0 END
U-238 1 0 0.00281-4 END
N 1 0 1.178-4 END
H 1 0 0.066360 END
O 1 0 0.033608 END
B-10 1 0 0.0 END
B-11 1 0 0.0 END
TH-232 1 0 0.000196-3 END
AL 2 1 END
SS316 3 1 END
CARBONSTEEL 4 1 END
END COMP
ETA EXPERIMENTS # 5
READ PARAM NPG=600 FDN=YES NUB=YES TME=59 END PARAM
READ GEOM
SPHERE 1 1 34.5948 SPHERE 2 1 34.9148 CUBOID 0 1 6P34.9148
END GEOM READ START NST=1 END START
END DATA
END
  
```

```

CAS06
=CSAS25
ETA EXPERIMENTS EXP # 6
27GROUPNDF4 INFHOMMEDIUM
U-233 1 0 0.45120-4 END
U-234 1 0 0.00744-4 END
U-235 1 0 0.00018-4 END
U-236 1 0 0.0 END
U-238 1 0 0.00291-4 END
N 1 0 1.224-4 END
H 1 0 0.066345 END
O 1 0 0.033621 END
B-10 1 0 0.00263-4 END
B-11 1 0 0.01066-4 END
TH-232 1 0 0.000205-3 END
AL 2 1 END
SS316 3 1 END
CARBONSTEEL 4 1 END
END COMP
ETA EXPERIMENTS # 6
READ PARAM NPG=600 FDN=YES NUB=YES TME=59 END PARAM
READ GEOM
SPHERE 1 1 34.5948 SPHERE 2 1 34.9148 CUBOID 0 1 6P34.9148
END GEOM READ START NST=1 END START
END DATA
END
  
```

```

CAS07
=CSAS25
ETA EXPERIMENTS EXP # 7
27GROUPNDF4 INFHOMMEDIUM
U-233 1 0 0.46798-4 END
U-234 1 0 0.00772-4 END
U-235 1 0 0.00018-4 END
U-236 1 0 0.0 END
U-238 1 0 0.00301-4 END
N 1 0 1.274-4 END
H 1 0 0.066329 END
O 1 0 0.033634 END
B-10 1 0 0.00512-4 END
B-11 1 0 0.02075-4 END
TH-232 1 0 0.000213-3 END
AL 2 1 END
SS316 3 1 END
CARBONSTEEL 4 1 END
END COMP
ETA EXPERIMENTS # 7
READ PARAM NPG=600 FDN=YES NUB=YES TME=59 END PARAM
READ GEOM
SPHERE 1 1 34.5948 SPHERE 2 1 34.9148 CUBOID 0 1 6P34.9148
END GEOM READ START NST=1 END START
END DATA
END
  
```

```

CAS08
=CSAS25
ETA EXPERIMENTS EXP # 8
27GROUPNDF4 INFHOMMEDIUM
U-233 1 0 0.48455-4 END
U-234 1 0 0.00801-4 END
U-235 1 0 0.00021-4 END
U-236 1 0 0.0 END
U-238 1 0 0.00311-4 END
N 1 0 1.319-4 END
H 1 0 0.066315 END
O 1 0 0.033646 END
B-10 1 0 0.00758-4 END
B-11 1 0 0.03069-4 END
TH-232 1 0 0.000221-3 END
AL 2 1 END
SS316 3 1 END
CARBONSTEEL 4 1 END
END COMP
ETA EXPERIMENTS # 8
READ PARAM NPG=600 FDN=YES NUB=YES TME=59 END PARAM
READ GEOM
SPHERE 1 1 34.5948 SPHERE 2 1 34.9148 CUBOID 0 1 6P34.9148
END GEOM READ START NST=1 END START
END DATA
END
  
```

Table A.6 (continued)

```

CAS09
=CSAS25
ETA EXPERIMENTS EXP # 9
27GROUPNDF4 INFHOMMEDIUM
U-233 1 0 0.5066-4 END
U-234 1 0 0.00827-4 END
U-235 1 0 0.00021-4 END
U-236 1 0 0.0 END
U-238 1 0 0.00327-4 END
N 1 0 1.363-4 END
H 1 0 0.0663 END
O 1 0 0.033659 END
B-10 1 0 0.01005-4 END
B-11 1 0 0.04070-4 END
TH-232 1 0 0.000227-3 END
AL 2 1 END
SS316 3 1 END
CARBONSTEEL 4 1 END
END COMP
ETA EXPERIMENTS # 9
READ PARAM NPG=600 FDN=YES NUB=YES TME=59 END PARAM
READ GEOM
SPHERE 1 1 34.5948 SPHERE 2 1 34.9148 CUBOID 0 1 6P34.9148
END GEOM READ START NST=1 END START
END DATA
END
    
```

```

CAS10
=CSAS25
ETA EXPERIMENTS EXP # 10
27GROUPNDF4 INFHOMMEDIUM
U-233 1 0 0.0 END
U-234 1 0 0.00409-4 END
U-235 1 0 0.36185-4 END
U-236 1 0 0.00220-4 END
U-238 1 0 0.01985-4 END
N 1 0 1.116-4 END
H 1 0 0.066394 END
O 1 0 0.033592 END
B-10 1 0 0.0 END
B-11 1 0 0.0 END
TH-232 1 0 0.0 END
AL 2 1 END
SS316 3 1 END
CARBONSTEEL 4 1 END
END COMP
ETA EXPERIMENTS # 10
READ PARAM NPG=600 FDN=YES NUB=YES TME=59 END PARAM
READ GEOM
SPHERE 1 1 61.0108 SPHERE 2 1 61.7808 CUBOID 0 1 6P61.7808
END GEOM READ START NST=1 END START
END DATA
END
    
```

```

CAS11
=CSAS25
ETA EXPERIMENTS EXP # 11
27GROUPNDF4 INFHOMMEDIUM
U-233 1 0 0.33460-4 END
U-234 1 0 0.00525-4 END
U-235 1 0 0.00010-4 END
U-236 1 0 0.0 END
U-238 1 0 0.00256-4 END
N 1 0 0.753-4 END
H 1 0 0.066467 END
O 1 0 0.033525 END
B-10 1 0 0.0 END
B-11 1 0 0.0 END
TH-232 1 0 0.000148-3 END
AL 2 1 END
SS316 3 1 END
CARBONSTEEL 4 1 END
END COMP
ETA EXPERIMENTS # 11
READ PARAM NPG=600 FDN=YES NUB=YES TME=59 END PARAM
READ GEOM
SPHERE 1 1 61.0108 SPHERE 2 1 61.7808 CUBOID 0 1 6P61.7808
END GEOM READ START NST=1 END START
END DATA
END
    
```

```

CAS12
=CSAS25
ETA EXPERIMENTS EXP # 12
27GROUPNDF4 INFHOMMEDIUM
U-233 1 0 0.00000-4 END
U-234 1 0 0.00469-4 END
U-235 1 0 0.41364-4 END
U-236 1 0 0.00243-4 END
U-238 1 0 0.02271-4 END
N 1 0 1.27200-4 END
H 1 0 0.066345 END
O 1 0 0.033624 END
B-10 1 0 0.0 END
B-11 1 0 0.0 END
TH-232 1 0 0.000000-3 END
AL 2 1 END
SS316 3 1 END
CARBONSTEEL 4 1 END
END COMP
ETA EXPERIMENTS # 12
READ PARAM NPG=600 FDN=YES NUB=YES TME=59 END PARAM
READ GEOM CYLINDER 1 1 77.3684 45.1358 0.0
CYLINDER 0 1 77.3684 264.0 0.0
CYLINDER 3 1 77.4984 264.13 -0.13
CUBOID 0 1 4P77.4984 264.13 -0.13
END GEOM
READ START NST=1 END START
END DATA
END
    
```


Table A.6 (continued)

```

CAS13
=CSAS25
ETA EXPERIMENTS EXP # 13
27GROUPNDF4 INFHOMMEDIUM
U-233 1 0 0.00000-4 END
U-234 1 0 0.00451-4 END
U-235 1 0 0.40595-4 END
U-236 1 0 0.00222-4 END
U-238 1 0 0.02339-4 END
N 1 0 1.40900-4 END
H 1 0 0.066343 END
O 1 0 0.033655 END
B-10 1 0 0.0 END
B-11 1 0 0.0 END
TH-232 1 0 0.000000-3 END
AL 2 1 END
SS316 3 1 END
CARBONSTEEL 4 1 END
END COMP
ETA EXPERIMENTS # 13
READ PARAM NPG=600 FDN=YES NUB=YES TME=59 END PARAM
READ GEOM CYLINDER 1 1 77.3684 47.4472 0.0
CYLINDER 0 1 77.3684 264.0 0.0
CYLINDER 3 1 77.4984 264.13 -0.13
CUBOID 0 1 4P77.4984 264.13 -0.13
END GEOM
READ START NST=1 END START
END DATA
END
    
```

```

CAS14
=CSAS25
ETA EXPERIMENTS EXP # 14
27GROUPNDF4 INFHOMMEDIUM
U-233 1 0 0.00000-4 END
U-234 1 0 0.00409-4 END
U-235 1 0 0.36452-4 END
U-236 1 0 0.00209-4 END
U-238 1 0 0.02048-4 END
N 1 0 1.18500-4 END
H 1 0 0.066383 END
O 1 0 0.033605 END
B-10 1 0 0.0 END
B-11 1 0 0.0 END
TH-232 1 0 0.000000-3 END
AL 2 1 END
SS316 3 1 END
CARBONSTEEL 4 1 END
END COMP
ETA EXPERIMENTS # 14
READ PARAM NPG=600 FDN=YES NUB=YES TME=59 END PARAM
READ GEOM CYLINDER 1 1 77.3684 72.7456 0.0
CYLINDER 0 1 77.3684 264.0 0.0
CYLINDER 3 1 77.4984 264.13 -0.13
CUBOID 0 1 4P77.4984 264.13 -0.13
END GEOM
READ START NST=1 END START
END DATA
END
    
```

```

CAS15
=CSAS25
ETA EXPERIMENTS EXP # 15
27GROUPNDF4 INFHOMMEDIUM
U-233 1 0 0.00000-4 END
U-234 1 0 0.00397-4 END
U-235 1 0 0.34845-4 END
U-236 1 0 0.00194-4 END
U-238 1 0 0.01962-4 END
N 1 0 1.20800-4 END
H 1 0 0.066389 END
O 1 0 0.033609 END
B-10 1 0 0.0 END
B-11 1 0 0.0 END
TH-232 1 0 0.000000-3 END
AL 2 1 END
SS316 3 1 END
CARBONSTEEL 4 1 END
END COMP
ETA EXPERIMENTS # 15
READ PARAM NPG=600 FDN=YES NUB=YES TME=59 END PARAM
READ GEOM CYLINDER 1 1 77.3684 105.2068 0.0
CYLINDER 0 1 77.3684 264.0 0.0
CYLINDER 3 1 77.4984 264.13 -0.13
CUBOID 0 1 4P77.4984 264.13 -0.13
END GEOM
READ START NST=1 END START
END DATA
END
    
```

```

CAS16
=CSAS25
ETA EXPERIMENTS EXP # 16
27GROUPNDF4 INFHOMMEDIUM
U-233 1 0 0.00000-4 END
U-234 1 0 0.00384-4 END
U-235 1 0 0.33519-4 END
U-236 1 0 0.00186-4 END
U-238 1 0 0.01924-4 END
N 1 0 1.24400-4 END
H 1 0 0.066391 END
O 1 0 0.033615 END
B-10 1 0 0.0 END
B-11 1 0 0.0 END
TH-232 1 0 0.000000-3 END
AL 2 1 END
SS316 3 1 END
CARBONSTEEL 4 1 END
END COMP
ETA EXPERIMENTS # 16
READ PARAM NPG=600 FDN=YES NUB=YES TME=59 END PARAM
READ GEOM CYLINDER 1 1 77.3684 203.2762 0.0
CYLINDER 0 1 77.3684 264.0 0.0
CYLINDER 3 1 77.4984 264.13 -0.13
CUBOID 0 1 4P77.4984 264.13 -0.13
END GEOM
READ START NST=1 END START
END DATA
END
    
```

Table A.6 (continued)

```

CAS17
=CSAS25
ETA EXPERIMENTS EXP # 17
27GROUPNDF4 INFHOMMEDIUM
U-233 1 0 0.36517-4 END
U-234 1 0 0.00556-4 END
U-235 1 0 0.00000-4 END
U-236 1 0 0.00000-4 END
U-238 1 0 0.00410-4 END
N 1 0 0.82600-4 END
H 1 0 0.066439 END
O 1 0 0.033539 END
B-10 1 0 0.0 END
B-11 1 0 0.0 END
TH-232 1 0 0.000037-3 END
AL 2 1 END
SS316 3 1 END
CARBONSTEEL 4 1 END
END COMP
ETA EXPERIMENTS # 17
READ PARAM NPG=600 FDN=YES NUB=YES TME=59 END PARAM
READ GEOM CYLINDER 1 1 77.3684 49.5046 0.0
CYLINDER 0 1 77.3684 264.0 0.0
CYLINDER 3 1 77.4984 264.13 -0.13
CUBOID 0 1 4P77.4984 264.13 -0.13
END GEOM
READ START NST=1 END START
END DATA
END
    
```

```

CAS18
=CSAS25
ETA EXPERIMENTS EXP # 18
27GROUPNDF4 INFHOMMEDIUM
U-233 1 0 0.34978-4 END
U-234 1 0 0.00525-4 END
U-235 1 0 0.00000-4 END
U-236 1 0 0.00000-4 END
U-238 1 0 0.00395-4 END
N 1 0 0.84900-4 END
H 1 0 0.066444 END
O 1 0 0.033542 END
B-10 1 0 0.0 END
B-11 1 0 0.0 END
TH-232 1 0 0.000032-3 END
AL 2 1 END
SS316 3 1 END
CARBONSTEEL 4 1 END
END COMP
ETA EXPERIMENTS # 18
READ PARAM NPG=600 FDN=YES NUB=YES TME=59 END PARAM
READ GEOM CYLINDER 1 1 77.3684 59.2074 0.0
CYLINDER 0 1 77.3684 264.0 0.0
CYLINDER 3 1 77.4984 264.13 -0.13
CUBOID 0 1 4P77.4984 264.13 -0.13
END GEOM
READ START NST=1 END START
END DATA
END
    
```

```

CAS19
=CSAS25
ETA EXPERIMENTS EXP # 19
27GROUPNDF4 INFHOMMEDIUM
U-233 1 0 0.33292-4 END
U-234 1 0 0.00507-4 END
U-235 1 0 0.00000-4 END
U-236 1 0 0.00000-4 END
U-238 1 0 0.00375-4 END
N 1 0 0.80200-4 END
H 1 0 0.066459 END
O 1 0 0.033533 END
B-10 1 0 0.0 END
B-11 1 0 0.0 END
TH-232 1 0 0.000037-3 END
AL 2 1 END
SS316 3 1 END
CARBONSTEEL 4 1 END
END COMP
ETA EXPERIMENTS # 19
READ PARAM NPG=600 FDN=YES NUB=YES TME=59 END PARAM
READ GEOM CYLINDER 1 1 77.3684 77.6732 0.0
CYLINDER 0 1 77.3684 264.0 0.0
CYLINDER 3 1 77.4984 264.13 -0.13
CUBOID 0 1 4P77.4984 264.13 -0.13
END GEOM
READ START NST=1 END START
END DATA
END
    
```

```

CAS20
=CSAS25
ETA EXPERIMENTS EXP # 20
27GROUPNDF4 INFHOMMEDIUM
U-233 1 0 0.31567-4 END
U-234 1 0 0.00481-4 END
U-235 1 0 0.00000-4 END
U-236 1 0 0.00000-4 END
U-238 1 0 0.00354-4 END
N 1 0 0.79500-4 END
H 1 0 0.066470 END
O 1 0 0.033531 END
B-10 1 0 0.0 END
B-11 1 0 0.0 END
TH-232 1 0 0.000258-3 END
AL 2 1 END
SS316 3 1 END
CARBONSTEEL 4 1 END
END COMP
ETA EXPERIMENTS # 20
READ PARAM NPG=600 FDN=YES NUB=YES TME=59 END PARAM
READ GEOM CYLINDER 1 1 77.3684 138.9126 0.0
CYLINDER 0 1 77.3684 264.0 0.0
CYLINDER 3 1 77.4984 264.13 -0.13
CUBOID 0 1 4P77.4984 264.13 -0.13
END GEOM
READ START NST=1 END START
END DATA
END
    
```

Table A.6 (continued)

```

CAS21
=CSAS25
ETA EXPERIMENTS EXP # 21
27GROUPNDF4 INFHOMMEDIUM
U-233      1 0 0.00000-4 END
U-234      1 0 0.00397-4 END
U-235      1 0 0.33940-4 END
U-236      1 0 0.00240-4 END
U-238      1 0 0.01975-4 END
N          1 0 1.40700-4 END
H          1 0 0.066367 END
O          1 0 0.033645 END
B-10       1 0 0.0 END
B-11       1 0 0.0 END
TH-232     1 0 0.000000-3 END
AL         2 1 END
SS316      3 1 END
CARBONSTEEL 4 1 END
END COMP
ETA EXPERIMENTS # 21
READ PARAM NPG=600 FDN=YES NUB=YES TME=59 END PARAM
READ GEOM CYLINDER 1 1 136.7790 90.8812 0.0
CYLINDER 0 1 136.7790 274.0 0.0
CYLINDER 4 1 138.6840 275.905 -1.905
CUBOID 0 1 4P138.6840 275.905 -1.905
END GEOM
READ START NST=1 END START
END DATA
END

```

```

CAS22
=CSAS25
ETA EXPERIMENTS EXP # 22
27GROUPNDF4 INFHOMMEDIUM
U-233      1 0 0.00000-4 END
U-234      1 0 0.00381-4 END
U-235      1 0 0.33124-4 END
U-236      1 0 0.00232-4 END
U-238      1 0 0.01942-4 END
N          1 0 1.36700-4 END
H          1 0 0.066374 END
O          1 0 0.033634 END
B-10       1 0 0.0 END
B-11       1 0 0.0 END
TH-232     1 0 0.000000-3 END
AL         2 1 END
SS316      3 1 END
CARBONSTEEL 4 1 END
END COMP
ETA EXPERIMENTS # 22
READ PARAM NPG=600 FDN=YES NUB=YES TME=59 END PARAM
READ GEOM CYLINDER 1 1 136.7790 122.4280 0.0
CYLINDER 0 1 136.7790 274.0 0.0
CYLINDER 4 1 138.6840 275.905 -1.905
CUBOID 0 1 4P138.6840 275.905 -1.905
END GEOM
READ START NST=1 END START
END DATA
END

```

```

CAS23
=CSAS25
ETA EXPERIMENTS EXP # 23
27GROUPNDF4 INFHOMMEDIUM
U-233      1 0 0.00000-4 END
U-234      1 0 0.00368-4 END
U-235      1 0 0.32347-4 END
U-236      1 0 0.00220-4 END
U-238      1 0 0.01894-4 END
N          1 0 1.33800-4 END
H          1 0 0.066385 END
O          1 0 0.033631 END
B-10       1 0 0.0 END
B-11       1 0 0.0 END
TH-232     1 0 0.000000-3 END
AL         2 1 END
SS316      3 1 END
CARBONSTEEL 4 1 END
END COMP
ETA EXPERIMENTS # 23
READ PARAM NPG=600 FDN=YES NUB=YES TME=59 END PARAM
READ GEOM CYLINDER 1 1 136.7790 241.1222 0.0
CYLINDER 0 1 136.7790 274.0 0.0
CYLINDER 4 1 138.6840 275.905 -1.905
CUBOID 0 1 4P138.6840 275.905 -1.905
END GEOM
READ START NST=1 END START
END DATA
END

```

Appendix B

PLOT OF AVERAGE K_{eff} BY GENERATION SKIPPED FOR VALIDATION CASES

Plots of average k_{eff} by generation skipped for the validation cases appear in the same order as listed in Tables 1-6 of Sect. 1 of this report.

| | |
|-----------------------------|-------|
| Fig. B.1. Plots for Table 1 | B-2 |
| Fig. B.2. Plots for Table 2 | B-22 |
| Fig. B.3. Plots for Table 3 | B-28 |
| Fig. B.4. Plots for Table 4 | B-53 |
| Fig. B.5. Plots for Table 5 | B-75 |
| Fig. B.6. Plots for Table 6 | B-121 |

TABLE 1 (CAA01)
 LIBBY EXP. 4.89% RODS 30 CM LONG, .762CM DIAM, 1.3CM PITCH
 PLOT OF AVERAGE K-EFFECTIVE BY GENERATION SKIPPED. THE FINAL VALUE IS 0.9985

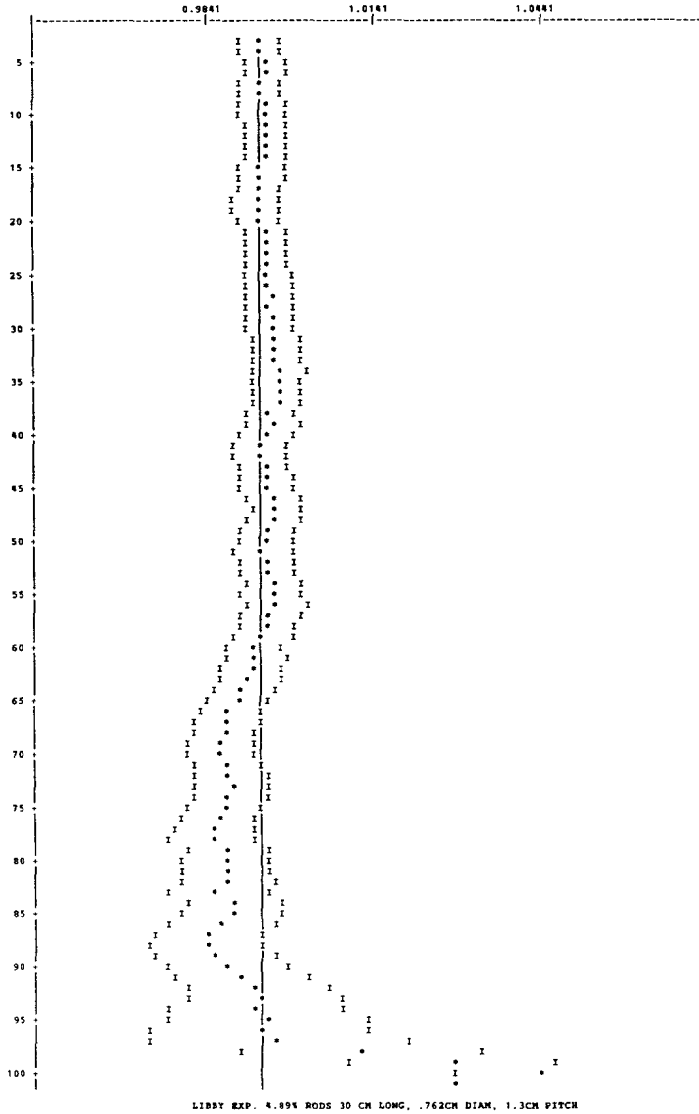


TABLE 1 (CAA02)
 LIBBY H2O REFL. CASE 4B
 PLOT OF AVERAGE K-EFFECTIVE BY GENERATION SKIPPED. THE FINAL VALUE IS 0.9912

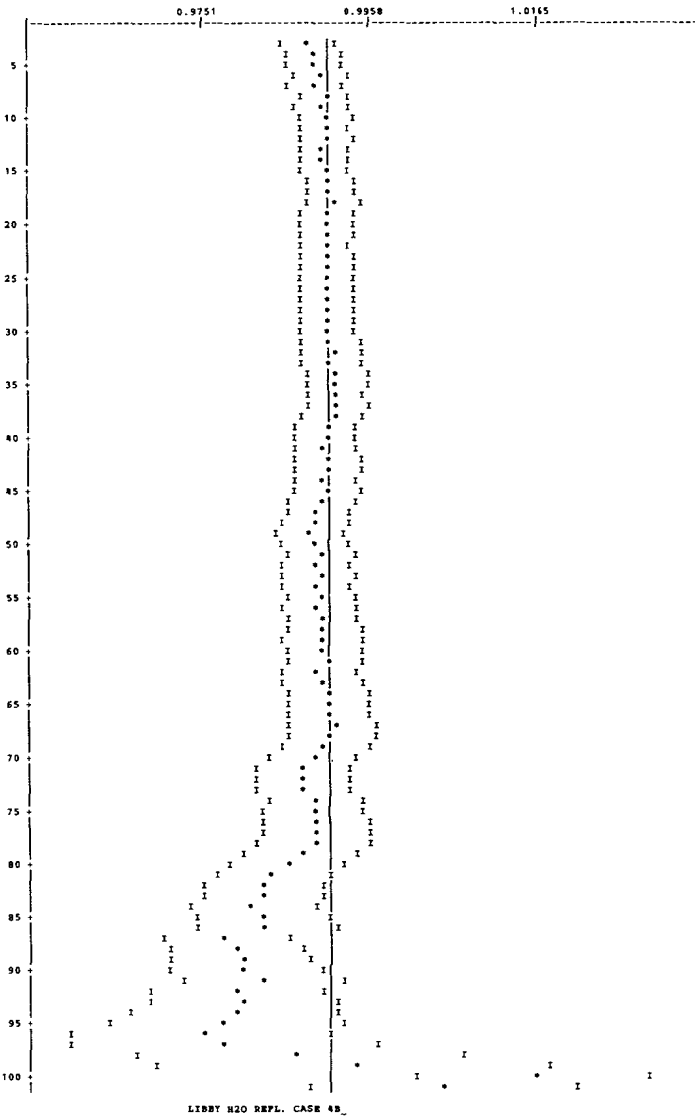


Fig. B.1. Plots for Table 1.

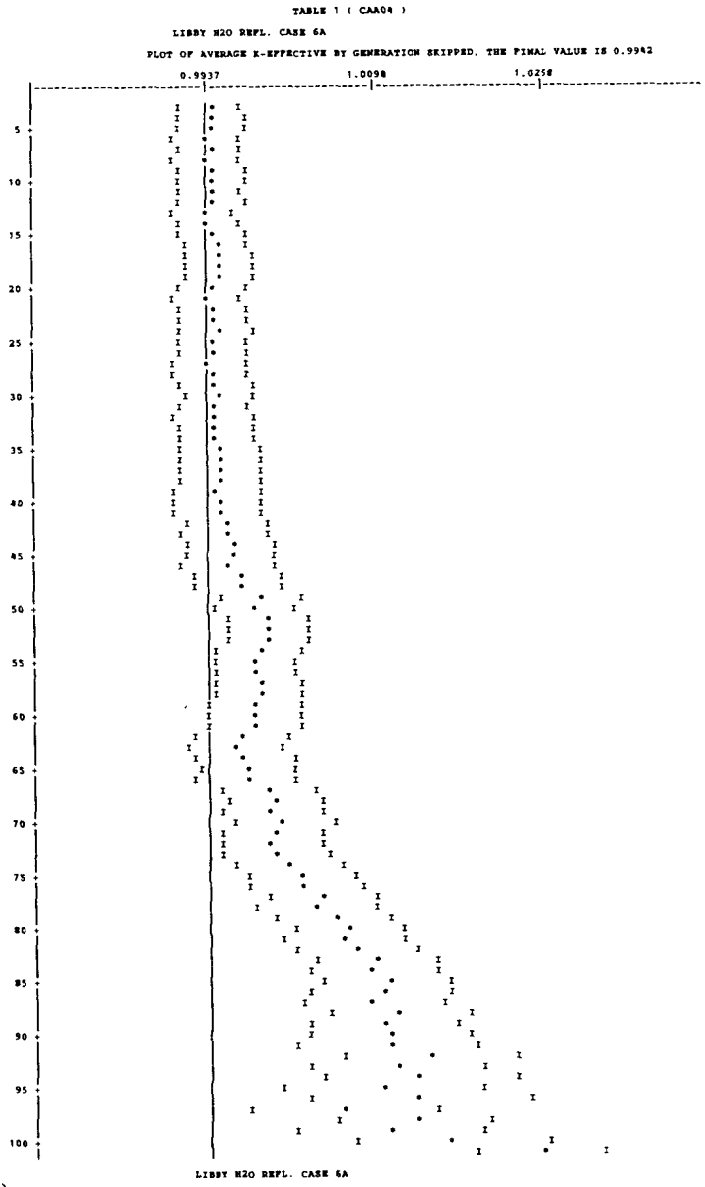
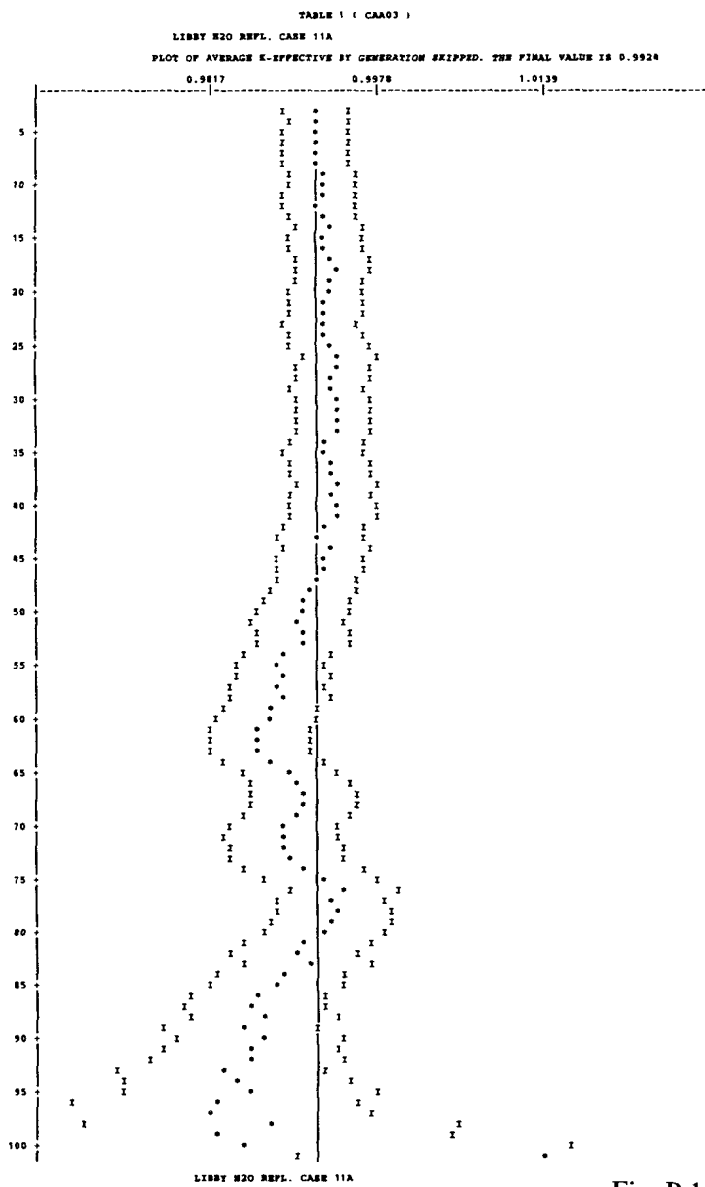


Fig. B.1 (continued)

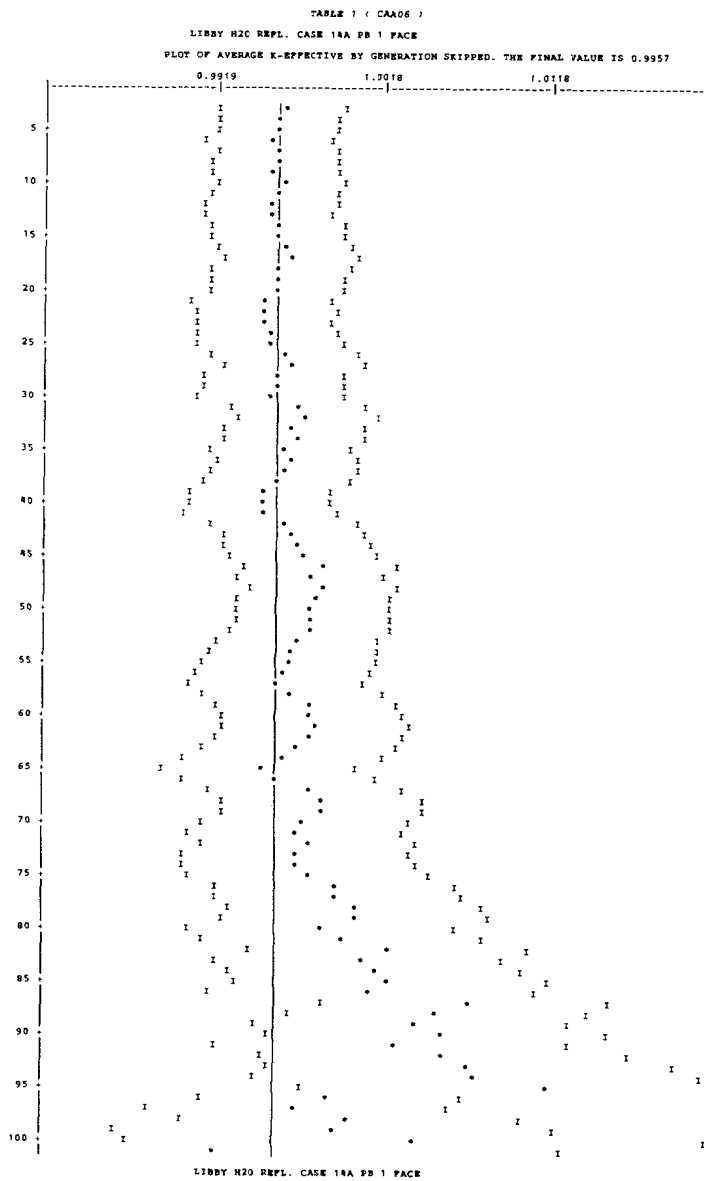
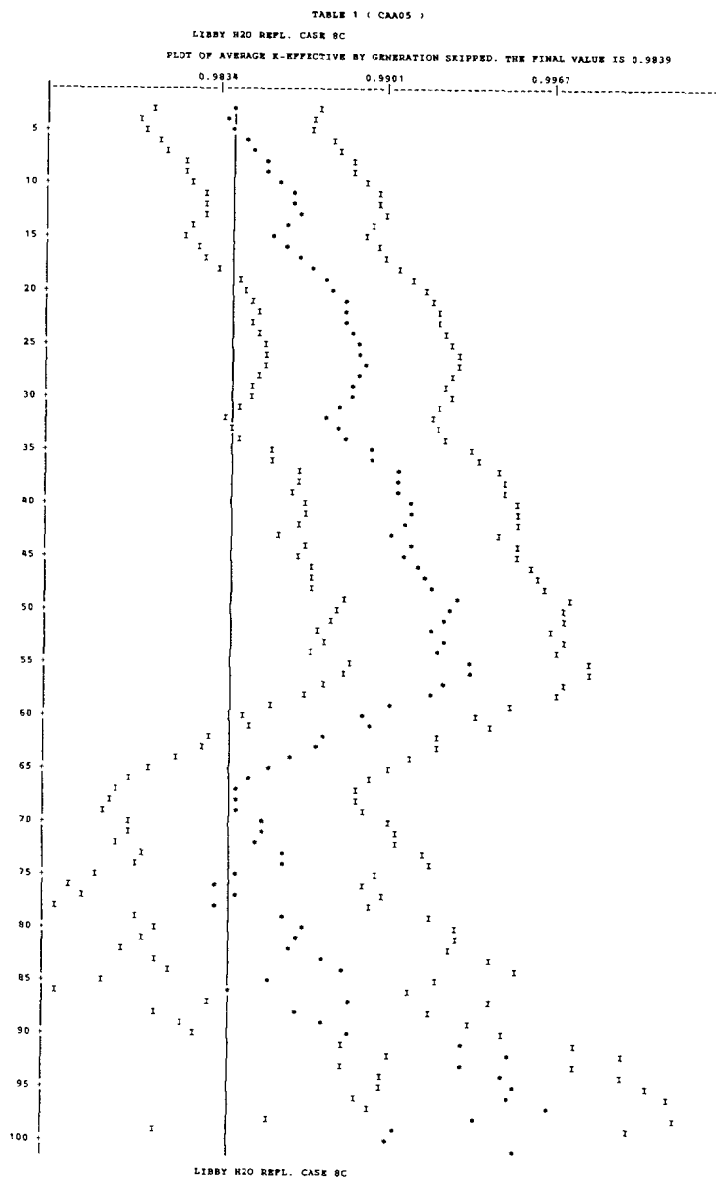


Fig. B.1 (continued)

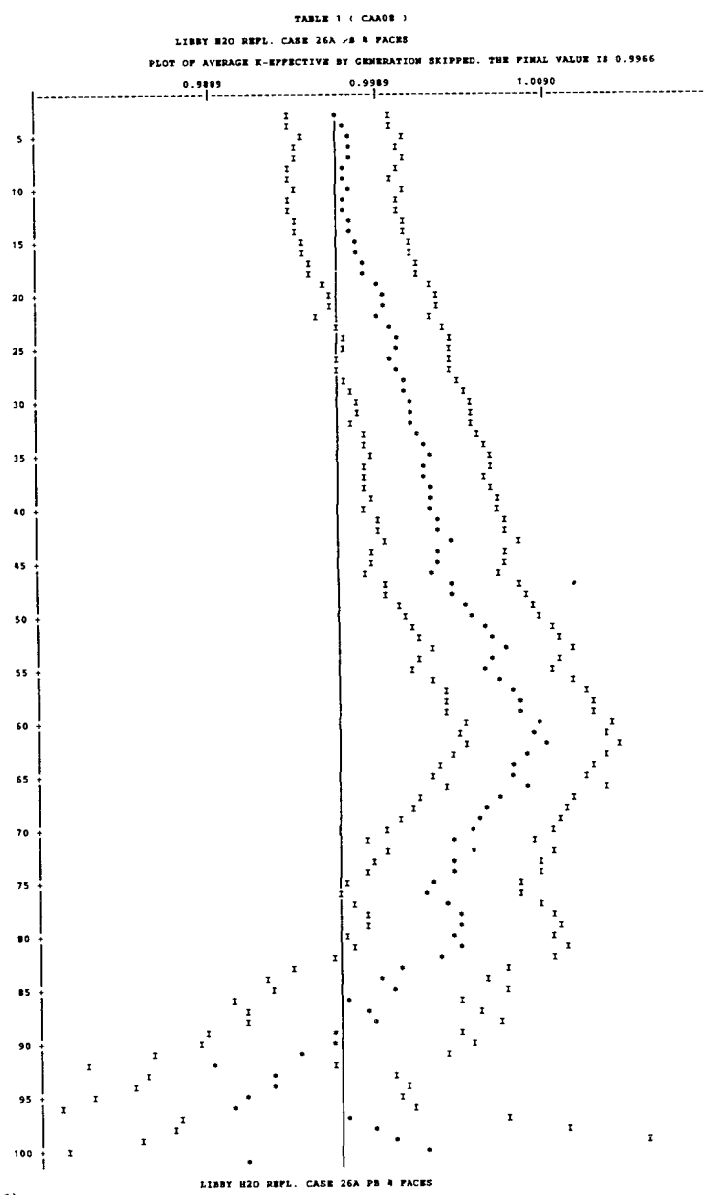
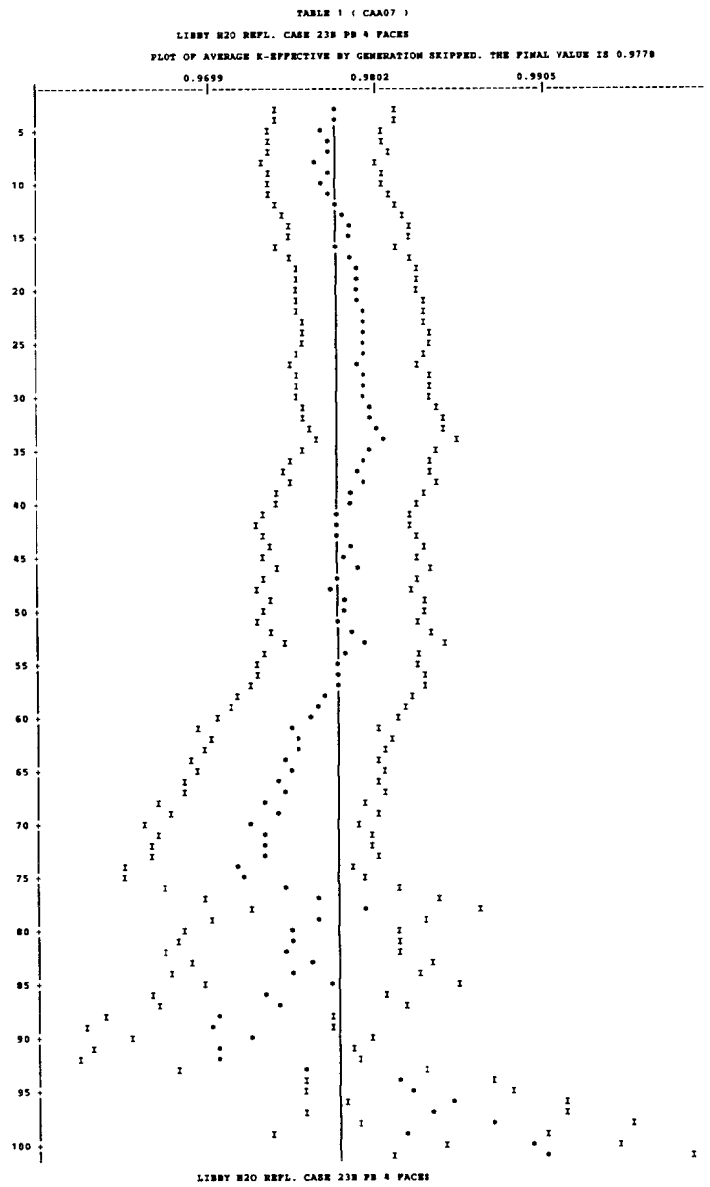


Fig. B.1 (continued)

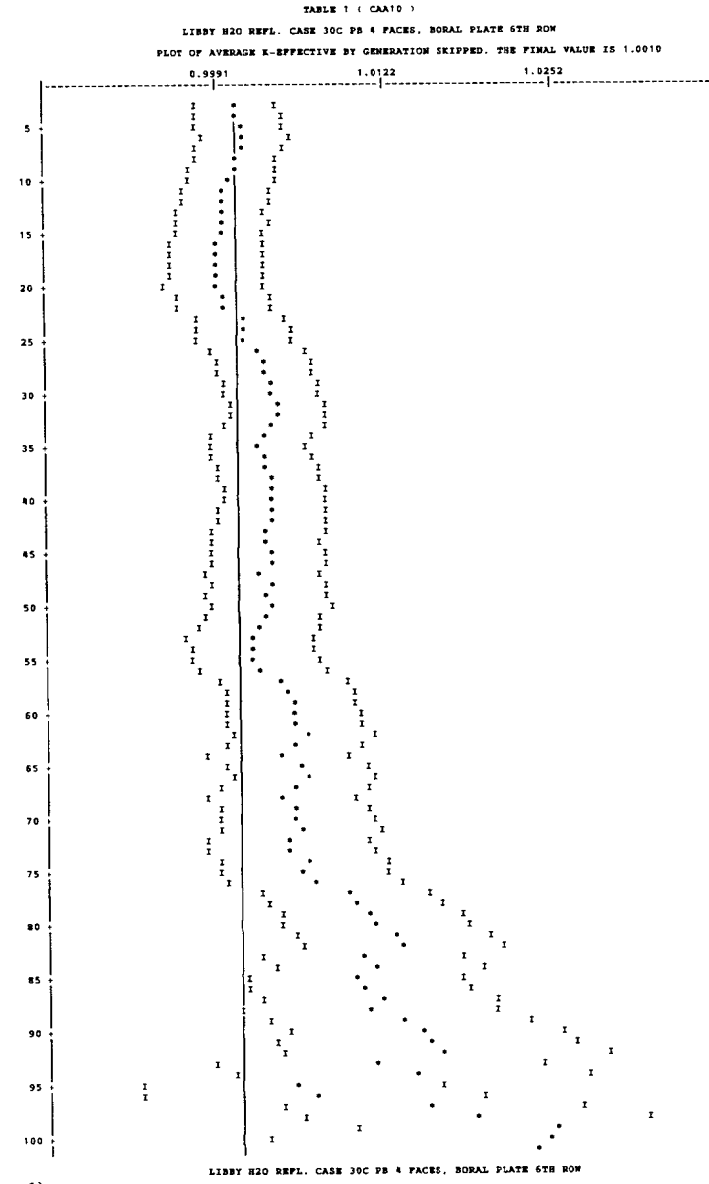
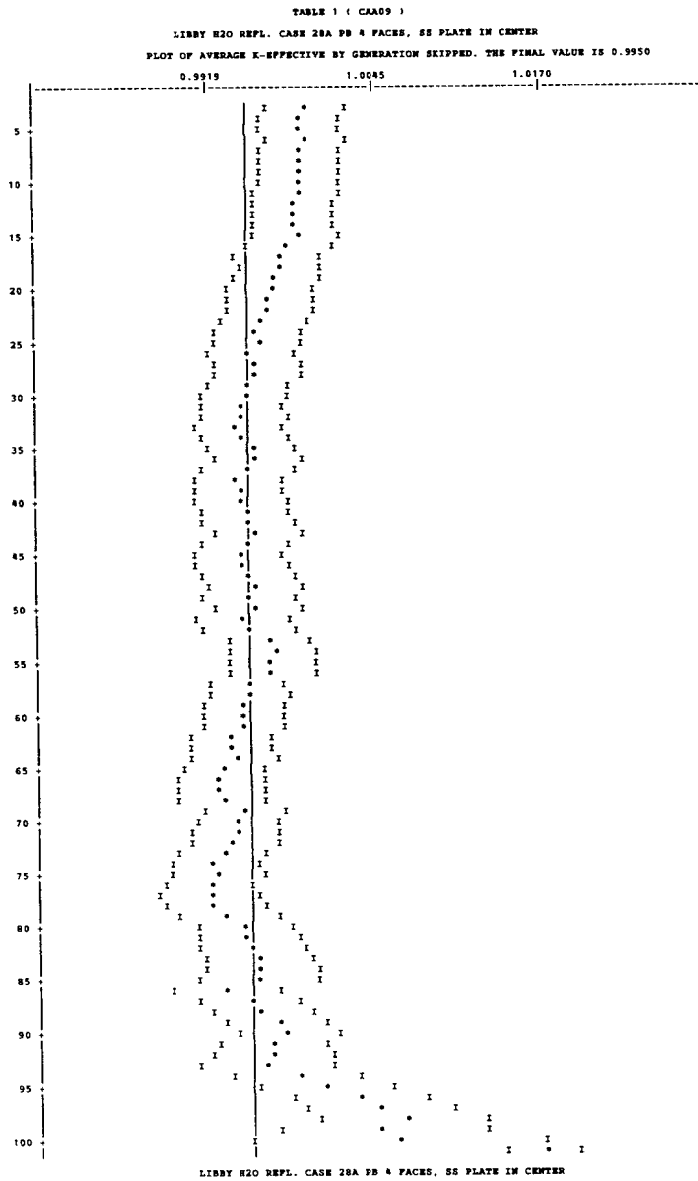


Fig. B.1 (continued)

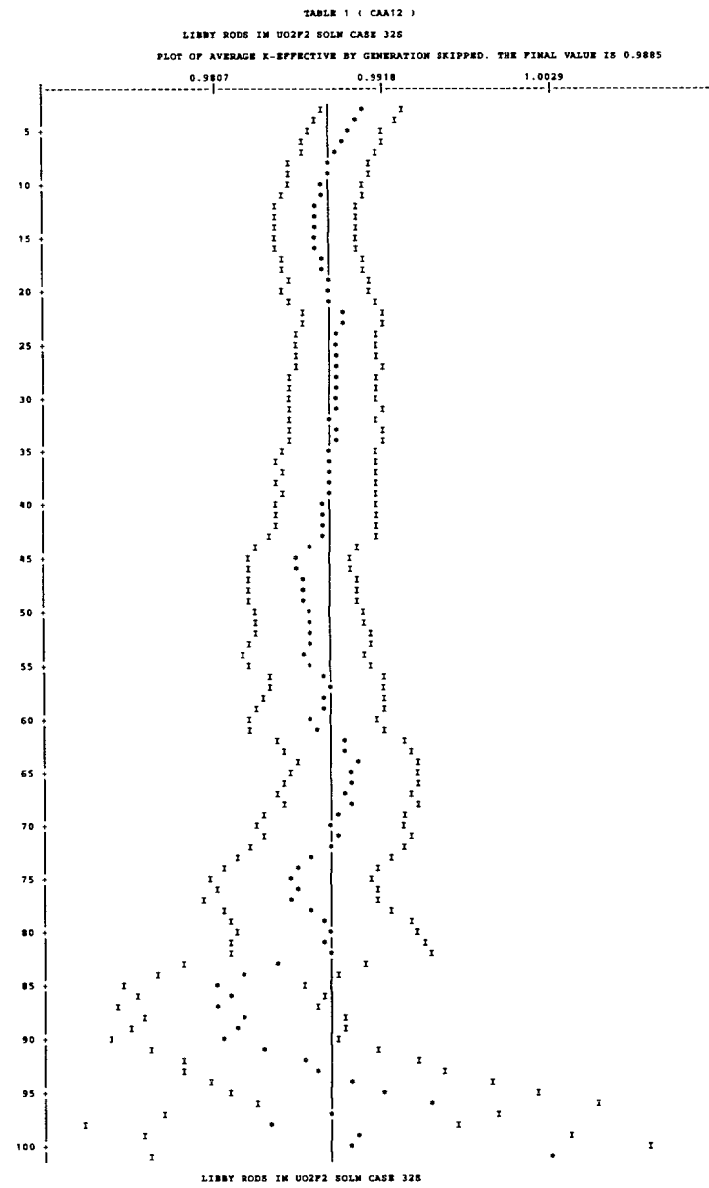
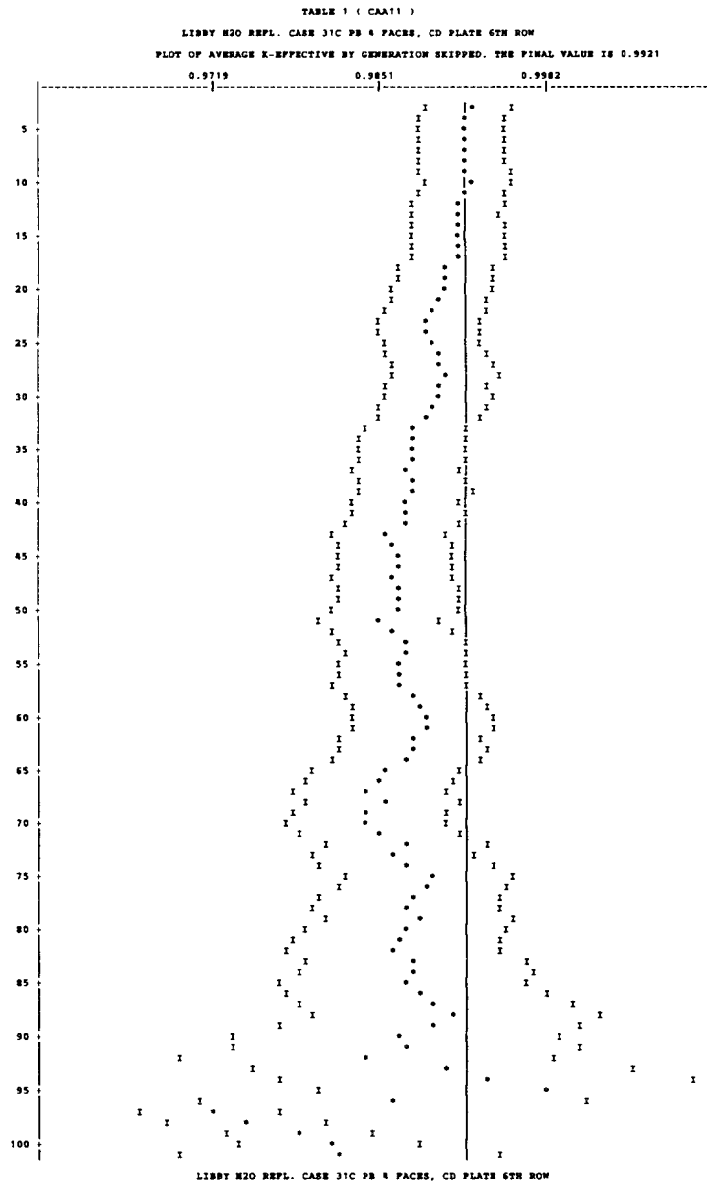


Fig. B.1 (continued)

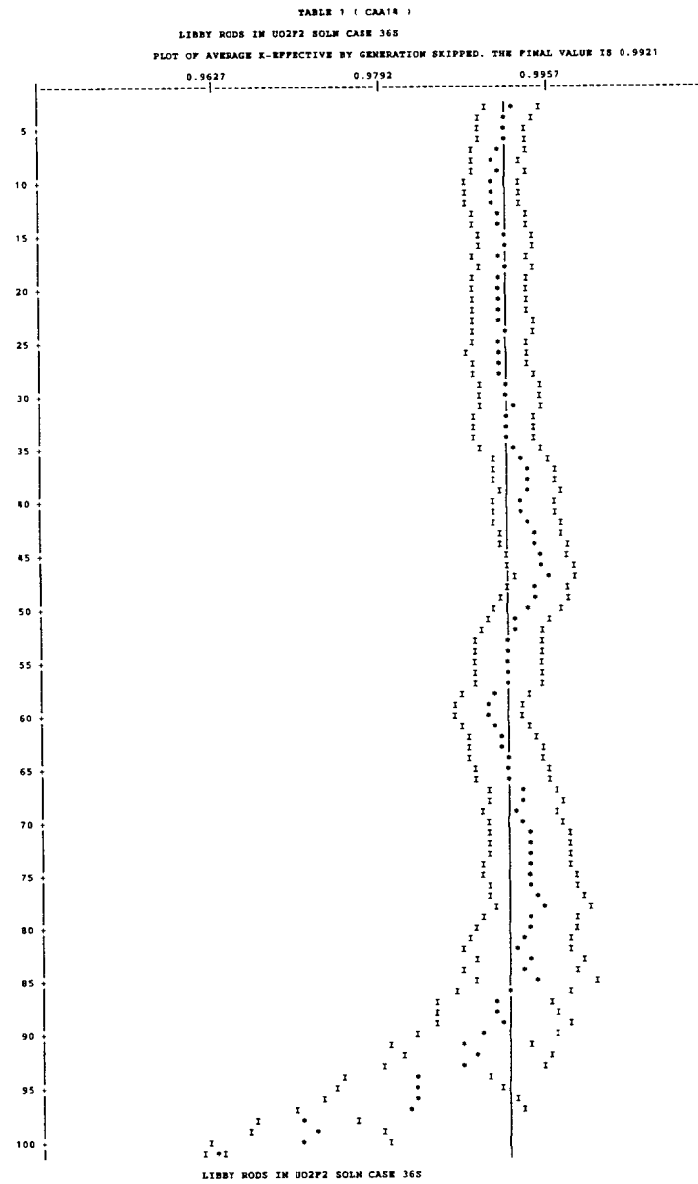
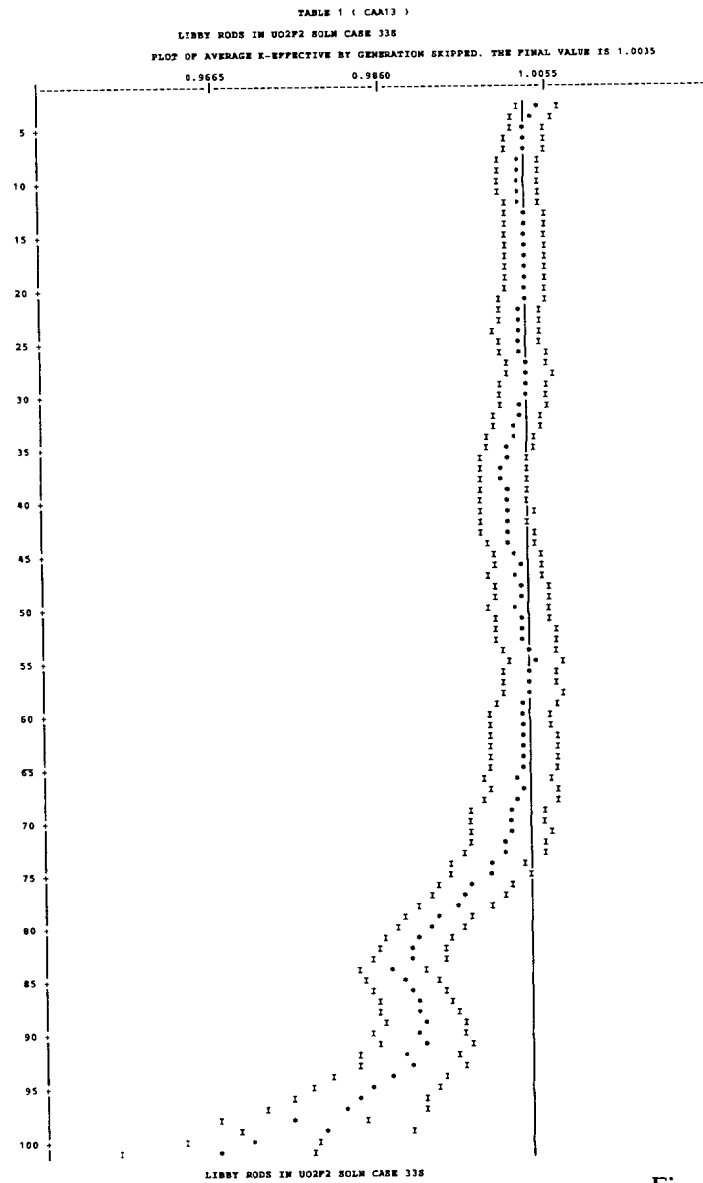


Fig. B.1 (continued)

NOTE: There are 132 pages of
keff plots in Appendix B - only
a few were reproduced and included.

Appendix C

CALCULATED RESULTS AND EXPERIMENTAL PARAMETERS

In order to analyze the data from the validation calculations, the experiments were parameterized. The results could then be categorized in a number of ways to test for trends and bias. Table C.1 contains the parameters which were used for data analysis for each experiment.

Key terms are as follows:

| | | |
|----------|---|---|
| RUN | - | Sequential number assigned to experiments. |
| MEMB | - | Case number which corresponds to Tables 1-6. |
| KEFF | - | KENO calculated k. |
| SDM | - | KENO calculated standard deviation. |
| GBAR | - | Average energy group of neutron causing fission. |
| ENRLEV | - | Enrichment level (high, intermediate, low). |
| ASSAY | - | Fuel enrichment. |
| REFLCOND | - | Reflection condition (reflected, partially reflected, unreflected). |
| REFL | - | Reflector material. |
| SYSGEOM | - | Overall system geometry (array, single unit). |
| UNITGEOM | - | Principal geometry of unit (cylinder, slab, sphere). |
| FUELMIX | - | Indicator as to whether the system was considered primarily heterogeneous or homogeneous. |
| FUEL | - | Primary form of fissile material. |
| FMATL | - | Principal fissile nuclide in fuel. |
| REF | - | Reference number for reference which describes the critical experiment. |

Table C.1. Calculational results and experimental parameters

| TABLE=1 | | | | | | | | | | | | | | |
|---------|-------|--------|--------|---------|--------|-------|----------|-------|---------|----------|---------|-------|-------|-----|
| RUN | MEMB | KEPF | SDM | GBAR | ENRLEV | ASSAY | REFLCOND | REFL | SYSGEOM | UNITGEOM | FUELMIX | FUEL | FMATL | REF |
| 1 | CAA01 | 0.9945 | 0.0036 | 21.2098 | L | 4.89 | R | H2O | A | CY | HET | METAL | U235 | 14 |
| 2 | CAA02 | 0.9912 | 0.0030 | 21.7488 | L | 4.89 | R | H2O | A | CY | HET | METAL | U235 | 14 |
| 3 | CAA03 | 0.9924 | 0.0031 | 22.8842 | L | 4.89 | R | H2O | A | CY | HET | METAL | U235 | 14 |
| 4 | CAA04 | 0.9942 | 0.0032 | 23.1207 | L | 4.89 | R | H2O | A | CY | HET | METAL | U235 | 14 |
| 5 | CAA05 | 0.9839 | 0.0034 | 23.2252 | L | 4.89 | R | H2O | A | CY | HET | METAL | U235 | 14 |
| 6 | CAA06 | 0.9957 | 0.0036 | 21.1295 | L | 4.89 | R | COMP | A | CY | HET | METAL | U235 | 14 |
| 7 | CAA07 | 0.9778 | 0.0036 | 21.4048 | L | 4.89 | R | PB | A | CY | HET | METAL | U235 | 14 |
| 8 | CAA08 | 0.9966 | 0.0030 | 22.8577 | L | 4.89 | R | PB | A | CY | HET | METAL | U235 | 14 |
| 9 | CAA09 | 0.9950 | 0.0029 | 22.7496 | L | 4.89 | R | PB | A | CY | HET | METAL | U235 | 14 |
| 10 | CAA10 | 1.0010 | 0.0032 | 20.9158 | L | 4.89 | R | PB | A | CY | HET | METAL | U235 | 14 |
| 11 | CAA11 | 0.9921 | 0.0033 | 20.8889 | L | 4.89 | R | PB | A | CY | HET | METAL | U235 | 14 |
| 12 | CAA12 | 0.9885 | 0.0026 | 24.0050 | L | 4.89 | R | UO2F2 | A | CY | HET | METAL | U235 | 14 |
| 13 | CAA13 | 1.0035 | 0.0022 | 24.3601 | L | 4.89 | R | UO2F2 | A | CY | HET | METAL | U235 | 14 |
| 14 | CAA14 | 0.9921 | 0.0025 | 24.4837 | L | 4.89 | R | UO2F2 | A | CY | HET | METAL | U235 | 14 |
| 15 | CAA15 | 0.9908 | 0.0020 | 24.1875 | L | 4.89 | R | UO2F2 | A | CY | HET | METAL | U235 | 14 |
| 16 | CAA16 | 0.9940 | 0.0025 | 24.1867 | L | 4.89 | R | UO2F2 | A | CY | HET | METAL | U235 | 14 |
| 17 | CAA17 | 0.9884 | 0.0029 | 24.2535 | L | 4.89 | R | UO2F2 | A | CY | HET | METAL | U235 | 14 |
| 18 | CAA18 | 0.9885 | 0.0025 | 24.3097 | L | 4.89 | R | UO2F2 | A | CY | HET | METAL | U235 | 14 |
| 19 | CAA19 | 0.9875 | 0.0035 | 23.3587 | L | 4.89 | U | | S | SL | HOM | U308 | U235 | 15 |
| 20 | CAA20 | 1.0030 | 0.0031 | 24.0125 | L | 4.89 | U | | S | SL | HOM | U308 | U235 | 15 |
| 21 | CAA21 | 1.0055 | 0.0029 | 24.5659 | L | 4.89 | U | | S | SL | HOM | U308 | U235 | 15 |
| 22 | CAA22 | 1.0042 | 0.0034 | 24.2557 | L | 4.89 | U | | S | SL | HOM | U308 | U235 | 15 |
| 23 | CAA23 | 0.9791 | 0.0036 | 23.3846 | L | 4.89 | R | H2O | S | SL | HOM | U308 | U235 | 15 |
| 24 | CAA24 | 0.9918 | 0.0033 | 23.6607 | L | 4.89 | R | H2O | S | SL | HOM | U308 | U235 | 15 |
| 25 | CAA25 | 1.0015 | 0.0035 | 24.1830 | L | 4.89 | R | H2O | S | SL | HOM | U308 | U235 | 15 |
| 26 | CAA26 | 0.9991 | 0.0025 | 24.6232 | L | 4.89 | R | H2O | S | SL | HOM | U308 | U235 | 15 |
| 27 | CAA27 | 0.9991 | 0.0040 | 22.8645 | L | 4.89 | R | H2O | S | SL | HOM | U308 | U235 | 15 |
| 28 | CAA28 | 0.9739 | 0.0035 | 21.6194 | L | 4.89 | R | H2O | S | SL | HOM | U308 | U235 | 15 |
| 29 | CAA29 | 0.9938 | 0.0031 | 24.3746 | L | 4.89 | R | H2O | S | SL | HOM | U308 | U235 | 15 |
| 30 | CAA30 | 0.9861 | 0.0032 | 24.2794 | L | 4.89 | U | | S | CY | HOM | UO2F2 | U235 | 15 |
| 31 | CAA31 | 0.9936 | 0.0032 | 24.2837 | L | 4.89 | U | | S | SL | HOM | UO2F2 | U235 | 15 |
| 32 | CAA32 | 0.9856 | 0.0028 | 24.5312 | L | 4.89 | U | | S | CY | HOM | UO2F2 | U235 | 15 |
| 33 | CAA33 | 0.9949 | 0.0027 | 24.7174 | L | 4.89 | U | | S | SP | HOM | UO2F2 | U235 | 15 |
| 34 | CAA34 | 0.9959 | 0.0022 | 24.7148 | L | 4.89 | U | | S | CY | HOM | UO2F2 | U235 | 15 |
| 35 | CAA35 | 1.0029 | 0.0030 | 24.3638 | L | 4.89 | R | H2O | S | CY | HOM | UO2F2 | U235 | 15 |
| 36 | CAA36 | 1.0106 | 0.0026 | 24.3983 | L | 4.89 | R | H2O | S | SL | HOM | UO2F2 | U235 | 15 |
| 37 | CAA37 | 0.9931 | 0.0027 | 24.5838 | L | 4.89 | R | H2O | S | CY | HOM | UO2F2 | U235 | 15 |
| 38 | CAA38 | 0.9927 | 0.0022 | 24.7829 | L | 4.89 | R | H2O | S | SP | HOM | UO2F2 | U235 | 15 |
| 39 | CAA39 | 1.0001 | 0.0025 | 24.7326 | L | 4.89 | R | H2O | S | CY | HOM | UO2F2 | U235 | 15 |

Table C.1 (continued)

| TABLE=2 | | | | | | | | | | | | | | |
|---------|-------|--------|--------|---------|--------|-------|----------|------|---------|----------|---------|-------|-------|-----|
| RUN | MEMB | KEFF | SDM | GBAR | ENRLEV | ASSAY | REPLCOND | REFL | SYSGEOM | UNITGEOM | FUELMIX | FUEL | FMATL | REF |
| 40 | CAB01 | 0.9893 | 0.0026 | 14.4590 | L | 3.85 | R | H2O | A | CY | HET | METAL | U235 | 16 |
| 41 | CAB02 | 1.0025 | 0.0029 | 15.9174 | L | 3.85 | R | H2O | A | CY | HET | METAL | U235 | 16 |
| 42 | CAB03 | 0.9927 | 0.0025 | 16.7417 | L | 3.85 | R | H2O | A | CY | HET | METAL | U235 | 16 |
| 43 | CAB07 | 0.9897 | 0.0025 | 13.4583 | L | 3.85 | R | H2O | A | CY | HET | METAL | U235 | 16 |
| 44 | CAB08 | 0.9924 | 0.0032 | 15.6574 | L | 3.85 | R | H2O | A | CY | HET | METAL | U235 | 16 |
| 45 | CAB09 | . | . | . | L | 3.85 | R | H2O | A | CY | HET | METAL | U235 | 16 |
| 46 | CAB10 | 0.9998 | 0.0024 | 16.8740 | L | 3.85 | R | H2O | A | CY | HET | METAL | U235 | 16 |
| 47 | CAB11 | 0.9953 | 0.0025 | 17.1558 | L | 3.85 | R | H2O | A | CY | HET | METAL | U235 | 16 |
| 48 | CAB12 | 0.9943 | 0.0028 | 17.5492 | L | 3.85 | R | H2O | A | CY | HET | METAL | U235 | 16 |
| 49 | CAB13 | 0.9960 | 0.0028 | 15.8499 | L | 3.85 | R | H2O | A | CY | HET | METAL | U235 | 16 |
| 50 | CAB14 | 1.0093 | 0.0026 | 17.1937 | L | 3.85 | R | H2O | A | CY | HET | METAL | U235 | 16 |
| 51 | CAB15 | 0.9992 | 0.0030 | 18.5920 | L | 3.85 | R | H2O | A | CY | HET | METAL | U235 | 16 |
| 52 | CAB16 | 0.9877 | 0.0029 | 19.6705 | L | 3.85 | R | H2O | A | CY | HET | METAL | U235 | 16 |

Table C.1 (continued)

TABLE-3

| RUN | MEMB | KEFF | SDM | GBAR | ENRLEV | ASSAY | REPLCOND | REPL | SYSGEOM | UNITGEOM | FUELMIX | FUEL | FMATL | REF |
|-----|-------|--------|--------|---------|--------|-------|----------|------|---------|----------|---------|-------|-------|-----|
| 53 | CAS04 | 0.9998 | 0.0022 | 23.2902 | L | 1.40 | U | | S | SL | HOM | UF4 | U235 | 17 |
| 54 | CAS05 | 0.9989 | 0.0026 | 23.2900 | L | 1.40 | U | | S | SL | HOM | UF4 | U235 | 17 |
| 55 | CAS06 | 0.9967 | 0.0022 | 23.2874 | L | 1.40 | U | | S | SL | HOM | UF4 | U235 | 17 |
| 56 | CAS11 | 1.0023 | 0.0030 | 22.5151 | L | 2.00 | R | PARA | S | SL | HOM | UF4 | U235 | 18 |
| 57 | CAS12 | 1.0096 | 0.0026 | 22.2578 | L | 2.00 | U | | S | SL | HOM | UF4 | U235 | 18 |
| 58 | CAS13 | 1.0054 | 0.0029 | 23.2545 | L | 2.00 | R | PARA | S | SL | HOM | UF4 | U235 | 18 |
| 59 | CAS14 | 1.0028 | 0.0027 | 23.0477 | L | 2.00 | U | | S | SL | HOM | UF4 | U235 | 18 |
| 60 | CAS15 | 0.9967 | 0.0024 | 23.6820 | L | 2.00 | R | PARA | S | SL | HOM | UF4 | U235 | 18 |
| 61 | CAS16 | 1.0000 | 0.0026 | 23.9033 | L | 2.00 | R | PARA | S | SL | HOM | UF4 | U235 | 18 |
| 62 | CAS17 | 0.9982 | 0.0027 | 24.1189 | L | 2.00 | R | PARA | S | SL | HOM | UF4 | U235 | 18 |
| 63 | CAS18 | 0.9975 | 0.0024 | 24.0427 | L | 2.00 | U | | S | SL | HOM | UF4 | U235 | 18 |
| 64 | CAS19 | 0.9885 | 0.0020 | 24.4577 | L | 2.00 | R | PARA | S | SL | HOM | UF4 | U235 | 18 |
| 65 | CAS20 | 0.9846 | 0.0018 | 24.4312 | L | 2.00 | U | | S | SL | HOM | UF4 | U235 | 18 |
| 66 | CAS21 | 1.0145 | 0.0030 | 22.2473 | L | 3.00 | R | PARA | S | SL | HOM | UF4 | U235 | 18 |
| 67 | CAS22 | 1.0228 | 0.0030 | 22.2309 | L | 3.00 | R | PARA | S | SL | HOM | UF4 | U235 | 18 |
| 68 | CAS23 | 1.0169 | 0.0032 | 22.2164 | L | 3.00 | R | PARA | S | SL | HOM | UF4 | U235 | 18 |
| 69 | CAS24 | 1.0129 | 0.0026 | 22.2283 | L | 3.00 | R | PARA | S | SL | HOM | UF4 | U235 | 18 |
| 70 | CAS25 | 1.0201 | 0.0032 | 22.2284 | L | 3.00 | R | PARA | S | SL | HOM | UF4 | U235 | 18 |
| 71 | CAS26 | 1.0152 | 0.0025 | 21.7760 | L | 3.00 | U | | S | SL | HOM | UF4 | U235 | 18 |
| 72 | CAS27 | 1.0187 | 0.0030 | 21.7904 | L | 3.00 | U | | S | SL | HOM | UF4 | U235 | 18 |
| 73 | CAS28 | 1.0180 | 0.0028 | 21.7835 | L | 3.00 | U | | S | SL | HOM | UF4 | U235 | 18 |
| 74 | CAS29 | 1.0131 | 0.0030 | 23.5158 | L | 3.00 | R | POLY | S | SL | HOM | UF4 | U235 | 18 |
| 75 | CAS30 | 1.0173 | 0.0030 | 23.2846 | L | 3.00 | U | | S | SL | HOM | UF4 | U235 | 18 |
| 76 | CAS31 | 1.0131 | 0.0030 | 23.2908 | L | 3.00 | U | | S | SL | HOM | UF4 | U235 | 18 |
| 77 | CAS32 | 1.0124 | 0.0030 | 23.2869 | L | 3.00 | U | | S | SL | HOM | UF4 | U235 | 18 |
| 78 | CAS33 | 0.9989 | 0.0030 | 24.2166 | L | 4.98 | R | COMP | S | CY | HOM | UO2F2 | U235 | 19 |
| 79 | CAS34 | 1.0006 | 0.0028 | 24.2332 | L | 4.98 | R | COMP | S | CY | HOM | UO2F2 | U235 | 19 |
| 80 | CAS35 | 0.9970 | 0.0034 | 24.2310 | L | 4.98 | U | | S | SP | HOM | UO2F2 | U235 | 20 |
| 81 | CAS36 | 1.0023 | 0.0032 | 24.2333 | L | 4.98 | U | | S | CY | HOM | UO2F2 | U235 | 21 |
| 82 | CAR01 | 1.0081 | 0.0034 | 21.4024 | L | 4.46 | R | PLEX | S | SL | HET | U308 | U235 | 22 |
| 83 | CAR02 | 1.0052 | 0.0031 | 21.3916 | L | 4.46 | R | PLEX | S | SL | HET | U308 | U235 | 22 |
| 84 | CAR03 | 0.9876 | 0.0030 | 19.6444 | L | 4.46 | R | PLEX | S | SL | HET | U308 | U235 | 22 |
| 85 | CAR04 | 1.0089 | 0.0029 | 21.2115 | L | 4.46 | R | CONC | S | SL | HET | U308 | U235 | 22 |
| 86 | CAR05 | 0.9998 | 0.0027 | 19.1840 | L | 4.46 | R | CONC | S | SL | HET | U308 | U235 | 22 |
| 87 | CAR06 | 0.9951 | 0.0031 | 12.8911 | L | 4.46 | R | PLEX | S | SL | HOM | U308 | U235 | 23 |
| 88 | CAR07 | 0.9998 | 0.0032 | 18.3330 | L | 4.46 | R | PLEX | S | SL | HOM | U308 | U235 | 23 |
| 89 | CAR08 | 0.9980 | 0.0036 | 19.2715 | L | 4.46 | R | PLEX | S | SL | HOM | U308 | U235 | 23 |
| 90 | CAR09 | 0.9983 | 0.0030 | 19.3540 | L | 4.46 | R | PLEX | S | SL | HOM | U308 | U235 | 23 |
| 91 | CAR10 | 1.0008 | 0.0034 | 17.7171 | L | 4.46 | R | CONC | S | SL | HOM | U308 | U235 | 23 |
| 92 | CAR11 | 1.0073 | 0.0032 | 21.5573 | L | 4.46 | R | PLEX | S | SL | HET | U308 | U235 | 24 |
| 93 | CAR12 | 1.0109 | 0.0031 | 20.2060 | L | 4.46 | R | PLEX | S | SL | HET | U308 | U235 | 24 |
| 94 | CAR13 | 1.0108 | 0.0032 | 20.1720 | L | 4.46 | R | PLEX | S | SL | HET | U308 | U235 | 24 |
| 95 | CAR14 | 0.9907 | 0.0034 | 18.5482 | L | 4.46 | R | PLEX | S | SL | HOM | U308 | U235 | 24 |
| 96 | CAR15 | 1.0106 | 0.0033 | 18.5995 | L | 4.46 | R | PLEX | S | SL | HOM | U308 | U235 | 24 |
| 97 | CAR16 | 0.9978 | 0.0036 | 19.2434 | L | 4.46 | R | PLEX | S | SL | HOM | U308 | U235 | 24 |
| 98 | CAR17 | 1.0069 | 0.0033 | 20.7665 | L | 4.46 | R | PLEX | S | SL | HET | U308 | U235 | 25 |
| 99 | CAR18 | 1.0005 | 0.0030 | 21.8233 | L | 4.46 | R | PLEX | S | SL | HET | U308 | U235 | 25 |
| 100 | CAR19 | 1.0097 | 0.0032 | 18.2384 | L | 4.46 | R | PLEX | S | SL | HOM | U308 | U235 | 25 |
| 101 | CAR20 | 0.9911 | 0.0031 | 18.4058 | L | 4.46 | R | PLEX | S | SL | HOM | U308 | U235 | 25 |

Table C.1 (continued)

| TABLE-C | | | | | | | | | | | | | | |
|---------|-------|--------|--------|---------|--------|-------|----------|------|---------|----------|---------|---------|-------|-----|
| RUN | MEMB | KEFF | SDM | GBAR | ENRLEV | ASSAY | REFLCOND | REFL | SYSGROM | UNITGROM | FUELMIX | FUEL | FMATL | REF |
| 102 | CAA01 | 1.0096 | 0.0026 | 24.9405 | H | 93.20 | U | | S | SP | HOM | UO2F2 | U235 | 26 |
| 103 | CAA02 | 1.0036 | 0.0023 | 25.0019 | H | 93.20 | U | | S | SP | HOM | UO2F2 | U235 | 26 |
| 104 | CAA03 | 0.9998 | 0.0023 | 24.9968 | H | 93.20 | U | | S | SP | HOM | NITRATE | U235 | 26 |
| 105 | CAA04 | 1.0071 | 0.0039 | 22.5453 | H | 93.20 | R | H2O | S | SP | HOM | UO2F2 | U235 | 26 |
| 106 | CAA05 | 0.9971 | 0.0046 | 23.4178 | H | 93.20 | R | H2O | S | SP | HOM | UO2F2 | U235 | 26 |
| 107 | CAA06 | 0.9964 | 0.0023 | 24.9948 | H | 93.20 | R | H2O | S | SP | HOM | UO2F2 | U235 | 26 |
| 108 | CAA07 | 1.0097 | 0.0043 | 24.2629 | H | 93.20 | R | H2O | S | SP | HOM | UO2F2 | U235 | 27 |
| 109 | CAA08 | 1.0212 | 0.0033 | 24.6833 | H | 93.20 | R | H2O | S | SP | HOM | UO2F2 | U235 | 27 |
| 110 | CAA09 | 0.9991 | 0.0039 | 23.7419 | H | 93.20 | U | | S | SP | HOM | UO2F2 | U235 | 27 |
| 111 | CAA10 | 1.0164 | 0.0042 | 24.1535 | H | 93.20 | R | H2O | S | SP | HOM | UO2F2 | U235 | 27 |
| 112 | CAA11 | 1.0351 | 0.0039 | 24.6366 | H | 93.20 | R | H2O | S | SP | HOM | UO2F2 | U235 | 27 |
| 113 | CAA12 | 1.0090 | 0.0039 | 23.6132 | H | 93.20 | U | | S | CY | HOM | NITRATE | U235 | 28 |
| 114 | CAA13 | 1.0060 | 0.0035 | 21.6046 | H | 93.20 | U | | S | CY | HOM | NITRATE | U235 | 28 |
| 115 | CAA14 | 1.0119 | 0.0042 | 24.5733 | H | 93.20 | U | | S | CY | HOM | NITRATE | U235 | 28 |
| 116 | CAA15 | 1.0027 | 0.0046 | 23.6688 | H | 93.20 | U | | S | CY | HOM | NITRATE | U235 | 28 |
| 117 | CAA16 | 1.0024 | 0.0045 | 21.5956 | H | 93.20 | U | | S | CY | HOM | NITRATE | U235 | 28 |
| 118 | CAA17 | 1.0106 | 0.0041 | 23.6234 | H | 93.20 | R | CONC | S | CY | HOM | NITRATE | U235 | 28 |
| 119 | CAA18 | 1.0145 | 0.0044 | 21.8900 | H | 93.20 | R | CONC | S | CY | HOM | NITRATE | U235 | 28 |
| 120 | CAA19 | 1.0056 | 0.0043 | 23.6210 | H | 93.20 | R | CONC | S | CY | HOM | NITRATE | U235 | 28 |
| 121 | CAA20 | 1.0037 | 0.0044 | 21.8675 | H | 93.20 | R | CONC | S | CY | HOM | NITRATE | U235 | 28 |
| 122 | CAA21 | 1.0094 | 0.0040 | 23.6508 | H | 93.20 | R | CONC | S | CY | HOM | NITRATE | U235 | 28 |
| 123 | CAA22 | 1.0092 | 0.0037 | 21.9725 | H | 93.20 | R | CONC | S | CY | HOM | NITRATE | U235 | 28 |
| 124 | CAA23 | 1.0085 | 0.0040 | 23.6011 | H | 93.20 | R | PLEX | S | CY | HOM | NITRATE | U235 | 28 |
| 125 | CAA24 | 1.0113 | 0.0047 | 21.8062 | H | 93.20 | R | PLEX | S | CY | HOM | NITRATE | U235 | 28 |
| 126 | CAA25 | 0.9947 | 0.0041 | 23.5969 | H | 93.20 | R | PLEX | S | CY | HOM | NITRATE | U235 | 28 |
| 127 | CAA26 | 1.0033 | 0.0040 | 21.8159 | H | 93.20 | R | PLEX | S | CY | HOM | NITRATE | U235 | 28 |
| 128 | CAA27 | 1.0157 | 0.0034 | 23.6729 | H | 93.20 | R | PLEX | S | CY | HOM | NITRATE | U235 | 28 |
| 129 | CAA28 | 1.0141 | 0.0043 | 22.0524 | H | 93.20 | R | PLEX | S | CY | HOM | NITRATE | U235 | 28 |
| 130 | CAA29 | 1.0046 | 0.0033 | 24.4591 | H | 93.20 | R | CONC | A | CY | HOM | NITRATE | U235 | 28 |
| 131 | CAA30 | 1.0061 | 0.0041 | 21.9559 | H | 93.20 | R | CONC | A | CY | HOM | NITRATE | U235 | 28 |
| 132 | CAA31 | 1.0119 | 0.0035 | 24.3045 | H | 93.20 | R | CONC | A | CY | HOM | NITRATE | U235 | 28 |
| 133 | CAA32 | 1.0056 | 0.0041 | 21.9640 | H | 93.20 | R | CONC | A | CY | HOM | NITRATE | U235 | 28 |
| 134 | CAA33 | 1.0098 | 0.0033 | 24.3539 | H | 93.20 | R | CONC | A | CY | HOM | NITRATE | U235 | 28 |
| 135 | CAA34 | 1.0014 | 0.0038 | 21.7453 | H | 93.20 | R | CONC | A | CY | HOM | NITRATE | U235 | 28 |
| 136 | CAA35 | 1.0129 | 0.0045 | 21.9253 | H | 93.20 | R | CONC | A | CY | HOM | NITRATE | U235 | 28 |
| 137 | CAA36 | 1.0099 | 0.0039 | 21.9359 | H | 93.20 | R | CONC | A | CY | HOM | NITRATE | U235 | 28 |
| 138 | CAA37 | 1.0000 | 0.0034 | 24.5738 | H | 93.20 | R | PLEX | A | CY | HOM | NITRATE | U235 | 28 |
| 139 | CAA38 | 0.9961 | 0.0038 | 22.1639 | H | 93.20 | R | PLEX | A | CY | HOM | NITRATE | U235 | 28 |
| 140 | CAA39 | 1.0045 | 0.0034 | 24.5916 | H | 93.20 | R | PLEX | A | CY | HOM | NITRATE | U235 | 28 |
| 141 | CAA40 | 0.9985 | 0.0039 | 22.2004 | H | 93.20 | R | PLEX | A | CY | HOM | NITRATE | U235 | 28 |
| 142 | CAA41 | 0.9984 | 0.0040 | 24.5568 | H | 93.20 | R | PLEX | A | CY | HOM | NITRATE | U235 | 28 |
| 143 | CAA42 | 1.0041 | 0.0036 | 21.9131 | H | 93.20 | R | PLEX | A | CY | HOM | NITRATE | U235 | 28 |
| 144 | CAA43 | 0.9982 | 0.0038 | 22.1281 | H | 93.20 | R | PLEX | A | CY | HOM | NITRATE | U235 | 28 |

Table C.1 (continued)

| TABLE-5 | | | | | | | | | | | | | | |
|---------|-------|--------|--------|---------|--------|-------|----------|------|---------|----------|---------|---------|-------|-----|
| RUN | MEMB | KEFF | SDM | GBAR | ENRLEV | ASSAY | REFLCOND | REFL | SYSGEOM | UNITGEOM | FUELMIX | FUEL | FMATL | REF |
| 145 | CAS01 | 1.0004 | 0.0027 | 4.8613 | H | 93.80 | U | | S | SP | HOM | METAL | U235 | 29 |
| 146 | CAS02 | 0.9995 | 0.0031 | 8.5157 | H | 97.67 | R | H2O | S | SP | HOM | METAL | U235 | 35 |
| 147 | CAS03 | 1.0029 | 0.0044 | 21.7017 | H | 93.20 | U | | S | CY | HOM | NITRATE | U235 | 28 |
| 148 | CAS04 | 1.0067 | 0.0028 | 4.9879 | H | 93.20 | U | | S | CY | HOM | ALLOY | U235 | 30 |
| 149 | CAS05 | 1.0023 | 0.0027 | 25.0041 | H | 93.20 | U | | S | SP | HOM | UO2F2 | U235 | 26 |
| 150 | CAS06 | 1.0012 | 0.0022 | 24.9987 | H | 93.20 | U | | S | SP | HOM | NITRATE | U235 | 31 |
| 151 | CAS07 | 1.0042 | 0.0030 | 11.7017 | H | 93.50 | R | H2O | S | SP | HET | METAL | U235 | 32 |
| 152 | CAS08 | 1.0124 | 0.0031 | 6.4136 | H | 93.20 | R | C | S | CY | HET | METAL | U235 | 33 |
| 153 | CAS09 | 1.0027 | 0.0025 | 4.9072 | H | 94.00 | R | U238 | S | SL | HOM | METAL | U235 | 32 |
| 154 | CAS10 | 1.0114 | 0.0034 | 10.4697 | H | 93.10 | R | OIL | S | SP | HET | METAL | U235 | 33 |
| 155 | CAS11 | 0.9977 | 0.0035 | 9.4346 | H | 93.10 | R | OIL | S | SP | HET | METAL | U235 | 34 |
| 156 | CAS12 | 1.0004 | 0.0031 | 4.8365 | H | 93.20 | U | | M | CY | HOM | METAL | U235 | 36 |
| 157 | CAS13 | 0.9854 | 0.0035 | 24.5321 | H | 92.60 | U | | A | CY | HOM | NITRATE | U235 | 38 |
| 158 | CAS14 | 1.0585 | 0.0038 | 21.1722 | H | 93.20 | R | PLEX | A | MIX | HOM | NITRATE | U235 | 39 |
| 159 | CAS15 | 1.0126 | 0.0030 | 8.2822 | H | 93.20 | R | POLY | A | CY | HET | METAL | U235 | 40 |
| 160 | CAS16 | 0.9879 | 0.0037 | 21.4089 | H | 92.60 | U | | A | CY | HOM | NITRATE | U235 | 38 |
| 161 | CAS17 | 1.0250 | 0.0037 | 22.1149 | H | 92.60 | R | PARA | A | CY | HOM | NITRATE | U235 | 38 |
| 162 | CAS18 | 1.0010 | 0.0045 | 21.5958 | H | 92.60 | R | PLEX | A | CY | HOM | NITRATE | U235 | 38 |
| 163 | CAS19 | 1.0329 | 0.0046 | 20.7978 | H | 93.10 | U | | A | CY | HOM | NITRATE | U235 | 41 |
| 164 | CAS20 | 1.0369 | 0.0037 | 22.2455 | H | 93.20 | R | PLEX | A | CY | HOM | NITRATE | U235 | 28 |
| 165 | CAS21 | 1.0239 | 0.0043 | 21.9649 | H | 93.20 | R | CONC | A | CY | HOM | NITRATE | U235 | 28 |
| 166 | CAS22 | 1.0082 | 0.0034 | 4.8329 | H | 93.20 | U | | M | CY | HOM | METAL | U235 | 36 |
| 167 | CAS23 | 0.9959 | 0.0030 | 4.8188 | H | 93.20 | U | | M | MIX | HOM | METAL | U235 | 36 |
| 168 | CAS24 | 0.9928 | 0.0033 | 4.8267 | H | 93.20 | U | | A | CY | HOM | METAL | U235 | 37 |
| 169 | CAS25 | 1.0079 | 0.0030 | 4.8332 | H | 93.20 | U | | A | CY | HOM | METAL | U235 | 37 |
| 170 | CAS26 | 1.0011 | 0.0033 | 10.0912 | H | 93.20 | R | PARA | A | CY | HOM | METAL | U235 | 37 |
| 171 | CAS27 | 1.0083 | 0.0031 | 10.3812 | H | 93.20 | R | PARA | A | CY | HOM | METAL | U235 | 37 |
| 172 | CAS28 | 1.0102 | 0.0037 | 7.6142 | H | 93.20 | U | | A | CY | HET | METAL | U235 | 37 |
| 173 | CAS29 | 0.9872 | 0.0041 | 21.4050 | H | 92.60 | U | | A | CY | HOM | NITRATE | U235 | 38 |
| 174 | CAS30 | 0.9978 | 0.0038 | 24.2763 | H | 93.20 | U | | S | SL | HOM | UO2F2 | U235 | 43 |
| 175 | CAS31 | 0.9949 | 0.0035 | 24.3936 | H | 93.20 | R | H2O | S | SL | HOM | UO2F2 | U235 | 43 |
| 176 | CAS32 | 0.9805 | 0.0039 | 24.2603 | H | 93.20 | U | | A | SL | HOM | UO2F2 | U235 | 43 |
| 177 | CAS33 | 0.9995 | 0.0039 | 24.5095 | H | 93.20 | R | H2O | A | SL | HOM | UO2F2 | U235 | 43 |
| 178 | CAS34 | 0.9803 | 0.0039 | 24.2515 | H | 93.20 | U | | A | SL | HOM | UO2F2 | U235 | 43 |
| 179 | CAS35 | 0.9906 | 0.0036 | 24.5440 | H | 93.20 | R | H2O | A | SL | HOM | UO2F2 | U235 | 43 |
| 180 | CAS36 | 0.9933 | 0.0035 | 24.2518 | H | 93.20 | U | | A | SL | HOM | UO2F2 | U235 | 43 |
| 181 | CAS37 | 1.0030 | 0.0031 | 24.5294 | H | 93.20 | R | H2O | A | SL | HOM | UO2F2 | U235 | 43 |
| 182 | CAS38 | 0.9881 | 0.0035 | 24.2464 | H | 93.20 | U | | A | SL | HOM | UO2F2 | U235 | 43 |
| 183 | CAS39 | 0.9952 | 0.0035 | 24.5228 | H | 93.20 | R | H2O | A | SL | HOM | UO2F2 | U235 | 43 |
| 184 | CAS40 | 0.9824 | 0.0041 | 24.2482 | H | 93.20 | U | | A | SL | HOM | UO2F2 | U235 | 43 |
| 185 | CAS41 | 0.9767 | 0.0038 | 24.2608 | H | 93.20 | U | | A | SL | HOM | UO2F2 | U235 | 43 |
| 186 | CAS42 | 0.9916 | 0.0037 | 24.2631 | H | 93.20 | U | | A | SL | HOM | UO2F2 | U235 | 43 |
| 187 | CAS43 | 0.9835 | 0.0037 | 24.2624 | H | 93.20 | U | | A | SL | HOM | UO2F2 | U235 | 43 |
| 188 | CAS44 | 0.9757 | 0.0035 | 24.2571 | H | 93.20 | U | | A | SL | HOM | UO2F2 | U235 | 43 |
| 189 | CAS45 | 0.9871 | 0.0040 | 24.2721 | H | 93.20 | U | | S | SL | HOM | UO2F2 | U235 | 43 |
| 190 | CAS46 | 0.9832 | 0.0040 | 24.2529 | H | 93.20 | U | | A | SL | HOM | UO2F2 | U235 | 43 |
| 191 | CAS47 | 0.9819 | 0.0037 | 24.2521 | H | 93.20 | U | | A | SL | HOM | UO2F2 | U235 | 43 |
| 192 | CAS48 | 0.9813 | 0.0039 | 24.2524 | H | 93.20 | U | | A | SL | HOM | UO2F2 | U235 | 43 |
| 193 | CAS49 | 0.9831 | 0.0045 | 24.2540 | H | 93.20 | U | | A | SL | HOM | UO2F2 | U235 | 43 |
| 194 | CAS50 | 0.9814 | 0.0038 | 24.2552 | H | 93.20 | U | | A | SL | HOM | UO2F2 | U235 | 43 |
| 195 | CAS51 | 0.9791 | 0.0036 | 24.2558 | H | 93.20 | U | | A | SL | HOM | UO2F2 | U235 | 43 |
| 196 | CAS52 | 0.9852 | 0.0038 | 24.2583 | H | 93.20 | U | | A | SL | HOM | UO2F2 | U235 | 43 |
| 197 | CAS53 | 0.9884 | 0.0039 | 24.2670 | H | 93.20 | U | | A | SL | HOM | UO2F2 | U235 | 43 |

Table C.1 (continued)

| TABLE=5 (CONTINUED) | | | | | | | | | | | | | | |
|---------------------|-------|--------|--------|---------|--------|-------|----------|------|---------|----------|---------|---------|-------|-----|
| RUN | MEMB | KEFF | SDM | GBAR | ENRLEV | ASSAY | REPLCOND | REPL | SYSGEOM | UNITGEOM | FUELMIX | FUEL | FMATL | REF |
| 198 | CAS54 | 0.9831 | 0.0034 | 24.2588 | H | 93.20 | U | | A | SL | HOM | UO2F2 | U235 | 43 |
| 199 | CAS55 | 0.9876 | 0.0038 | 24.2616 | H | 93.20 | U | | A | SL | HOM | UO2F2 | U235 | 43 |
| 200 | CAS56 | 0.9869 | 0.0042 | 24.2615 | H | 93.20 | U | | A | SL | HOM | UO2F2 | U235 | 43 |
| 201 | CAS57 | 0.9864 | 0.0041 | 24.2662 | H | 93.20 | U | | A | SL | HOM | UO2F2 | U235 | 43 |
| 202 | CAS58 | 0.9824 | 0.0037 | 24.2548 | H | 93.20 | U | | A | SL | HOM | UO2F2 | U235 | 43 |
| 203 | CAS59 | 0.9836 | 0.0036 | 24.2658 | H | 93.20 | U | | A | SL | HOM | UO2F2 | U235 | 43 |
| 204 | CAS60 | 0.9998 | 0.0036 | 22.5166 | H | 92.60 | U | | A | CY | HOM | NITRATE | U235 | 38 |
| 205 | CAS61 | 1.0005 | 0.0038 | 22.5263 | H | 92.60 | U | | A | CY | HOM | NITRATE | U235 | 38 |
| 206 | CAS62 | 0.9934 | 0.0039 | 21.4562 | H | 92.60 | U | | A | CY | HOM | NITRATE | U235 | 38 |
| 207 | CAS63 | 1.0050 | 0.0044 | 21.4410 | H | 92.60 | U | | A | CY | HOM | NITRATE | U235 | 38 |
| 208 | CAS64 | 0.9963 | 0.0038 | 21.4417 | H | 92.60 | U | | A | CY | HOM | NITRATE | U235 | 38 |
| 209 | CAS65 | 1.0081 | 0.0039 | 21.4918 | H | 92.60 | U | | A | CY | HOM | NITRATE | U235 | 38 |
| 210 | CAS66 | 1.0020 | 0.0037 | 21.6613 | H | 92.60 | P | PLEX | A | CY | HOM | NITRATE | U235 | 38 |
| 211 | CAS67 | 1.0217 | 0.0038 | 21.8258 | H | 92.60 | P | PLEX | A | CY | HOM | NITRATE | U235 | 38 |
| 212 | CAS68 | 1.0170 | 0.0042 | 21.7269 | H | 92.60 | P | PLEX | A | CY | HOM | NITRATE | U235 | 38 |
| 213 | CAS69 | 1.0227 | 0.0040 | 22.1217 | H | 92.60 | R | PARA | A | CY | HOM | NITRATE | U235 | 38 |
| 214 | CAS70 | 1.0205 | 0.0039 | 22.0406 | H | 92.60 | P | PARA | A | CY | HOM | NITRATE | U235 | 38 |
| 215 | CAS71 | 1.0302 | 0.0040 | 22.1075 | H | 92.60 | P | PARA | A | CY | HOM | NITRATE | U235 | 38 |
| 216 | CAS72 | 1.0016 | 0.0038 | 21.5822 | H | 92.60 | P | PLEX | A | CY | HOM | NITRATE | U235 | 38 |
| 217 | CAS73 | 1.0134 | 0.0041 | 21.6538 | H | 92.60 | P | PARA | A | CY | HOM | NITRATE | U235 | 38 |
| 218 | CAS74 | 1.0172 | 0.0035 | 22.1229 | H | 92.60 | R | PARA | A | CY | HOM | NITRATE | U235 | 38 |
| 219 | CAS75 | 1.0300 | 0.0037 | 22.0009 | H | 92.60 | P | PARA | A | CY | HOM | NITRATE | U235 | 38 |
| 220 | CAS76 | 1.0046 | 0.0044 | 21.6952 | H | 92.60 | P | PLEX | A | CY | HOM | NITRATE | U235 | 38 |
| 221 | CAS77 | 1.0225 | 0.0040 | 22.1244 | H | 92.60 | P | PLEX | A | CY | HOM | NITRATE | U235 | 38 |
| 222 | CAS78 | 1.0237 | 0.0045 | 22.1373 | H | 92.60 | R | PLEX | A | CY | HOM | NITRATE | U235 | 38 |
| 223 | CAS79 | 1.0137 | 0.0036 | 21.8230 | H | 92.60 | P | PLEX | A | CY | HOM | NITRATE | U235 | 38 |
| 224 | CAS80 | 1.0223 | 0.0045 | 21.9906 | H | 92.60 | P | PLEX | A | CY | HOM | NITRATE | U235 | 38 |
| 225 | CAS81 | 1.0197 | 0.0037 | 22.0513 | H | 92.60 | P | PLEX | A | CY | HOM | NITRATE | U235 | 38 |
| 226 | CAS82 | 1.0195 | 0.0038 | 21.7696 | H | 92.60 | P | PLEX | A | CY | HOM | NITRATE | U235 | 38 |
| 227 | CAS83 | 1.0225 | 0.0039 | 22.0273 | H | 92.60 | P | PLEX | A | CY | HOM | NITRATE | U235 | 38 |
| 228 | CAS84 | 1.0247 | 0.0041 | 22.1092 | H | 92.60 | P | PLEX | A | CY | HOM | NITRATE | U235 | 38 |
| 229 | CAS85 | 1.0175 | 0.0046 | 21.6264 | H | 92.60 | P | PLEX | A | CY | HOM | NITRATE | U235 | 38 |
| 230 | CAS86 | 1.0165 | 0.0042 | 21.6814 | H | 92.60 | P | PARA | A | CY | HOM | NITRATE | U235 | 38 |
| 231 | CAS87 | 1.0177 | 0.0042 | 22.1061 | H | 92.60 | R | PARA | A | CY | HOM | NITRATE | U235 | 38 |
| 232 | CAS88 | 1.0177 | 0.0041 | 22.0003 | H | 92.60 | P | PARA | A | CY | HOM | NITRATE | U235 | 38 |
| 233 | CAS89 | 1.0169 | 0.0046 | 22.1067 | H | 92.60 | P | PARA | A | CY | HOM | NITRATE | U235 | 38 |
| 234 | CAS90 | 0.9977 | 0.0042 | 21.7689 | H | 92.60 | U | | A | CY | HOM | NITRATE | U235 | 38 |
| 235 | CAS91 | 1.0052 | 0.0036 | 24.5355 | H | 92.60 | U | | A | CY | HOM | NITRATE | U235 | 38 |

Table C.1 (continued)

| TABLE-6 | | | | | | | | | | | | | | |
|---------|-------|--------|--------|---------|--------|-------|----------|------|---------|----------|---------|---------|-------|-----|
| RUN | MEMB | KEFF | SDM | GBAR | ENRLEV | ASSAY | REPLCOND | REPL | SYSGEOM | UNITGEOM | FUELMIX | FUEL | FMATL | REF |
| 236 | CAS01 | 0.9979 | 0.0022 | 24.9978 | H | 93.20 | U | | S | SP | HOM | NITRATE | U235 | 12 |
| 237 | CAS02 | 0.9960 | 0.0023 | 24.9338 | H | 93.20 | U | | S | SP | HOM | NITRATE | U235 | 12 |
| 238 | CAS03 | 0.9920 | 0.0027 | 24.8696 | H | 93.20 | U | | S | SP | HOM | NITRATE | U235 | 12 |
| 239 | CAS04 | 1.0020 | 0.0024 | 24.8423 | H | 93.20 | U | | S | SP | HOM | NITRATE | U235 | 12 |
| 240 | CAS05 | 1.0086 | 0.0022 | 24.6298 | H | 97.70 | U | | S | SP | HOM | NITRATE | U233 | 12 |
| 241 | CAS06 | 1.0079 | 0.0025 | 24.6005 | H | 97.70 | U | | S | SP | HOM | NITRATE | U233 | 12 |
| 242 | CAS07 | 1.0045 | 0.0023 | 24.5747 | H | 97.70 | U | | S | SP | HOM | NITRATE | U233 | 12 |
| 243 | CAS08 | 1.0065 | 0.0023 | 24.5493 | H | 97.70 | U | | S | SP | HOM | NITRATE | U233 | 12 |
| 244 | CAS09 | 1.0084 | 0.0023 | 24.5177 | H | 97.70 | U | | S | SP | HOM | NITRATE | U233 | 12 |
| 245 | CAS10 | 0.9979 | 0.0017 | 25.0633 | H | 93.20 | U | | S | SP | HOM | NITRATE | U235 | 12 |
| 246 | CAS11 | 0.9959 | 0.0017 | 24.7279 | H | 97.70 | U | | S | SP | HOM | NITRATE | U233 | 12 |
| 247 | CAS12 | 0.9989 | 0.0023 | 25.0338 | H | 93.20 | U | | S | CY | HOM | NITRATE | U235 | 12 |
| 248 | CAS13 | 0.9983 | 0.0022 | 25.0378 | H | 93.20 | U | | S | CY | HOM | NITRATE | U235 | 12 |
| 249 | CAS14 | 0.9992 | 0.0017 | 25.0618 | H | 93.20 | U | | S | CY | HOM | NITRATE | U235 | 12 |
| 250 | CAS15 | 0.9925 | 0.0019 | 25.0692 | H | 93.20 | U | | S | CY | HOM | NITRATE | U235 | 12 |
| 251 | CAS16 | 0.9976 | 0.0016 | 25.0784 | H | 93.20 | U | | S | CY | HOM | NITRATE | U235 | 12 |
| 252 | CAS17 | 0.9952 | 0.0020 | 24.6961 | H | 97.70 | U | | S | CY | HOM | NITRATE | U233 | 12 |
| 253 | CAS18 | 0.9973 | 0.0018 | 24.7122 | H | 97.70 | U | | S | CY | HOM | NITRATE | U233 | 12 |
| 254 | CAS19 | 0.9916 | 0.0015 | 24.7286 | H | 97.70 | U | | S | CY | HOM | NITRATE | U233 | 12 |
| 255 | CAS20 | 0.9927 | 0.0015 | 24.7480 | H | 97.70 | U | | S | CY | HOM | NITRATE | U233 | 12 |
| 256 | CAS21 | 0.9923 | 0.0015 | 25.0740 | H | 93.20 | U | | S | CY | HOM | NITRATE | U235 | 12 |
| 257 | CAS22 | 0.9915 | 0.0014 | 25.0786 | H | 93.20 | U | | S | CY | HOM | NITRATE | U235 | 12 |
| 258 | CAS23 | 0.9991 | 0.0014 | 25.0846 | H | 93.20 | U | | S | CY | HOM | NITRATE | U235 | 12 |

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